

Research and Development of Imaging Bolometers

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National Fusion Research Center

Topics

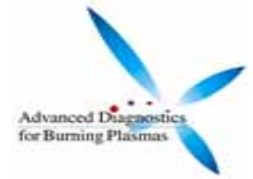
Advanced Diagnostics
for Burning Plasmas

- Definition and Motivation
- Conventional resistive bolometers
- IRVB concept & data analysis
- Sensitivity, foil material & IR cameras
- JT-60U IRVB
- JT-60U IRVB sample data
- JT-60U IRVB bolometer video
- 2-D profiles with tomography of IRVB
- Plans for JT-60U IRVB Upgrade
- Imaging Bolometer for ITER
- New detector foil R&D
- Summary & Conclusions



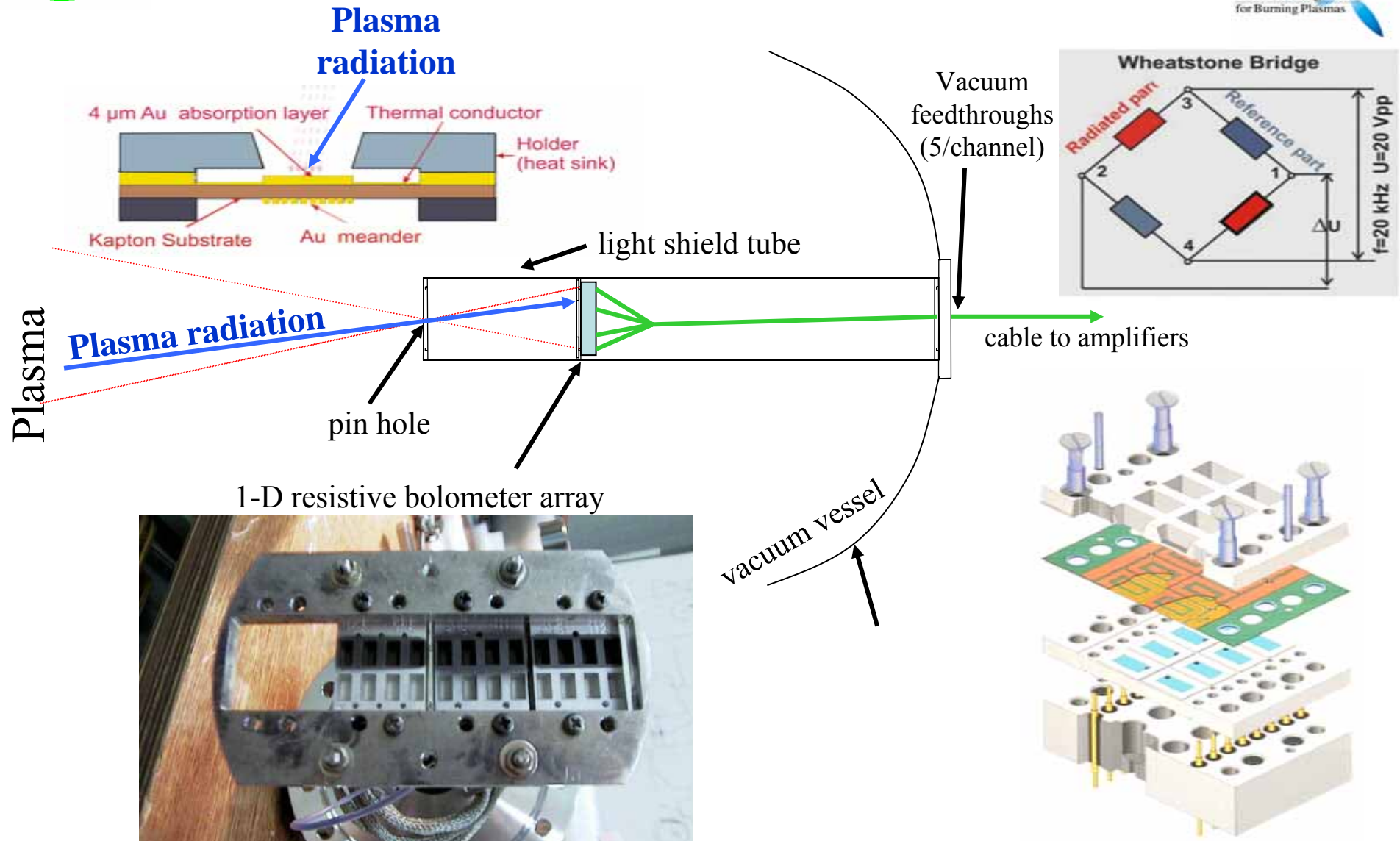


What is a Bolometer?



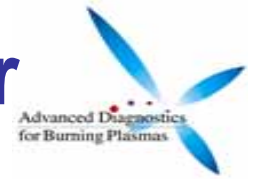
- Original definition – device whose **electrical properties** change **in response to radiation**
- **Resistive bolometer** first conceived in **1878** by S. P. Langley to **measure solar radiation**
- Used in **fusion plasma** physics to measure **total, broadband (IR – X-ray) radiated power**
- For **power balance** and **impurity radiation** studies

Resistive Bolometer – Concept





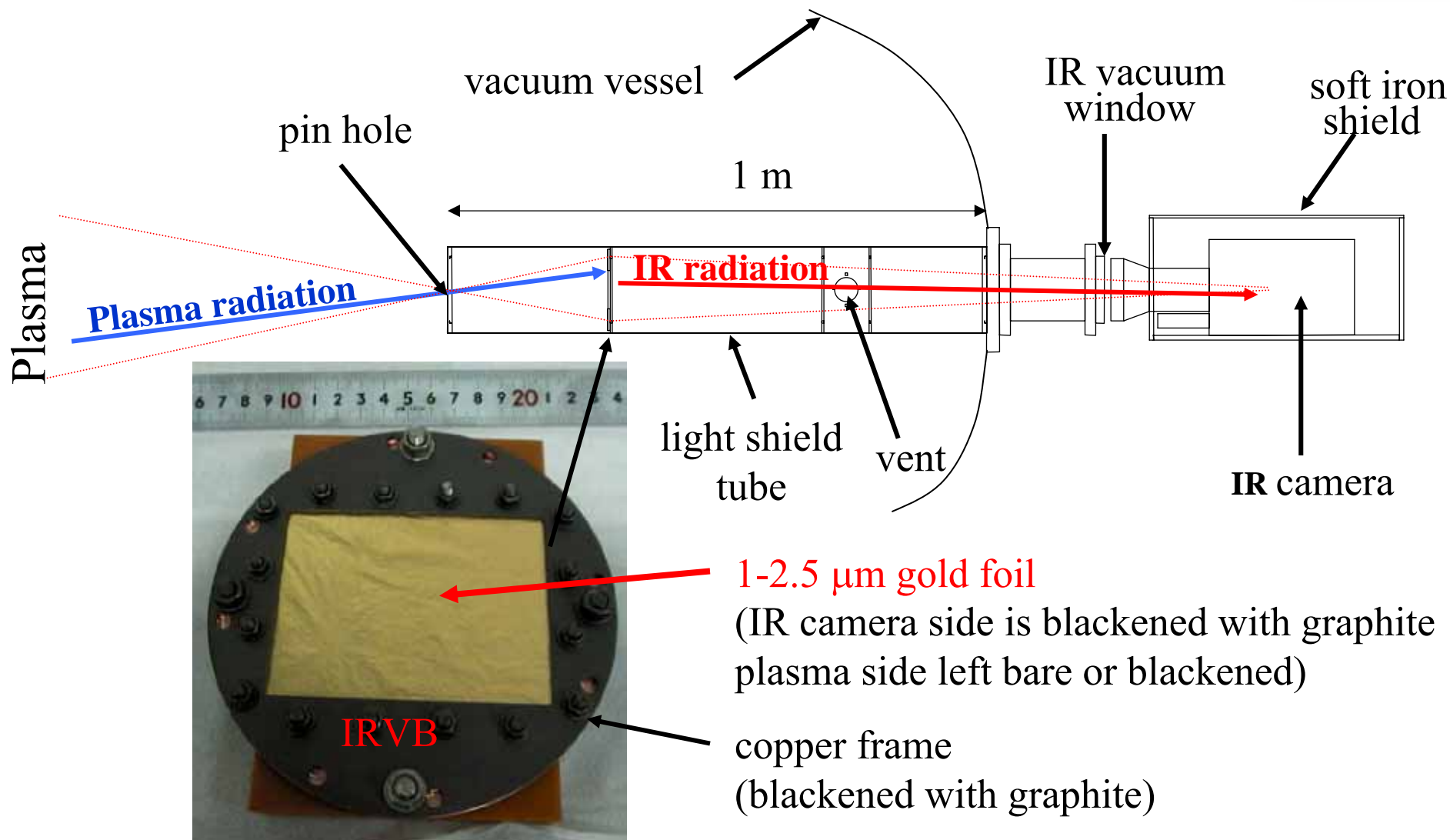
Motivation for IR Imaging Bolometer



- Real-time **measurements of** local **radiation** power loss **necessary for fusion reactor**
- Fusion **reactor conditions pose challenges** (RIEMF, fragile contacts, etc.) **to** conventional existing **wire-based** radiation sensing **devices** (resistive bolometers)
- **Lack of** a simple, reliable and cost effective **technique for** the **measurement of radiation** inside the vacuum vessel of a fusion reactor
- Continuing **advances in infrared detector** technology **provide** an **opportunity** to measure radiation fluxes in a reactor environment using thin absorber foils



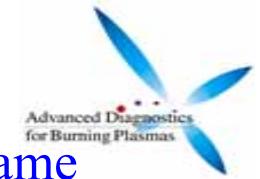
IR imaging Video Bolometer (IRVB) – Concept



[1] B.J. Peterson, *Rev. Sci. Instrum.* **70** (2000) 3696. [2] B.J. Peterson *et al.*, *Rev. Sci. Instrum.* **72** (2001) 923.



