


PE-13 16th International Toki Conference  
Advanced Imaging and Plasma Diagnostic  
Concepts Test, Gifu, JAPAN  
December 5-8, 2005

## Multi-channel microwave reflectometer with Fermi antenna receivers

Kunihiko HATTORI\*, Akira ANDO and Masaaki INUTAKE  
Department of Electrical Engineering,  
Graduate School of Engineering, Tohoku University  
Sendai 980-8579, Japan  
\*hattori@ecei.tohoku.ac.jp



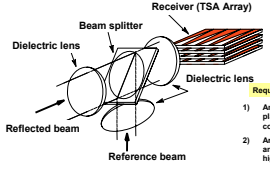
### Abstract

We have evaluated a Fermi antenna newly designed in X band for use in a multichannel reflectometer.

The advantages of the Fermi antenna are that it can be adopted as an array antenna owing to its planar shape and fabricated with a low cost due to its compactness and a light-weighted structure. The radiation-beam widths in the E- and H-plane are almost equal to each other and the side-lobe levels are low.

Plasma behaviors in the HITOP device are measured by reflectometry using two Fermi antenna receivers. Time evolution of the cutoff layer and plasma rotation velocity measured by the reflectometer are in good agreement with an electrostatic probe measurement.

### Schematic of Imaging System

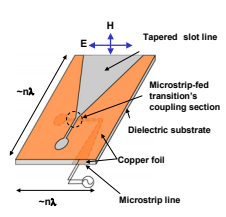


**Required characteristics of the receiver**

- 1) An axially symmetric E-plane and H-plane pattern to achieve the optimum coupling with a dielectric lens.
- 2) Arrangement of a large number of antennas in a limited area to obtain a high resolution of imaging.

1. The reflected beam and the reference beam are superimposed coaxially by a beam splitter using quasi-optical system, and are focused on a TSA array.
2. The phase shift is detected using a heterodyne method.

### Schematic of Tapered Slot Antenna (TSA)

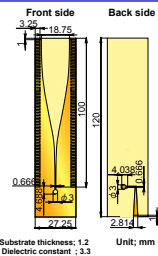


**Characteristics of TSA**

- Small size
- Simple structure
- Easy to make
- Easy to be arrayed
- Low cost
- Broad bandwidth
- High Gain
- Low crosstalk

(Linearly type tapered slot antenna: LTSA)

### Designed Fermi antenna with corrugated structure



**Characteristics of Fermi antenna**

1. Shape of the tapered section

Fermi-Dirac function  
 $f(x) = \frac{1}{1 + \exp(b(x+c))}$

Where x is a variable and a, b, and c are constants

↓  
lower side lobe

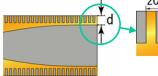
2. With corrugated structure around the edge.

↓  
Improved beam pattern

**References**

[1] S. Sugawara, et al., IEEE MTT-S International Microwave Symposium Digest, pp.959-962, Denver, USA, 1997.  
[2] S. Sugawara, et al., IEEE MTT-S International Microwave Symposium Digest, pp.533-536, Baltimore, USA, 1998.

### Designed corrugated structure

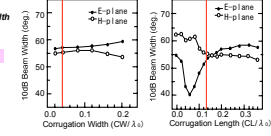


As d is shorter than  $\lambda/2$ , beam width and side lobe level increases.

**Dimensions of designed Fermi Antenna**

Antenna length:  
 $\lambda = 100\text{mm}$  (at 12GHz)

Corrugated structure:  
CW=1mm(0.04 $\lambda$ )  
CL=3.25mm(0.13 $\lambda$ )

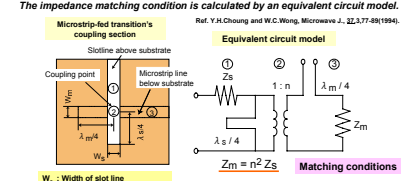


The measured 10dB beam width as a function of (a) corrugation width CW(1-0.2 to 0.4 $\lambda$ ) and (b) corrugation length CL(0.04 to 0.4 $\lambda$ ). (Ref. S. Sugawara, et al., IEEE MTT-S International Microwave Symposium Digest, pp.533-536, Baltimore, USA, 1998.)

### Electromagnetic Coupling Section of TSA (1)

The impedance matching condition is calculated by an equivalent circuit model.

Ref. Y.H. Choung and W.C. Wong, Microwave J., 32, 77-89(1994).

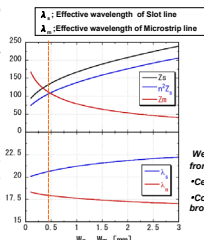


**Matching conditions**

$Z_m = n^2 Z_s$

where  
 $n = \cos(2\pi t / \lambda_0) - \cos(q) \sin(2\pi t / \lambda_0)$   
 $q = 2\pi t (\lambda_0 / \lambda_s) + \tan^{-1}(u/v)$   
 $u = \sqrt{\epsilon_r - (\lambda_0 / \lambda_s)^2}$ ,  $v = \sqrt{(\lambda_0 / \lambda_s)^2 - 1}$

### Electromagnetic Coupling Section of TSA (2)



$\lambda_s$ : Effective wavelength of Slot line  
 $\lambda_m$ : Effective wavelength of Microstrip line

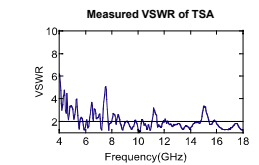
$\lambda_m / 4$  (4.49)  
 $\lambda_s / 4$  (5.17)

Dimension drawing of microstrip-fed transition (unit: mm)

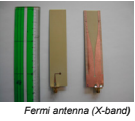
We designed microstrip-fed's coupling section from these calculation result.

