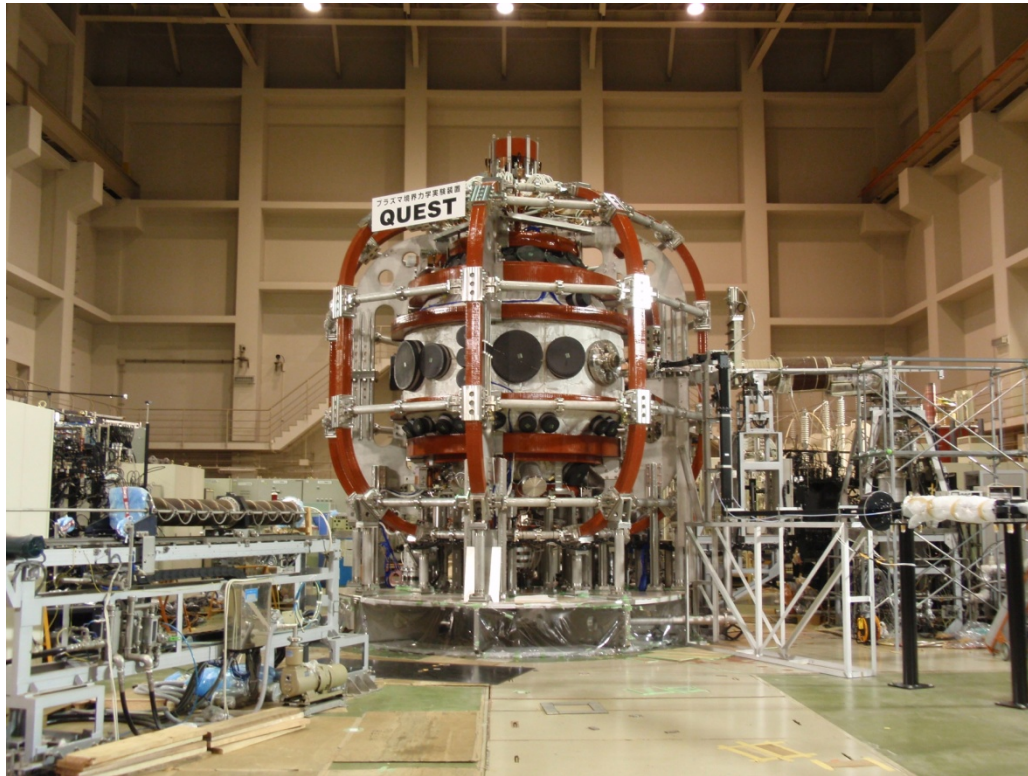


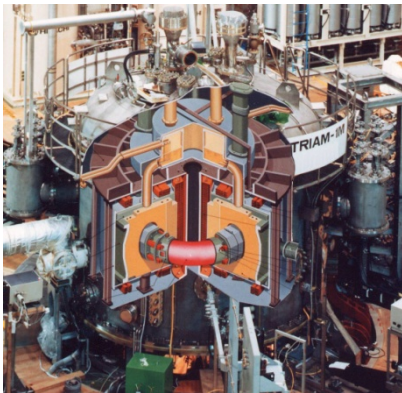
Steady-state operation scenario and the first experimental result on QUEST



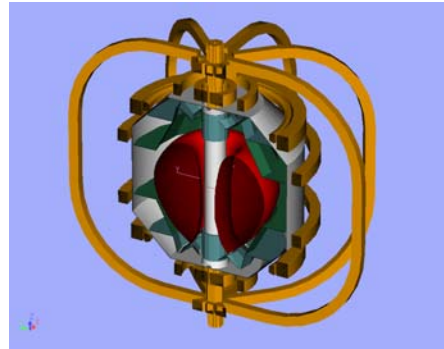
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Domestic Collaborators and Map of QUEST