IRVB - Concept



Heat diffusion equation for foil:

$$-\Omega_{rad} + \Omega_{bb} + \frac{1}{\kappa} \frac{\partial T}{\partial t} = \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2}$$

2-D
Laplacian

foil thermal diffusivity

$$\Omega_{bb} = \frac{\epsilon \sigma_{S-B} (T^4 - T_0^4)}{kt_f} \quad \epsilon \cong 1$$

black body cooling term

$$\Omega_{rad} = \frac{P_{rad}}{kt_f l^2}$$

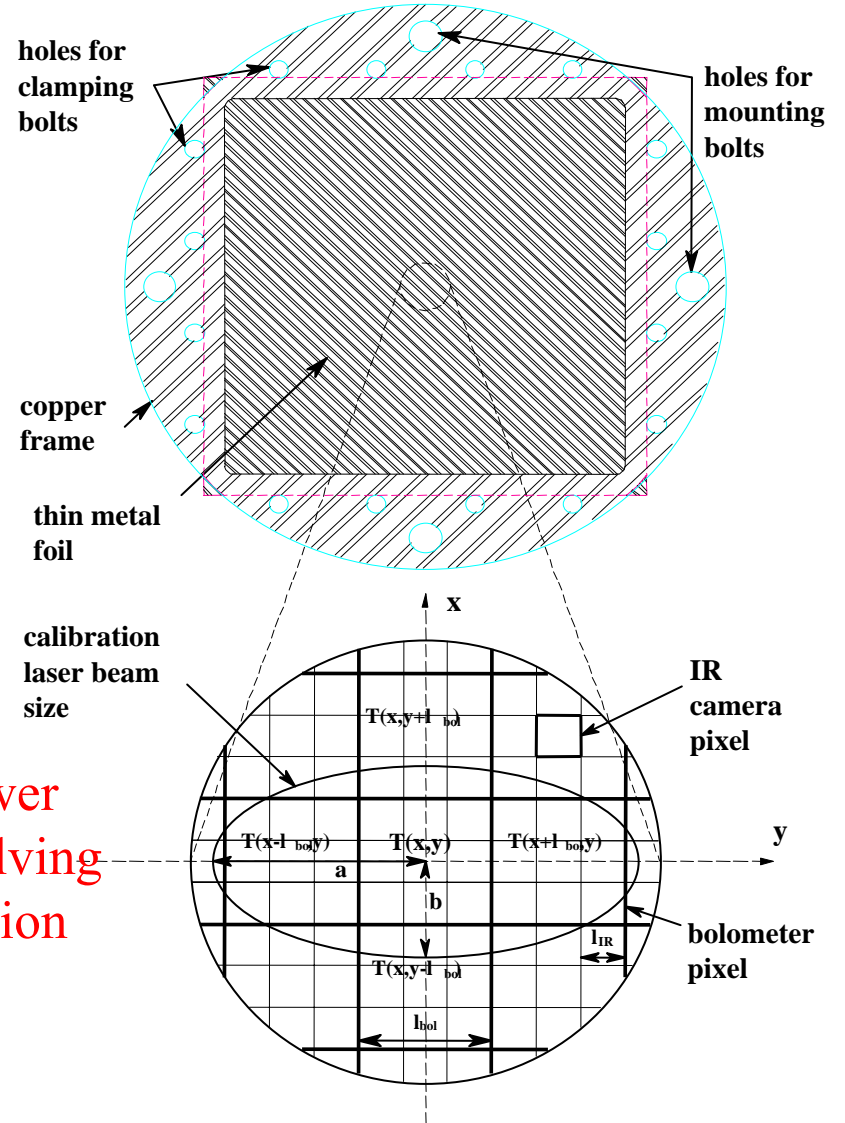
plasma radiated power is determined by solving heat diffusion equation

foil thermal conductivity

foil thickness

bolometer pixel area

IRVB Foil and Frame





JT-60U IRVB Data Analysis



B.J. Peterson et al., IEEE Trans. Plasma Sci. **30** (2002) 52-53.

IR Camera data
111 x 141 pixels

Resampled data
14 x 18 pixels

Derivatives

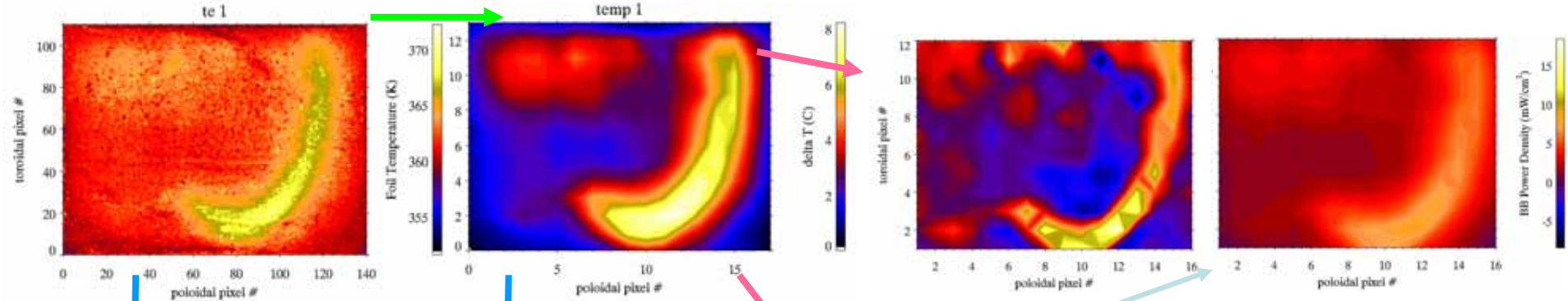
Radiation

(12 x 16 pixels, mW/cm²)

(a) $T(x,y,t-\Delta t)$ (K)

(c) $\Delta T(x,y,t-\Delta t)$ (K)

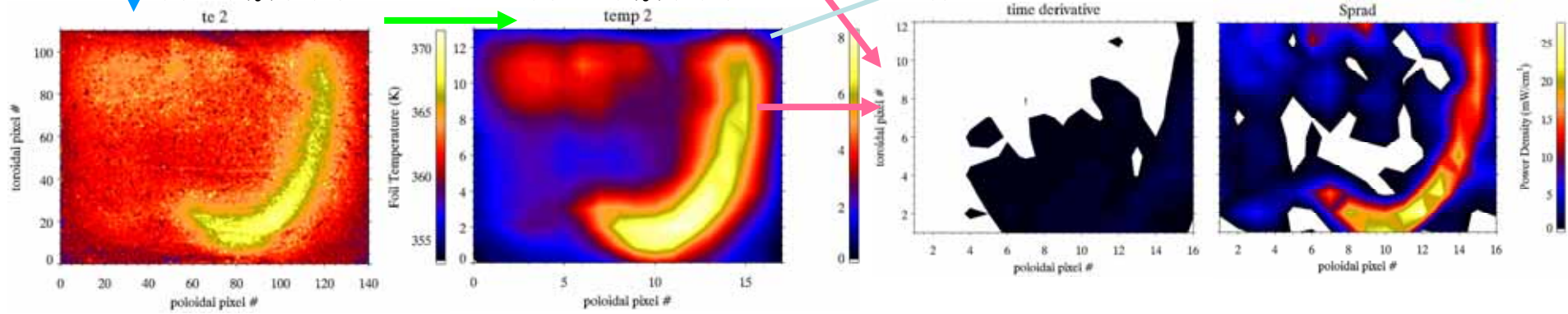
(e) Laplacian term + (g) Black Body term



Δt
(b) $T(x,y,t)$ (K)

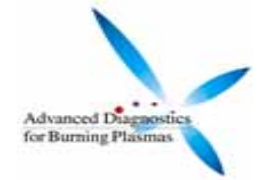
Δt
(d) $\Delta T(x,y,t)$ (K)

+ (f) dT/dt term = (h) Plasma Radiation





IRVB Sensitivity and Foil Material Selection



Noise equivalent power [1]:

small

small

$$\eta_{IB} = \frac{\sqrt{10kt_f \sigma_{IR}}}{\sqrt{mN}} \sqrt{1 + \frac{l^4}{5\kappa^2 m^2 \Delta t_{IR}^2} + \frac{4l^4 \epsilon^2 \sigma_{S-B}^2 T^6}{5k^2 t_f^2}}$$

IR camera frame interval

of frames averaged

IR camera sensitivity

of IR pixels / bolometer pixel

Simplifying:

$$\eta_{IB} \cong \frac{\sqrt{2kt_f \sigma_{IR} l^2}}{\Delta t_{IR} \kappa \sqrt{m^3 N}} \propto kt_f / \kappa \propto 1 / \text{bolometer sensitivity}$$

bolometer pixel area

foil thermal conductivity, thickness, thermal diffusivity

Considerations in foil material selection:

- **sensitivity** $\propto \kappa/k$
- **max. photon energy** (for 10 μm foil **< 8 keV, 8-13 keV, <17 keV**) [2]
- **melting temperature**
- **commercial availability** (min thickness of 10cm x 10 cm foil) [3]
- **neutron - proof?** (transmutation of Au to Hg)
- **outgassing?, cost?, others?**

(a) metal	(b) κ/k (cm ³ C/J)	(c) Eph (keV)	(d) T _m (C)	(e) t _{min} (μm)
Sn	0.65	10.0	232	6
Pb	0.56	19.6	327	4
Mg	0.56	1.2	649	10
Zr	0.55	7.6	1852	3
Hf	0.52	18.4	2227	9
Cd	0.50	10.2	321	5
Mo	0.45	9.4	2617	4
Ta	0.43	20.1	2996	2
Nb	0.43	8.6	2468	2.5
Al	0.41	3.9	660	0.8
Au	0.40	23.2	1064	1
W	0.40	21.4	3410	10
Ag	0.40	10.7	962	2
Ti	0.36	7.8	1660	4
Zn	0.36	12.3	419	2.5
Pt	0.35	23.9	1772	2
Pd	0.34	11.0	1554	4
V	0.34	9.1	1890	5
Cu	0.29	6.0	1083	2
SS304	0.27	4.4	1400	8
Ni	0.25	12.6	1453	2
Co	0.25	12.0	1495	3

[1] B.J. Peterson *et al.*, *Rev. Sci. Instrum.* **74** (2003) 2040.