- Center frequency  $f_c$ : 12GHz
- Coupling section with circular stub has a broadband frequency characteristic experimentally.

### Measured VSWR(Voltage Standing Wave Ratio) of TSA

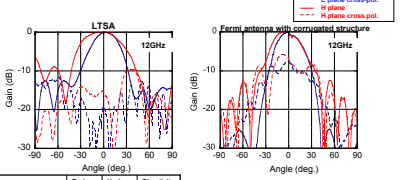


By optimizing the strip-line dimensions, the bandwidth of 8-18GHz with VSWR < 2 is obtained.



Fermi antenna (X-band)

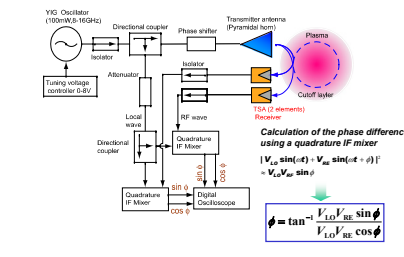
### Measured Radiation Patterns of TSA



This radiation pattern is an axially symmetric E-plane and H-plane. Compared with LTSA, directivity of the Fermi antenna is improved about 2dB, and side lobe level is lower.

	E-plane	H-plane	Directivity [dB above isotropic]
LTSA	32°	32°	19dB
Fermi antenna with corrugated structure	32°	33°	19dB

### Microwave Reflectometer System



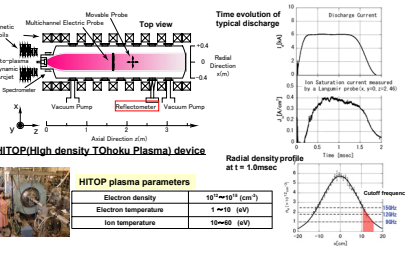
**Calculation of the phase difference using a quadrature IF mixer**

$$|V_{\text{in}} \sin(\omega t) - V_{\text{in}} \sin(\omega t - \phi)|^2$$

$$= V_{\text{in}}^2 V_{\text{in}} \sin \phi$$

$$\phi = \tan^{-1} \frac{V_{LO}/V_{RF} \sin \phi}{V_{LO}/V_{RF} \cos \phi}$$

### HITOP Plasma



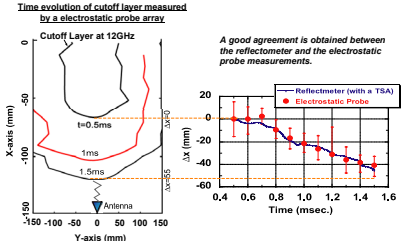
**HITOP (High density Tohoku Plasma) device**

**HITOP plasma parameters**

Electron density	$10^{20} \sim 10^{21} \text{ cm}^{-3}$
Electron temperature	1-5 eV
Ion temperature	10-50 eV

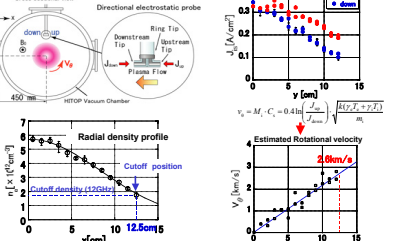
### Comparison of Electrostatic Probe and Reflectometer

#### Time evolution of cutoff layer measured by an electrostatic probe array



A good agreement is obtained between the reflectometer and the electrostatic probe measurements.

### Plasma rotation measurement with directional Probe



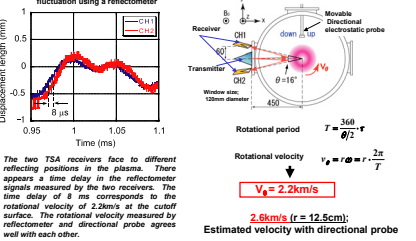
**Estimated Rotational velocity**

$V_{\theta} = 2.6 \text{ km/s}$

**Estimated velocity with directional probe**

$V_{\theta} = 2.2 \text{ km/s}$

### Comparison of Electrostatic Probe and Reflectometer



The two TSA receivers face to different reflecting positions in the plasma. There appears a time delay in the reflectometer signals measured by the two receivers. The time delay of 8 ns corresponds to the rotational velocity of 2.6km/s at the cutoff surface. The rotational velocity measured by reflectometer and directional probe agrees well with each other.

**Estimated velocity with directional probe**

$V_{\theta} = 2.2 \text{ km/s}$

### Summary

1. We designed a Fermi antenna with corrugated structure for X-band, and measured fundamental characteristics of the TSA, VSWR and radiation pattern. The impedance matching condition is calculated by an equivalent circuit model. By optimizing the strip-line dimensions, the bandwidth of 8-18GHz with VSWR < 2 is obtained. The HPBW is 32 degree in the E-plane and 37 degree in the H-plane, respectively. The Directivity of Fermi antenna with corrugated structure is 2dB better than the LTSA.
2. We have measured a HITOP plasma by using the reflectometer with two Fermi antenna receivers. Time evolution of cutoff layer measured by the electrostatic probe array and the reflectometer is in good agreements. Rotational velocity of the plasma is estimated from a time delay of the reflectometer signals measured by the two antenna receivers. The obtained rotation velocity agrees well with that obtained by a Mach probe.