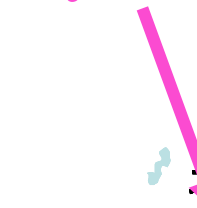
TRIAM-1M



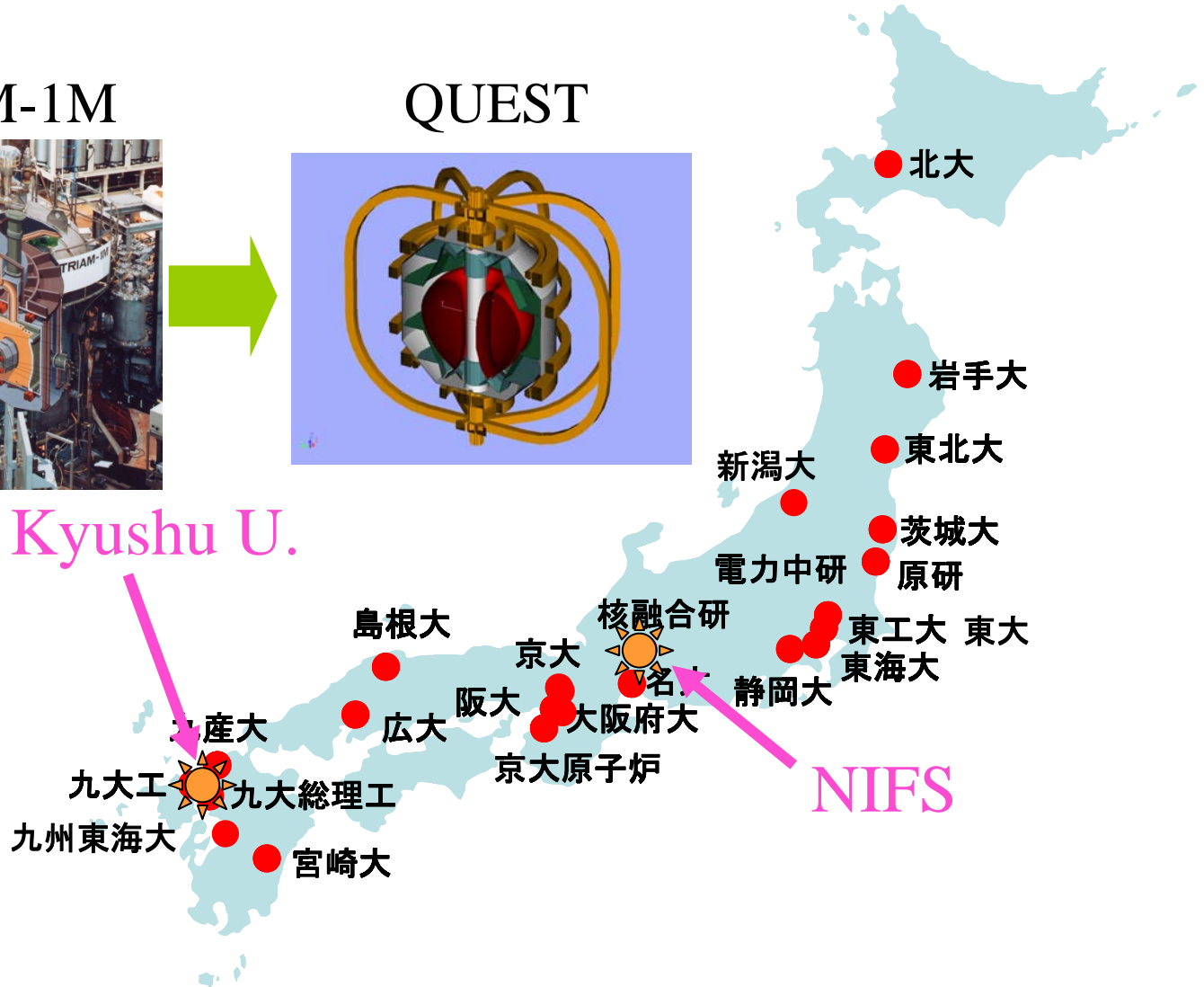
QUEST



Kyushu U.