[2] www-cxro.lbl.gov/optical_constants/atten2.html

[3] www.goodfellow.com; www.nilaco.jp



Ta and W are stronger and have smaller neutron x-section than Au or Pt

- Strength and thickness reduces motion of the foil
- Low $\sigma_{neutron}$ reduces nuclear heating

Foil Material Properties

	Tensile strength (MPa)	$\sigma_{neutron}$ (Barns)	k (W/m K) @0-100C	κ/k (cm ³ K/J)	T_m (C)	E_{ph} (keV) @10 μ m	t_{min} (μ m)
Hf	745	103	23.0	0.52	2227	18.4	9
Ta	760	22	57.5	0.43	2996	20.1	2
Au	220	98.8	318	0.40	1064	23.2	2.5
W	1920	18.5	173	0.39	3410	21.4	10
Pt	200-300	9.0	71.6	0.35	1772	23.9	2

E_{ph} courtesy Lawrence Berkeley Laboratory: http://www-cxro.lbl.gov/optical_constants/atten2.html
material properties from www.goodfellow.com

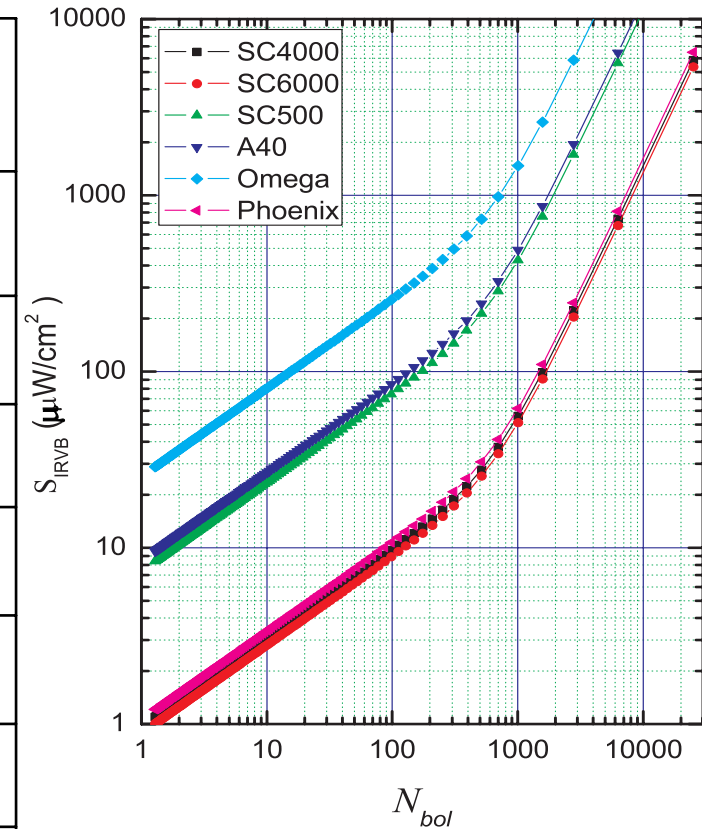


IRVB sensitivity improves with IR camera performance



$$S_{IRVB} = \frac{\eta_{IRVB} N_{bol}}{A_f} = \frac{\sqrt{10kt_f} \sigma_{IR}}{\sqrt{f_{IR} N_{IR}}} \sqrt{\frac{N_{bol}^3 f_{bol}}{A_f^2} + \frac{N_{bol} f_{bol}^3}{5k^2}}$$

Maker/ IR Camera	FLIR/ Omega (2)	FLIR/ SC500 (2)	FLIR/ A40-M	FLIR/ Phoenix (2)	FLIR/ SC4000	FLIR/ SC6000
λ (μm)	7.5-13.5	7.5-13	7.5-13	3-5	3-5	3-5
σ_{IR} ($\mu W/cm^2$) @ 30	0.1	0.1	0.08	0.025	0.025	0.025
type	μ bolo	μ bolo	μ bolo	InSb	InSb	InSb
cooling style	none	none	none	Stirling	Stirling	Stirling
N_{IR}	160x 120	320x 240	320x 240	320x 256	320x 256	640x 512
f_{IR} (Hz)	30	60	60	345	420	125
$*S_{IRVB}$ ($\mu W/cm^2$)	441	156	125	16	14	13



for Au IRVB foil with $A_f=60.75$ cm^2 , $t_f=4\mu m$, $f_{bol}=30/s$

* for IRVB with 16 x 12 ch, 30 Hz, $l = .5625$ cm, Au, $t_f = 4$ microns



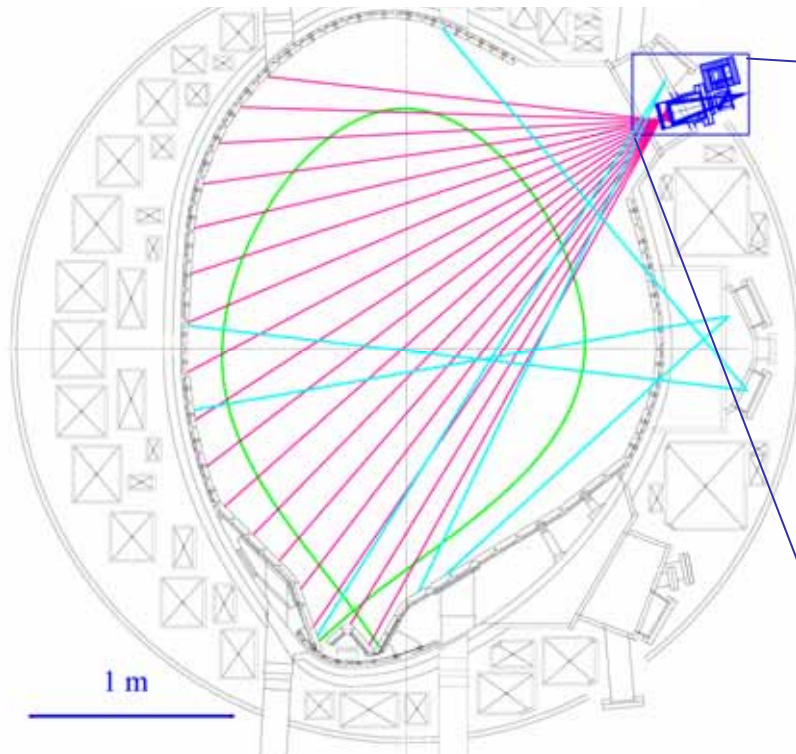
Imaging Bolometer for JT-60U



Design:

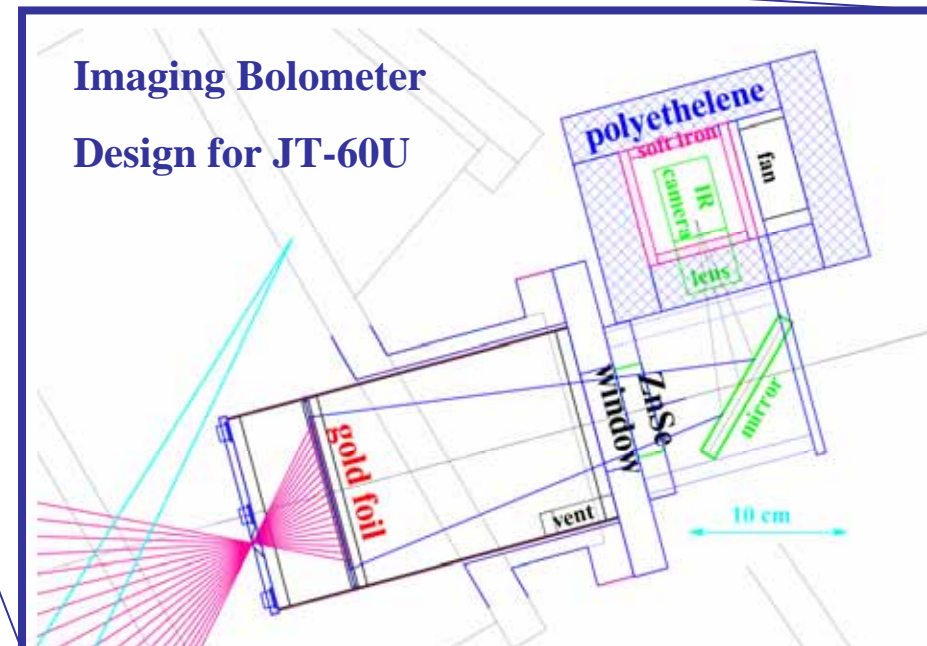
- IR camera: Indigo/Omega 67 mK, 30 Hz, 160 x 128 pixels, 14 bit
- Foil: Au, 0.0025 x 70 x 90 mm, $E_{ph} < 8$ keV
- Bolometer: 33 ms, 12(tor) x 16 (pol) = 192 ch
NEPD $> 350 \mu\text{W}/\text{cm}^2$, S/N < 100 , $\Delta x = 15$ cm

Cross-section of JT-60U



History:

- Foil installation 8/2003, operational 9/2004
- Shielding and data acq. upgrade 9/2005
- Analysis for brightness image 2/2006
- CT reconstruction of 2D profile 11/2006
- First imaging bolometer test in tokamak
- Foil durable vis-a-vis disruptions

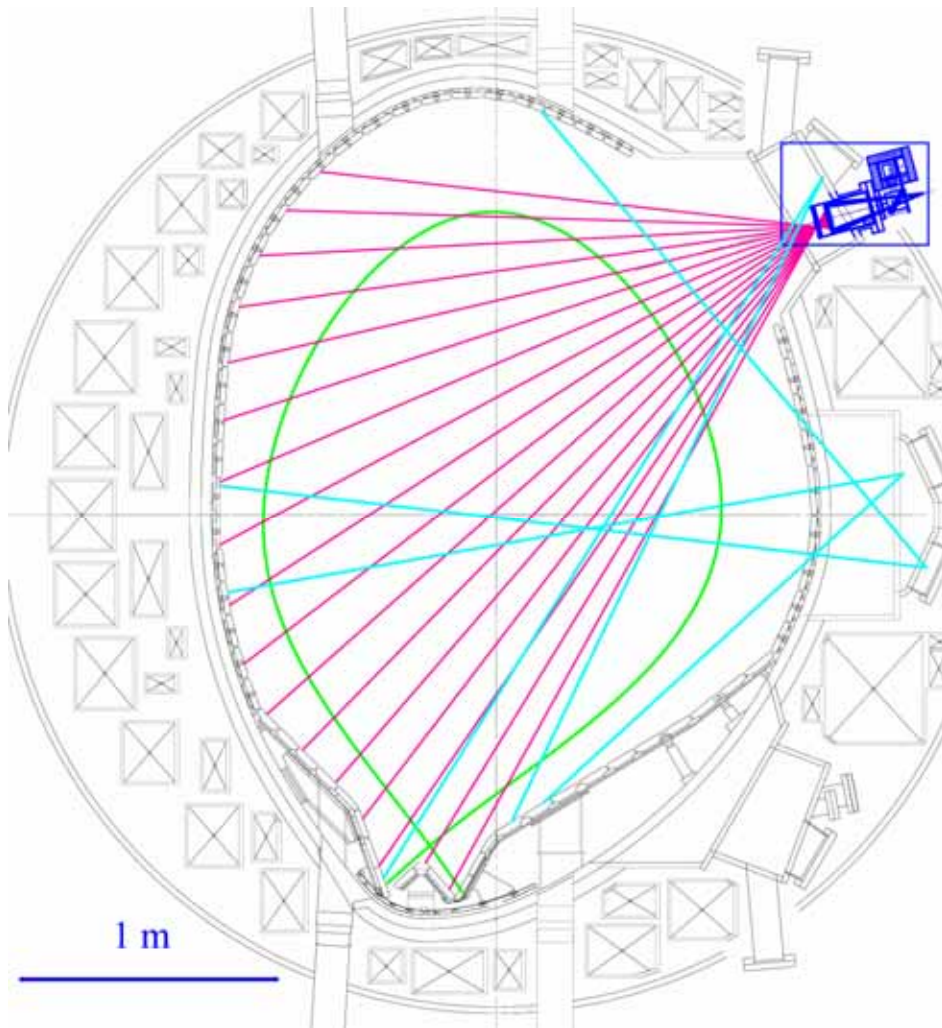