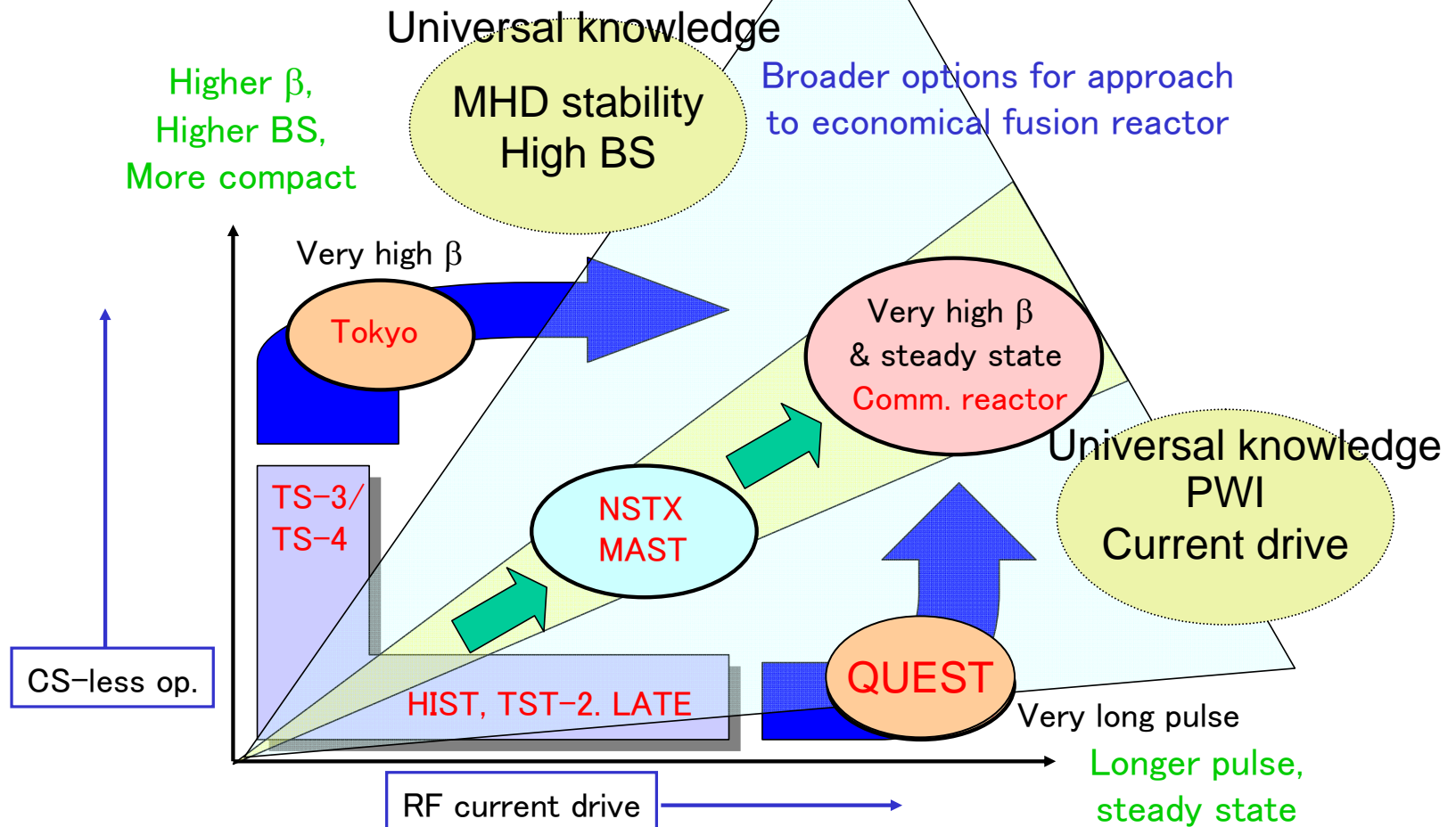
NIFS



Outline

- Purpose of QUEST project
- Plan for PWI research
- Plan for Current drive research
- Plan for Divertor research
- First experimental results

Strategy of Japanese ST Research

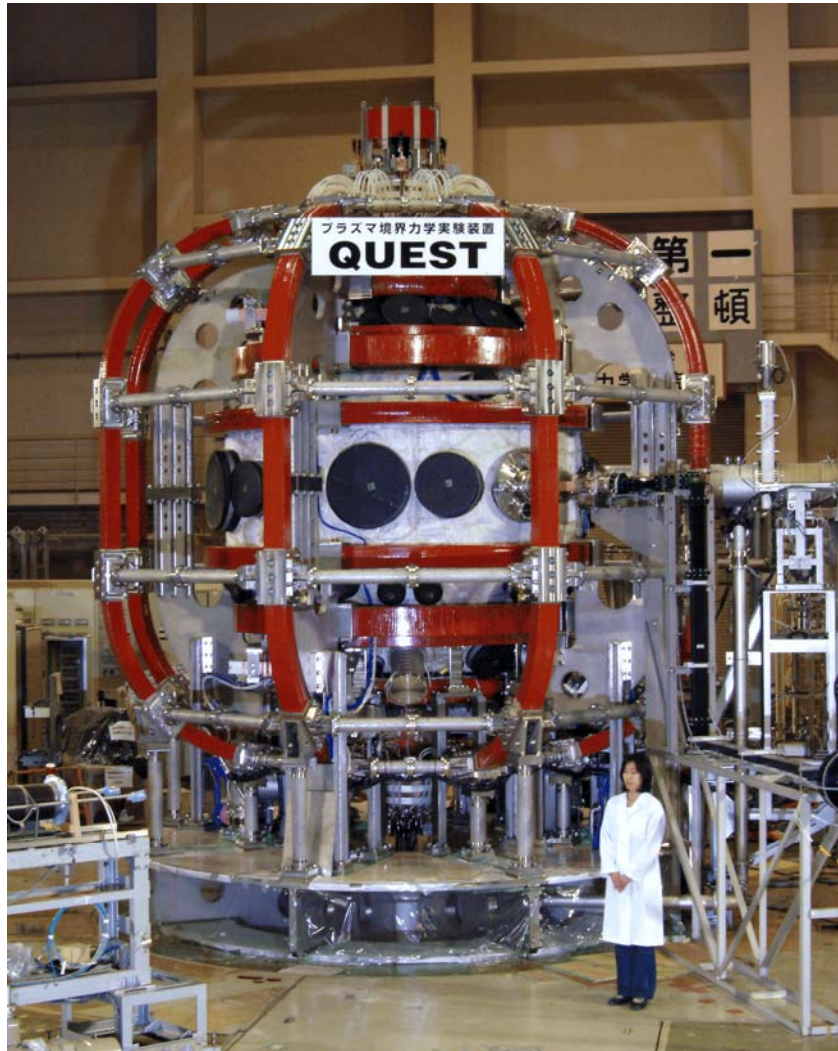


- QUEST is the main device for the research of steady state operation in this framework.