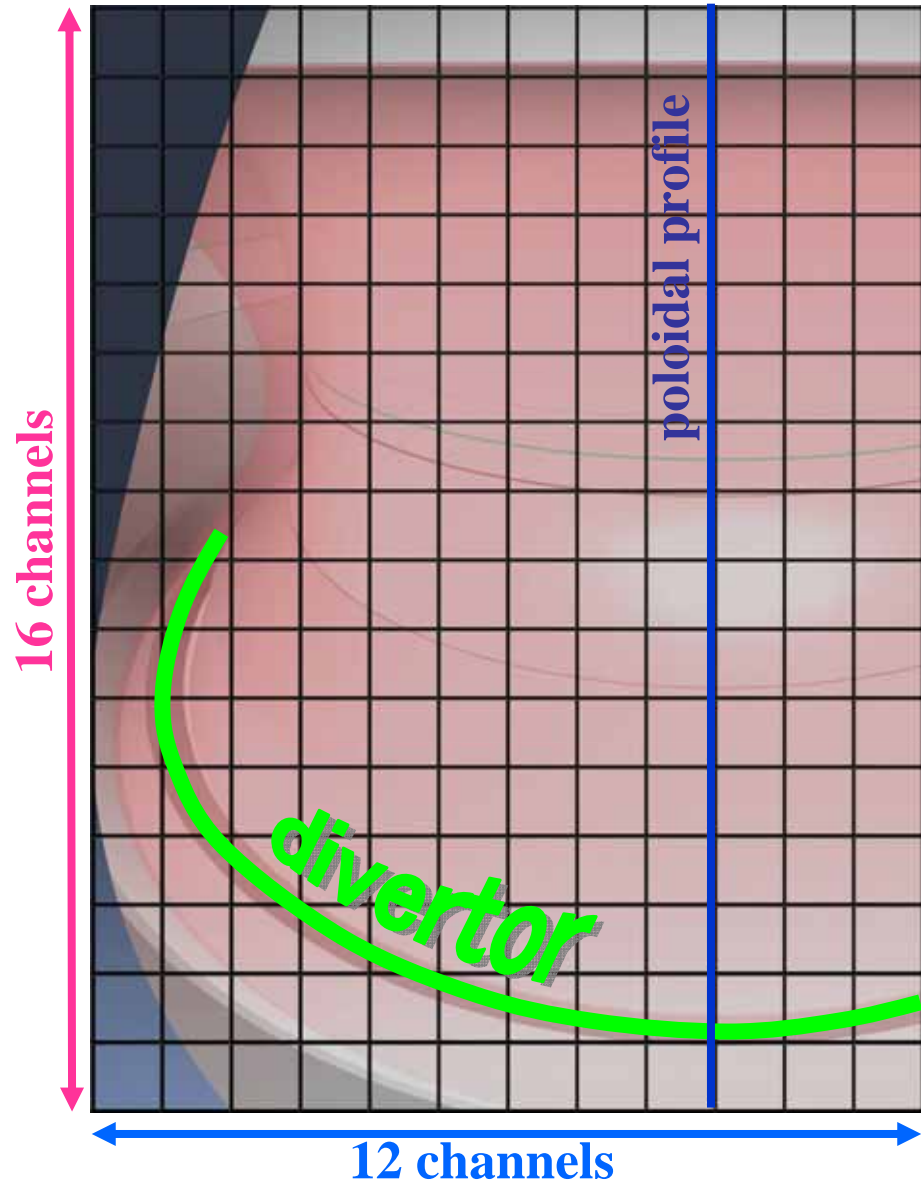
JT-60U Imaging Bolometer FOV



CAD of poloidal profile

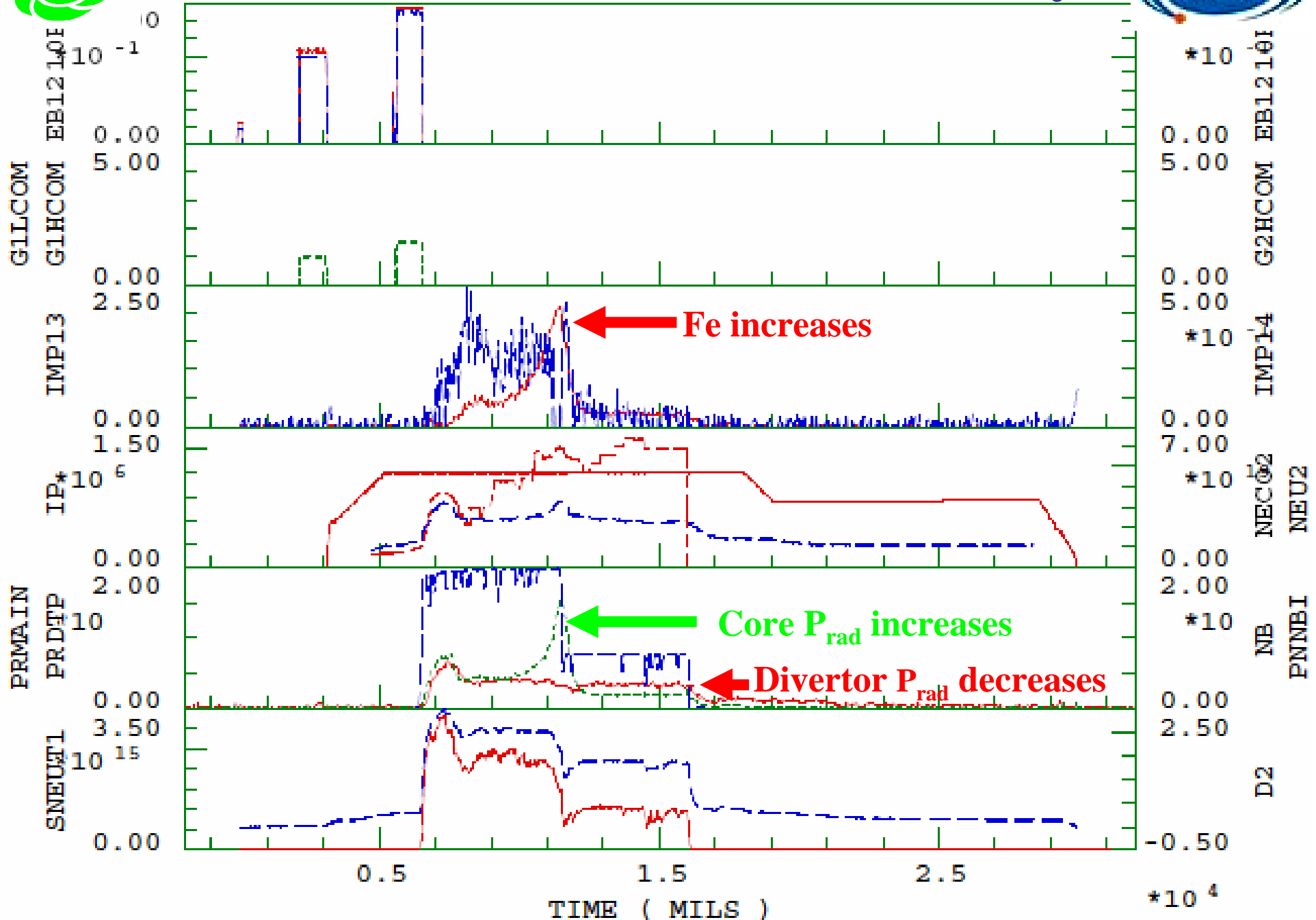


CAD of IRVB FOV



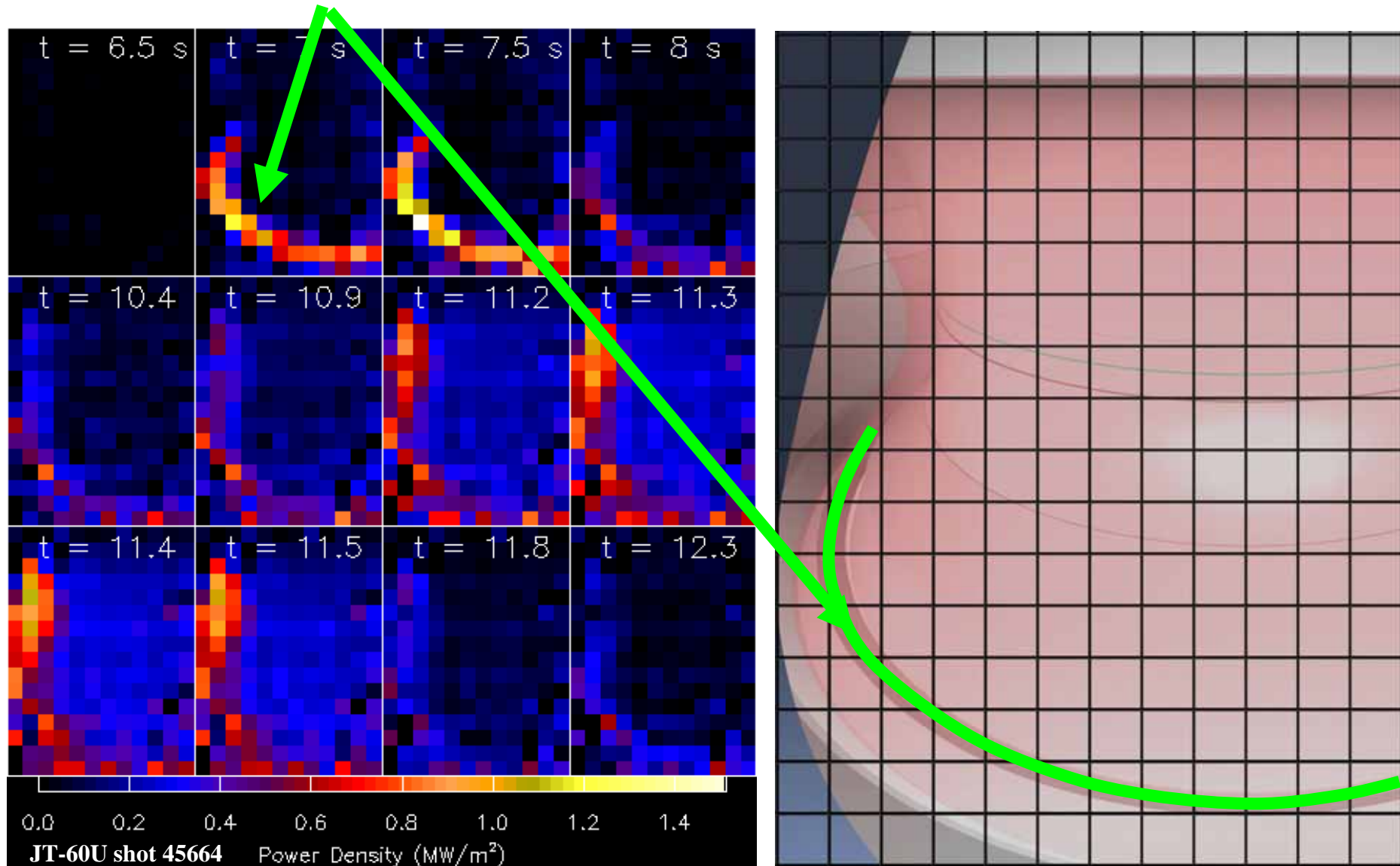


JT-60U Shot 45664 Summary



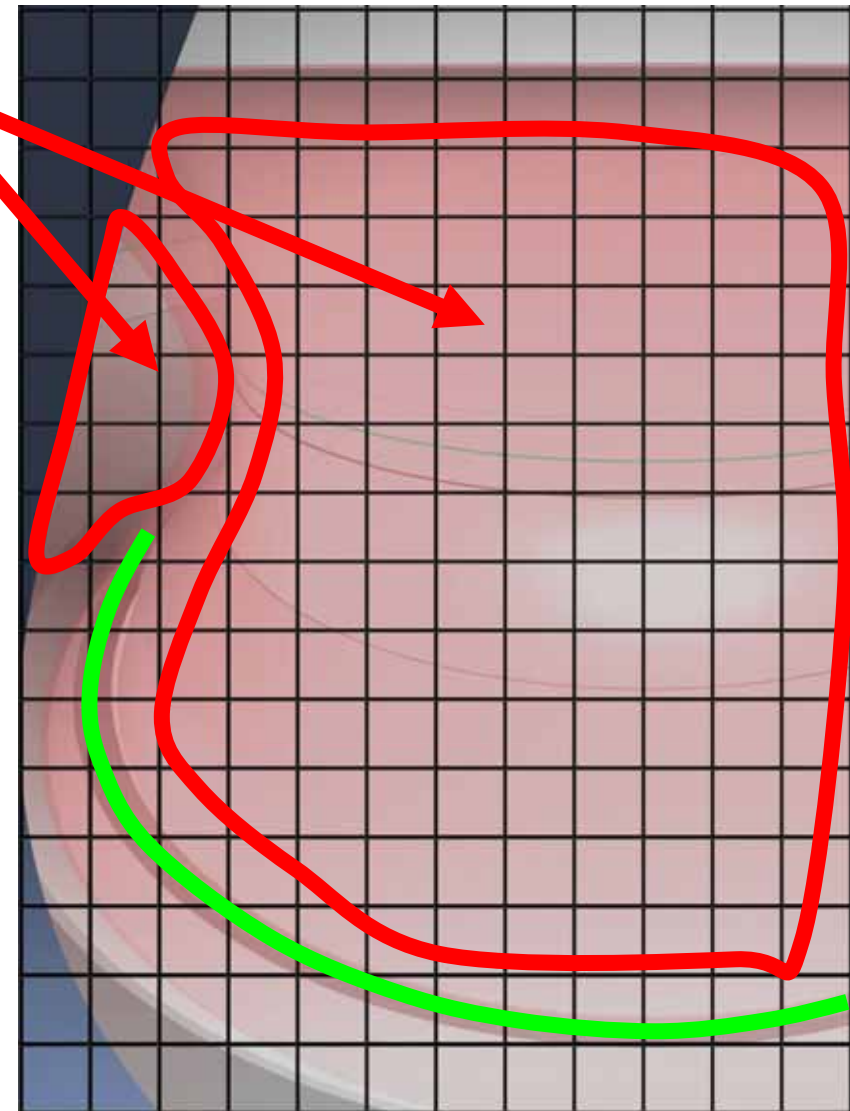
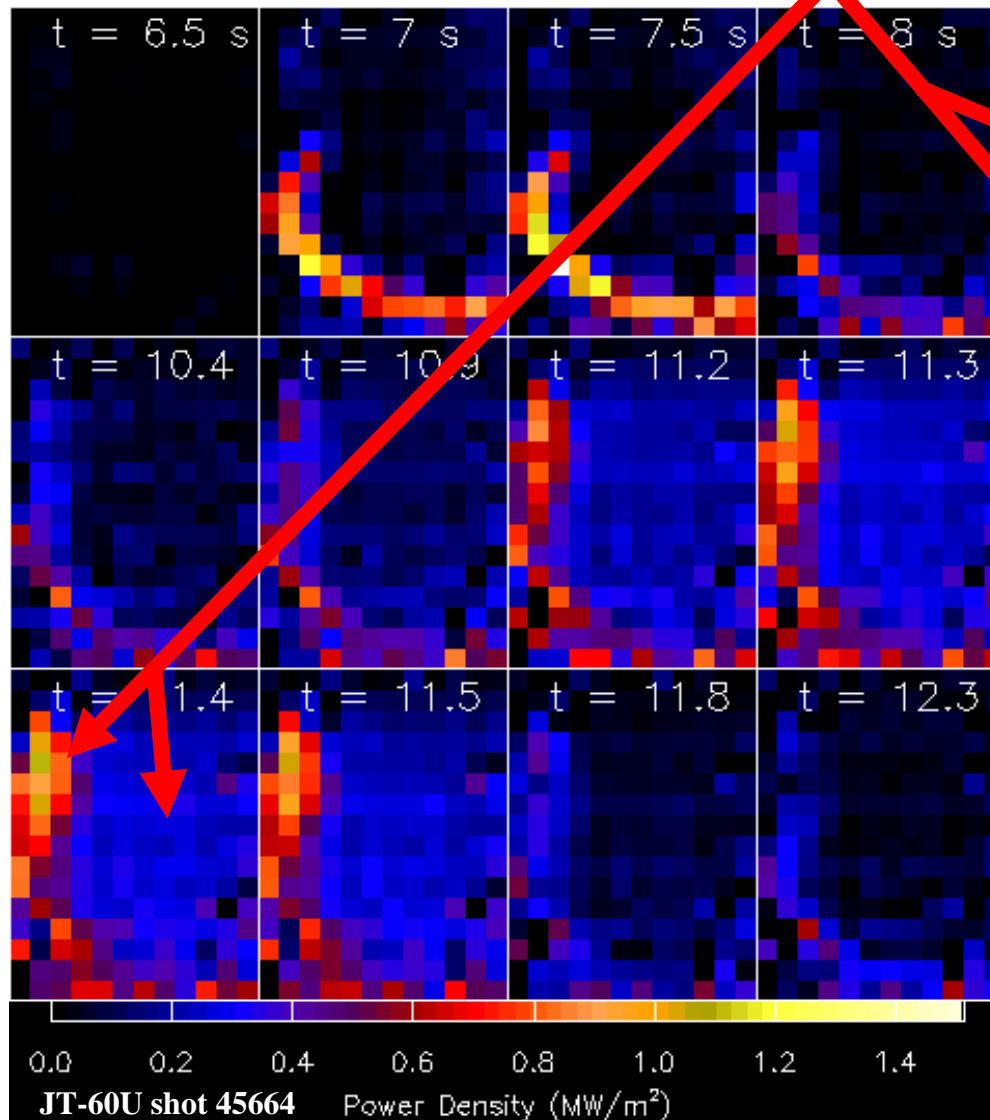


Radiation profile shifts from **divertor** to **core** with Fe influx





Radiation profile shifts from **divertor** to **core** with Fe influx



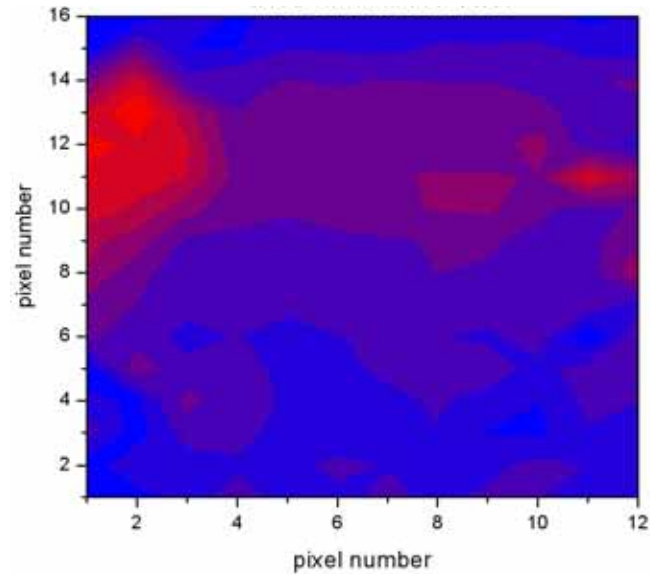
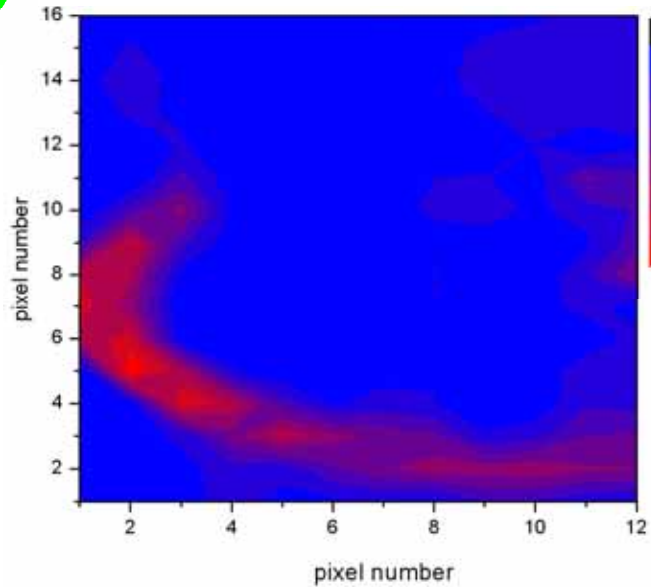
IRVB Tomography shows radiating divertor and impurity accumulation in core



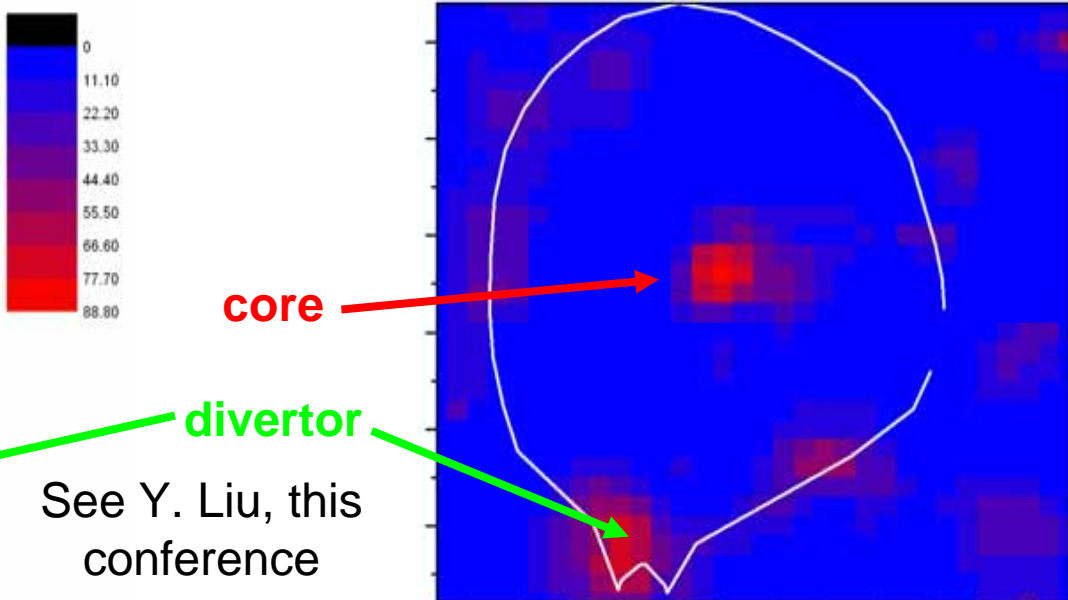
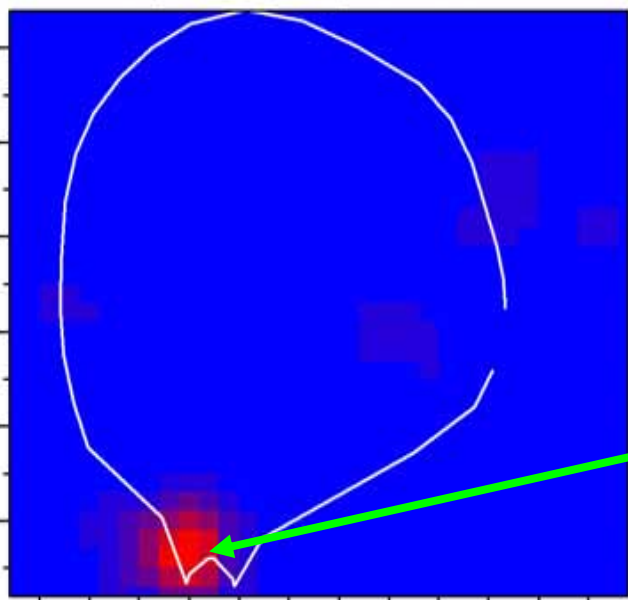
7.5 s

IRVB brightness data

11.3 s



2D tomographic inversion by minimizing chi-squared with Tikhonov-Phillips regularization