Mission of QUEST

- The mission of QUEST should be to develop the scientific basis for achieving a steady state condition at sufficiently high beta ($\sim 20\%$), with high confinement and low collisionality, in a longer term program that contains three Phases of R&D.
- The short-term goal of QUEST for **Phase I** (the first 2 years) is to establish the basis for sustained operation at low density ($\sim 4 \times 10^{18} \text{ m}^{-3}$) and low current (20-30 kA).
- In **Phase II** (5 years), progress towards higher current ($\sim 100 \text{ kA}$) in steady-state, and towards higher beta ($\sim 10\%$) in the pulsed operation will be pursued with an upgraded heating system.
- The goal of **Phase III** research is to achieve steady state operation of ST at sufficiently high beta ($\sim 20\%$).

Specification and parameters



	Phase I	Phase II		Final aim
		SSO	Pulse	
R(m)	0.68			
a(m)	0.4			
A	1.78			
Radius of VV(m)	1.4			
Height of VV(m)	2.8			
BT(T)	0.25	0.25	0.5	0.25
IP(MA)	0.02-0.03	0.1	0.3	0.5
Pinj(MW)	0.45	1	3	3
k	2.5	2.5	2.5	2.5
d	0.7	0.7	0.7	0.7
$\langle n_{e20} \rangle (m^{-3})$	-	0.04	0.3	0.3
$\langle T_e \rangle (keV)$	-	0.32	0.33	0.54
$\langle T_i \rangle (keV)$	-	0.32	0.33	0.54
$\tau_E (ms)$	-	2.5	6.8	10.8
$\beta (%)$	-	1.6	13	21
β_N	-	1.5	3.9	3.8
β_p	-	0.33	0.29	0.17
q95	-	25	8.2	5
$\Gamma_H (MW/m^2)$	-	6.5	10.1	13.6
$F_{rad} (%)$	-	20	40	40
$\Gamma_p (Pa m^3/s)$	-	17.5	50	31.1
f_{GW}	-	0.16	0.41	0.24
$I_{BS} (MA)$	-	0.008	0.022	0.021
$\eta_{CD} 10^{19} (A/W/m^2)$	-	0.026	0.19	0.32

Schedule and Research items

fiscal year	05	06	07	08	09	10	11	12	13	14	further
items											
construction											
High β						>10% (1sec)				20%	
Plasma start-up				RF+OH		RF+OH+NBI					
Current drive				RF		RF(8.2GHz)+NBI				16GHz	
PWI				W		W, high Temp. wall				Control of Recycling	
Divertor				open		closed				advanced	
fueling				Gas puff		CT injection				pellet	