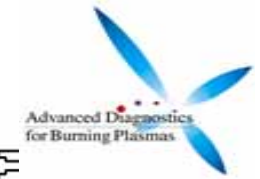
core

divertor

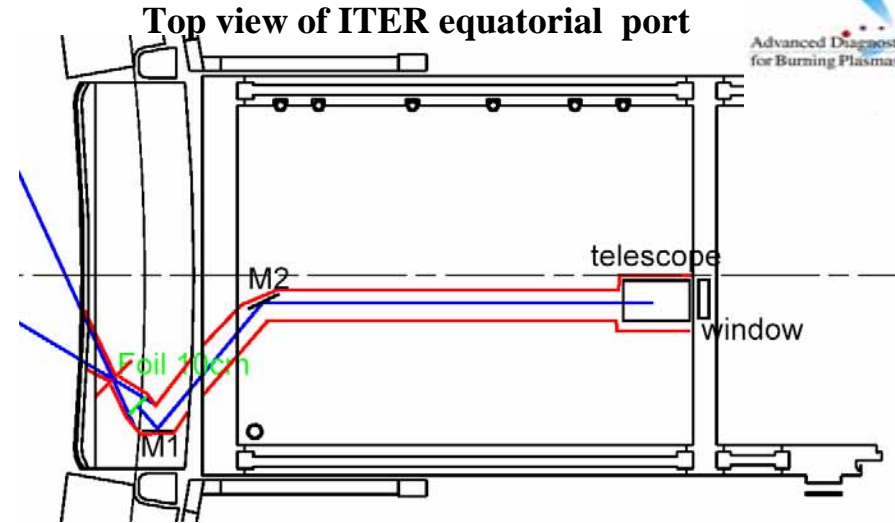
See Y. Liu, this conference



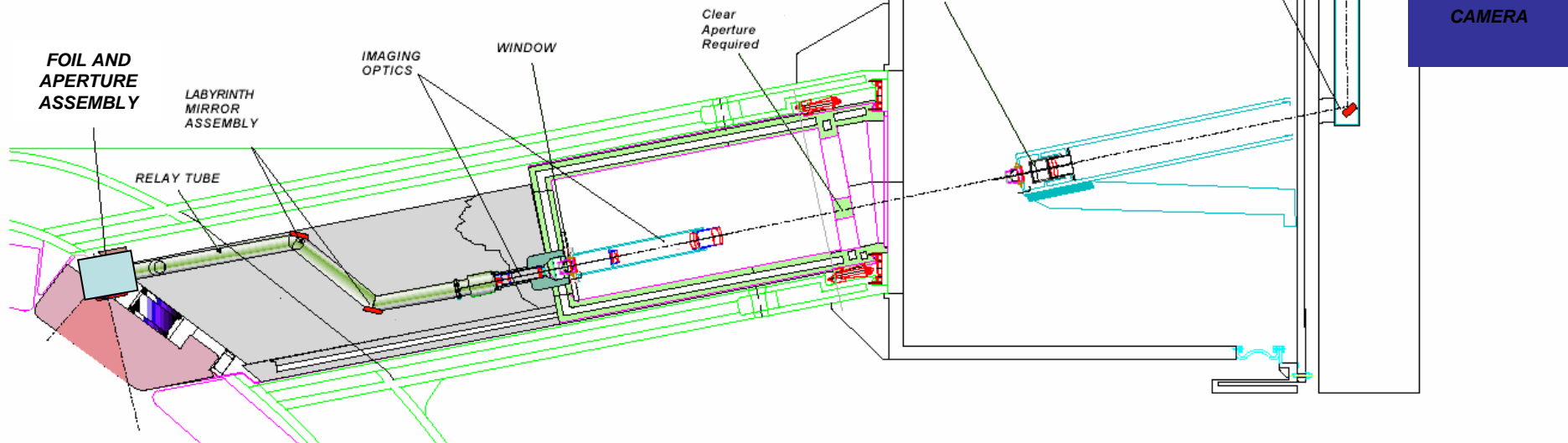
Imaging Bolometer for ITER: Installation



- Use endoscope/labyrinth similar to current IR thermography design by replacing final mirror with foil and aperture assembly
- Reflective optics near plasma, minimum 2 mirrors
- Refractive optics and IR camera beyond labyrinth for neutron shielding

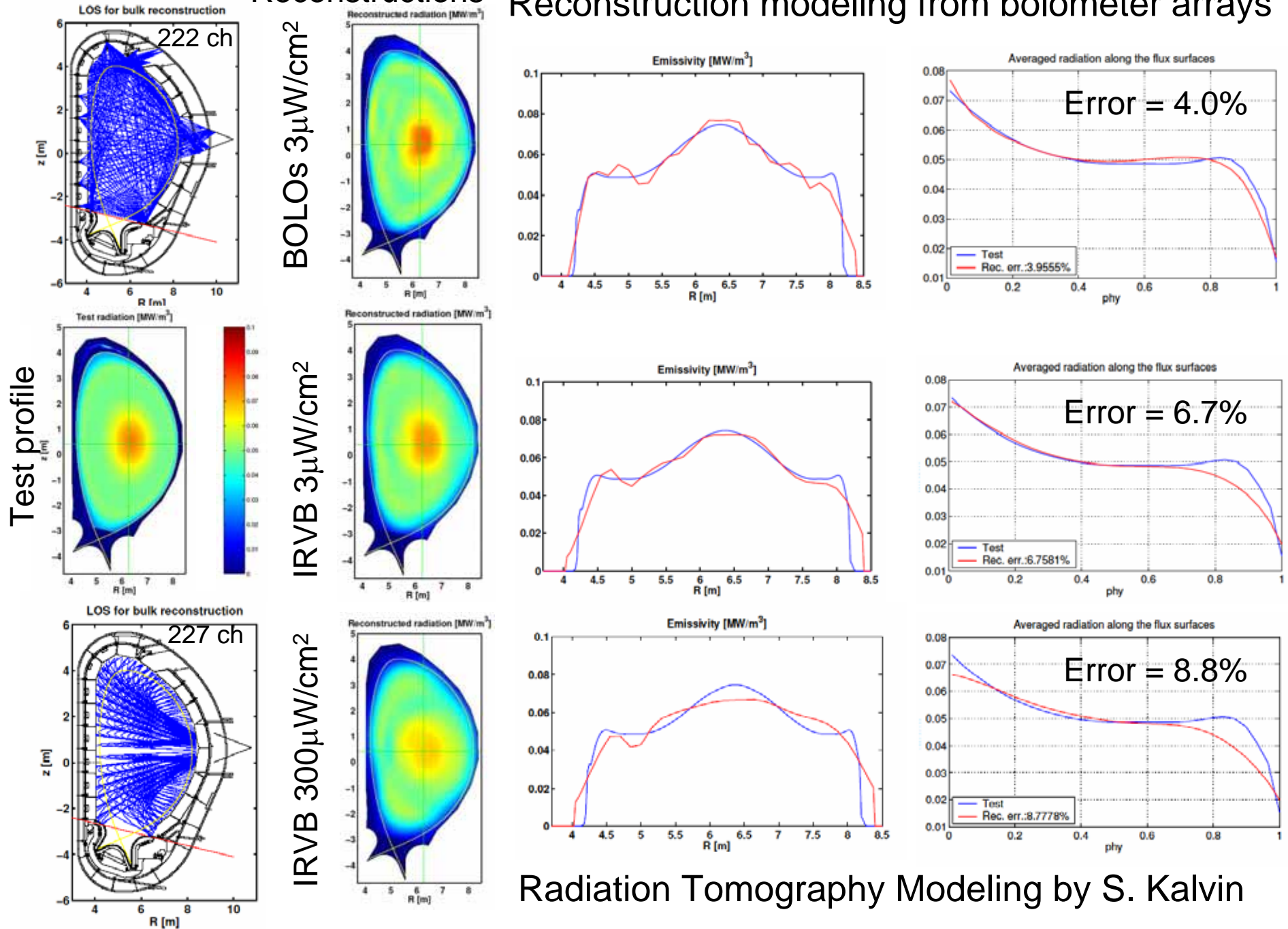


Side view of modified thermography design at ITER upper port



Reconstructions

Reconstruction modeling from bolometer arrays





JT-60U IRVB telescope Upgrade: Improving diagnostic capability



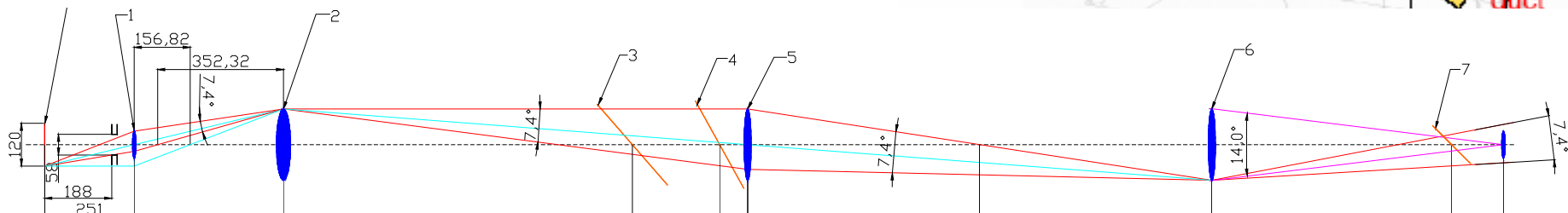
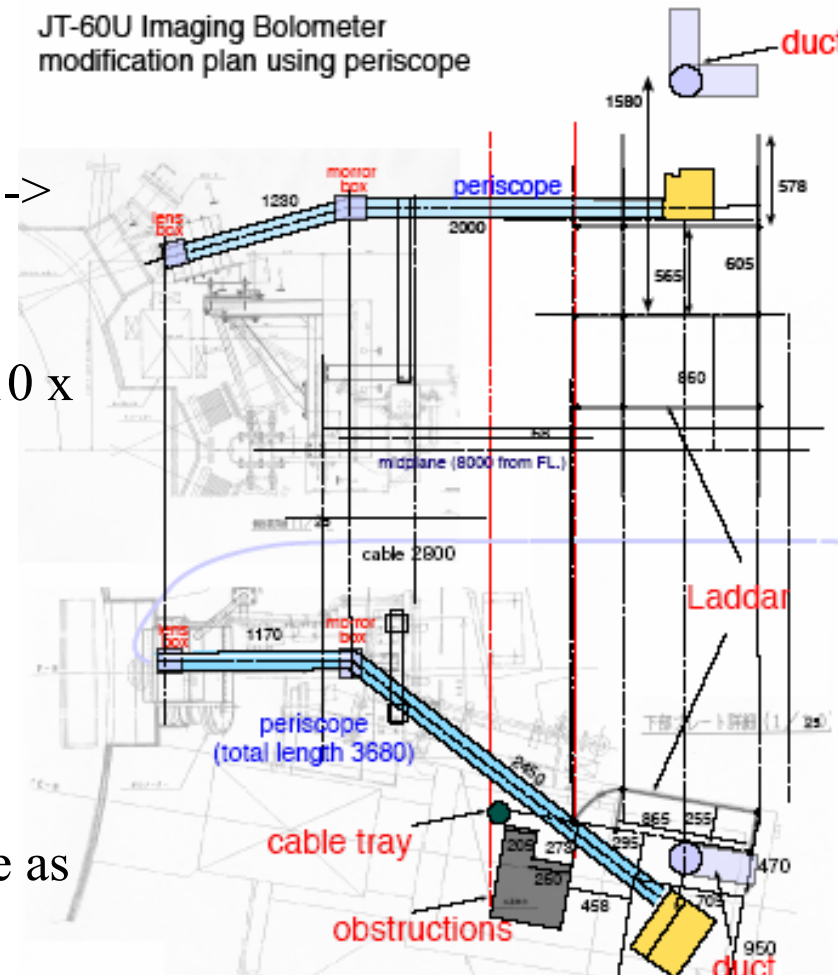
Improvement in bolometer sensitivity:

- IR camera upgrade (25 x sensitivity)
- 3.6 m telescope 42 times optical throughput ->
 - 2.5 x temperature sensitivity
- Improved shielding may decrease noise by 10 x
 - 1.8 x temperature sensitivity
- Total sensitivity increase up to 110 x

Improvement in diagnostic capability:

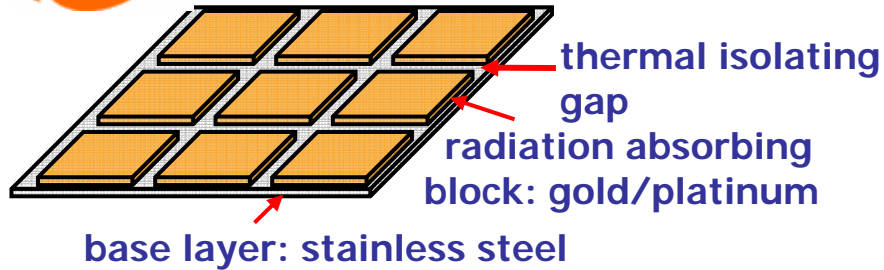
- 12 x 16 pixels -> 24 x 80 pixels
 - divertor resolution 15 cm -> 3 cm (same as resistive bolometers)

JT-60U Imaging Bolometer modification plan using periscope

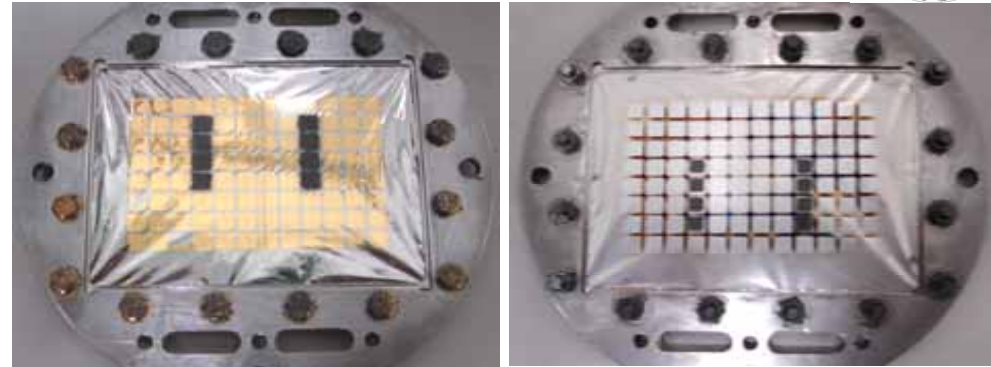




R&D of sensitive double layer foil

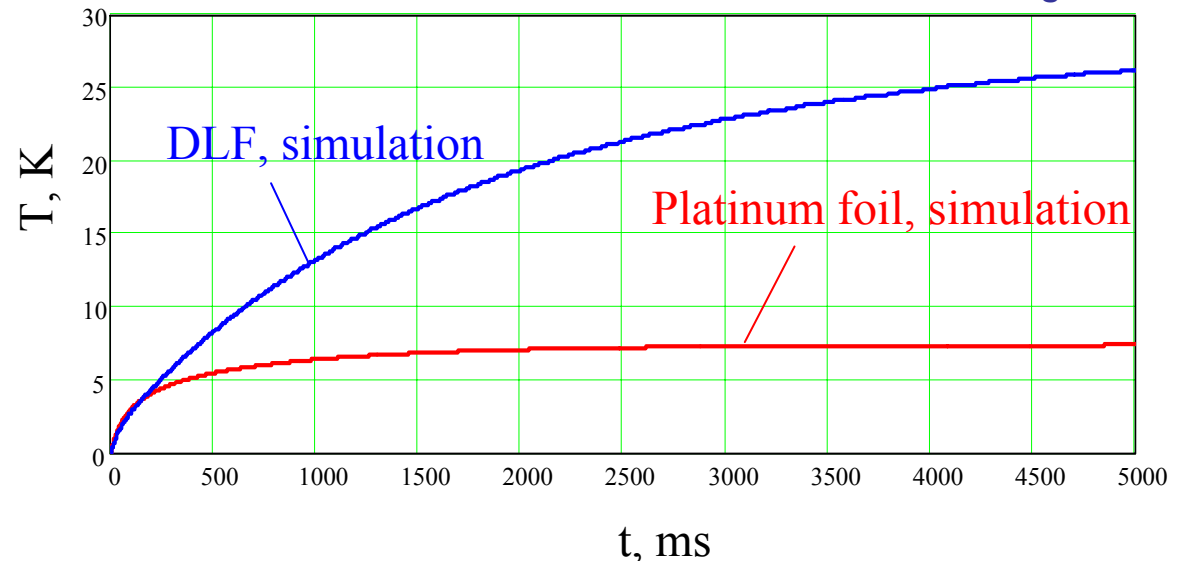
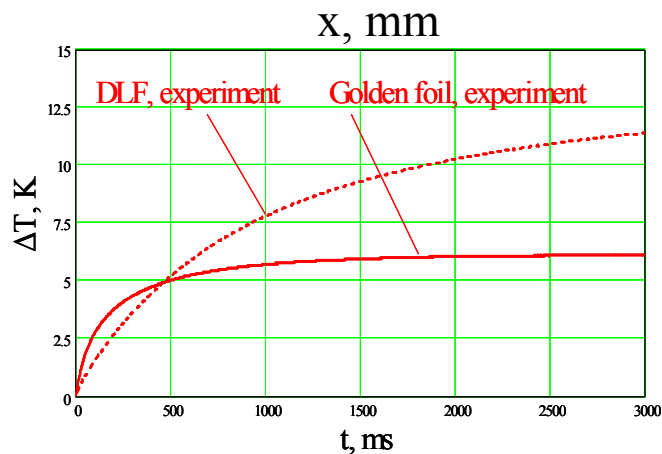
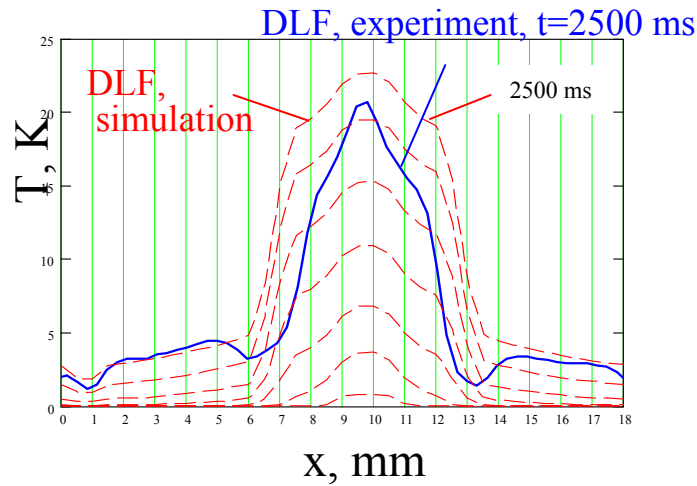


Double Layer Foil (DLF) prototype



Front
 (radiation absorbing) side
 Gold: $2.1 / 0.85 \pm 0.1 \mu\text{m}$
 Manufacturing process:
 vacuum vapor deposition

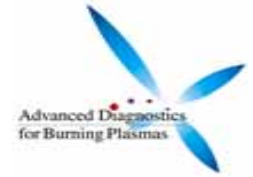
Back
 (IR camera viewed) side
 Stainless steel $2.5 \pm 0.1 \mu\text{m}$
 Manufacturing processes:
 electrochemical etching,
 ion beam etching



see I. Miroshnikov, Poster P6-11, this conference



Conclusions



- IRVB can operate in a fusion reactor environment
- A single imaging bolometer with a semi-tangential view can provide poloidal radiation profile through computed tomography
- Design similar to that for first wall thermography can be used for IRVB installation
- Single IRVB with tangential view can provide nearly the same poloidal profile information as equivalent number of resistive bolometer channels
- New double layer foil promises 3 – 10 times increase in sensitivity

Future Work

- 2-D tomography of JT-60U radiation with and without resistive bolometers
- Replace JT-60U 2.5 μm Au foil with 5 μm Ta (stronger and lower neutron x-section)
- Upgrade JT-60U IR camera (IRVB 10x faster or 25 x sensitivity or 10 x # of pixels)
- Upgrade JT-60U IR optics (ITER relevant, up to 4.5 x sensitivity)
- Improve 4 IRVBs on LHD with IR optics and camera upgrades
- 3-D tomography on LHD
- Design IRVBs for KSTAR, JT-60SA and ITER