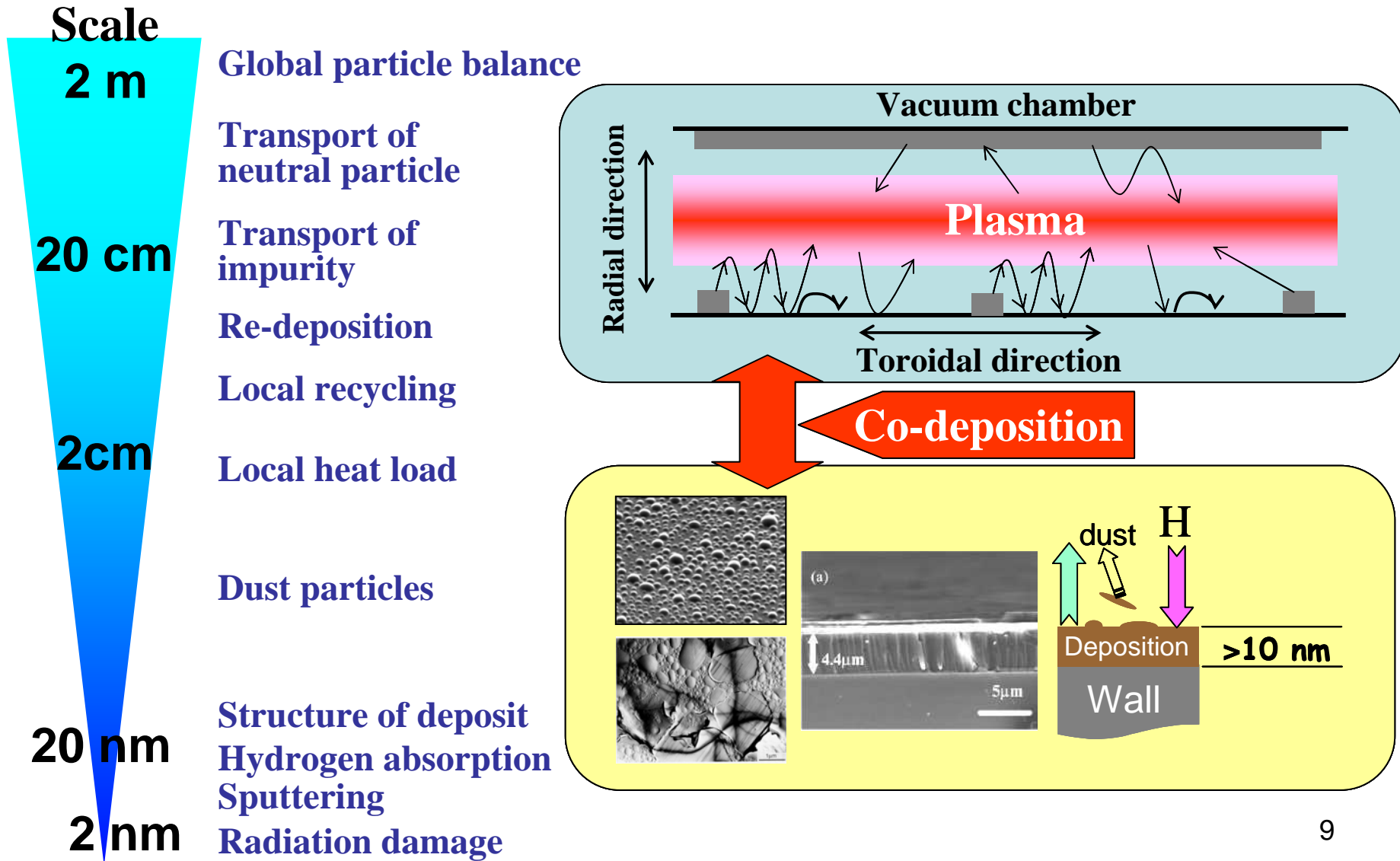

We are here.

Schedule and Research items

fiscal year	05	06	07	08	09	10	11	12	13	14	further
items											
construction											
High β						>10% (1sec)				20%	
Plasma start-up				RF+OH		RF+OH+NBI					
Current drive				RF		RF(8.2GHz)+NBI				16GHz	
PWI				W		W, high Temp. wall				Control of Recycling	
Divertor				open		closed				advanced	
fueling				Gas puff		CT injection				pellet	


We are here.

Multi-Scale of Plasma-Wall Interaction

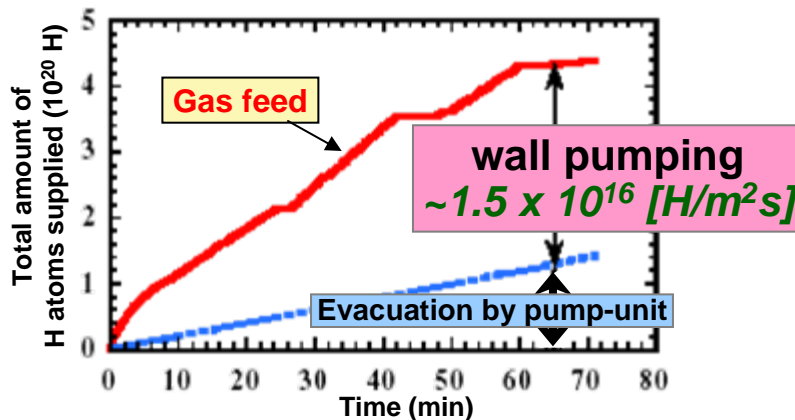


What is the main issue for steady-state ?

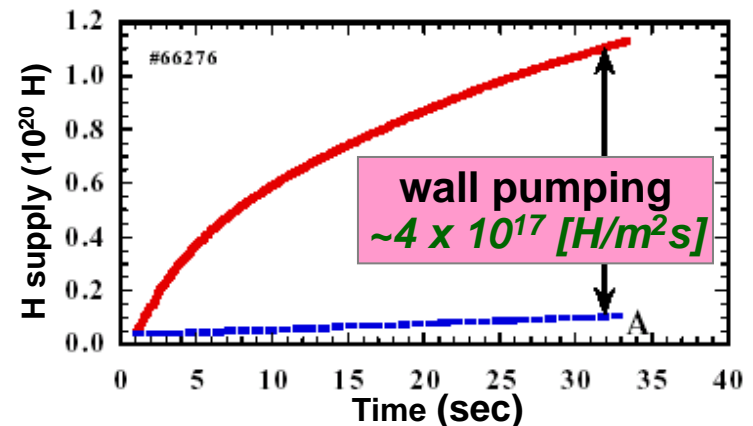
Wall pumping in long pulse operation

M. Sakamoto et al., Nucl. Fusion 42 (2002) 165

Low density ($n_e \sim 10^{18} \text{ m}^{-3}$)



High density ($n_e \sim 10^{19}$)

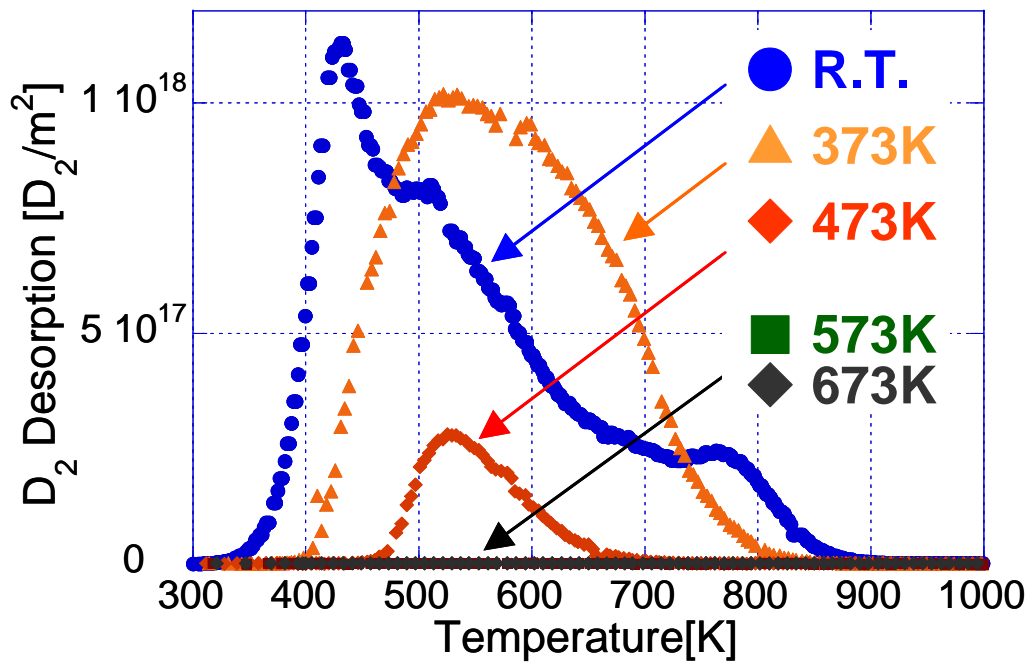


Time evolution of the total amount of gas feed and evacuation to the external pumping.

- The wall pumping depends on the plasma parameters and it leads to be difficult to control of particle balance in steady state. The co-deposition process plays an essential role in the wall pumping rate.

How to resolve

The wall pumping should be controlled. It is difficult to control the co-deposition process on the wall, therefore $R=1$ is the unique solution.



N.Yoshida et al.

- TDS spectrum for Mo implanted D (2keV-D+, 3x10²¹ D/m²) at various temperature.
- At the high temperature region, D does not absorbed in the material.
- We consider the high temp. wall works as the reflector of the particle.

Proposed particle control in steady state

- Wall works sometimes as particle sink and sometimes as source.
- Wall pumping rate is comparable to pumping rate of external pumps.
- It is difficult to control wall pumping rate, because the effect of co-deposition is crucial.

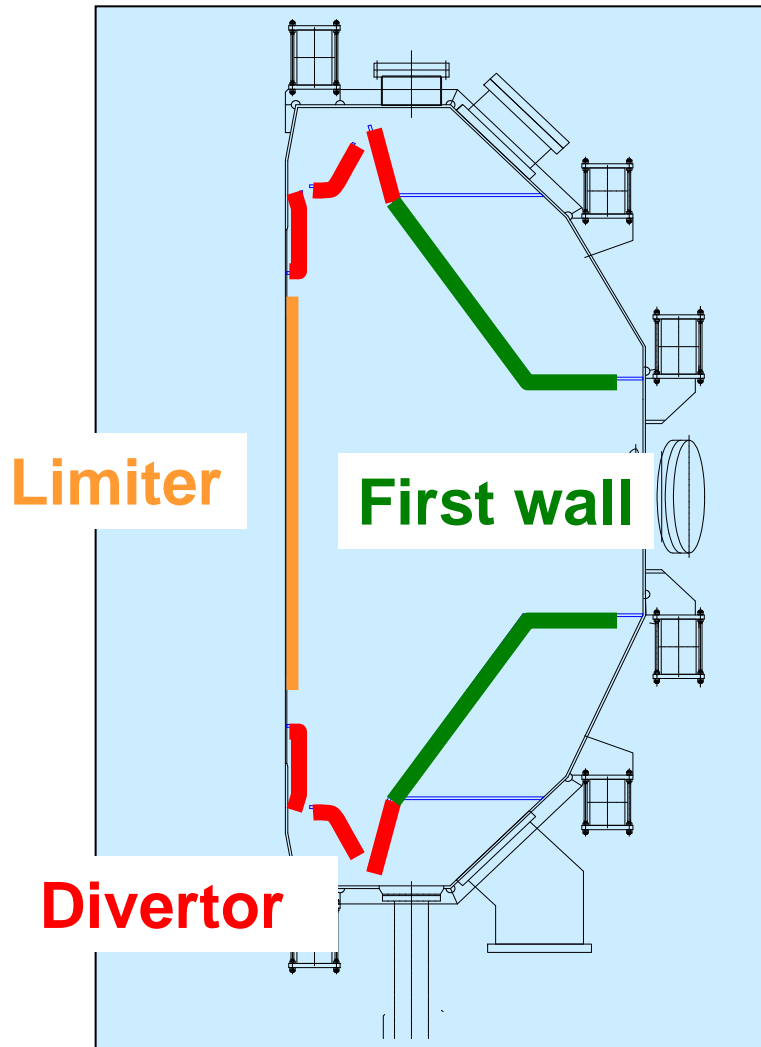


- Recycling rate will become to unity under metal high temp. wall .



- It is necessary to investigate it in real-operated plasma confinement device.

Plan for high temp. wall and divertor



V.V. : SUS316L ($\sim 150^{\circ}\text{C}$)

First wall: W ($300\sim 500^{\circ}\text{C}$)

Divertor: W ($400\sim 500^{\circ}\text{C}$)

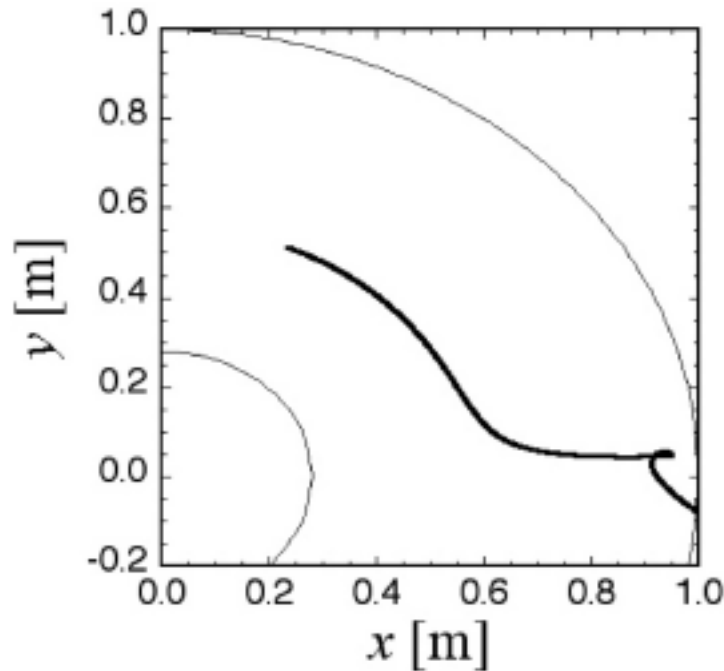
Limiter : SUS316L coated by
W (300°C)

Schedule and Research items

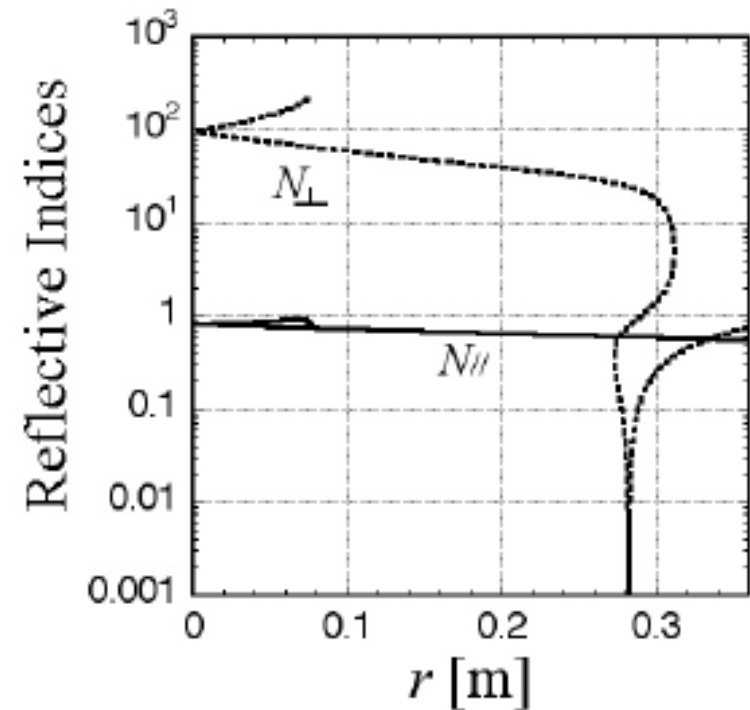
fiscal year	05	06	07	08	09	10	11	12	13	14	further
items											
construction											
High β						>10% (1sec)				20%	
Plasma start-up				RF+OH		RF+OH+NBI					
Current drive				RF		RF(8.2GHz)+NBI				16GHz	
PWI				W		W, high Temp. wall				Control of Recycling	
Divertor				open			closed			advanced	
fueling				Gas puff		CT injection				pellet	


We are here.

How to obtain steady state plasma Ray Trace for EBCD

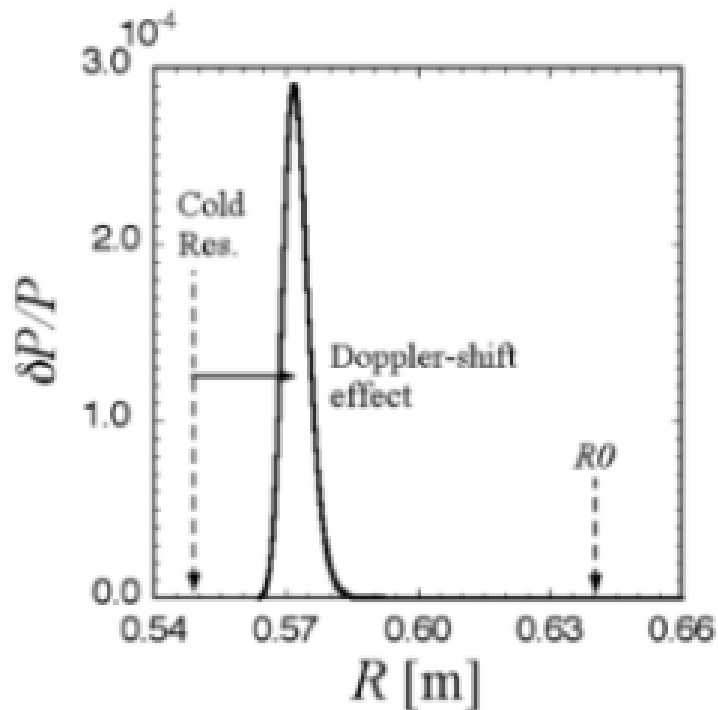


Wave trajectory at the toroidal cross section in the O-X-B conversion scenario at the QUEST.

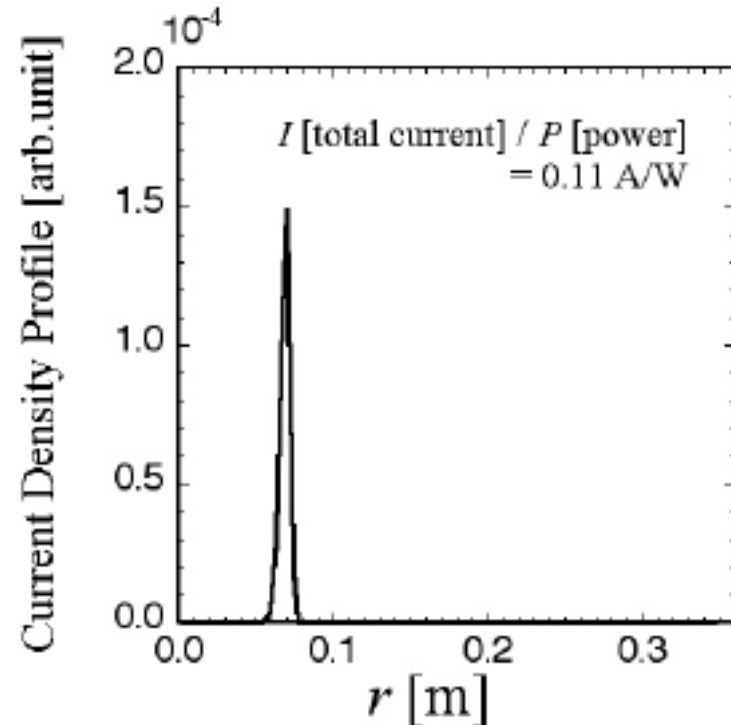


Evolutions of refractive indices N_{\perp} and N_{\parallel} in perpendicular and parallel to the magnetic field along the propagation.

Calculation of capability of current drive by use of TASK/FP



Power deposition profile in the
O-X-B conversion scenario.



Current profile driven in the
O-X-B conversion scenario.

$I_p/P=0.11$ A/W is obtained in 100eV, $0.4 \times 10^{19} \text{m}^{-3}$.

Capability of EBCD on QUEST

EBCD in W-AS

[H. P. Laqua *et al.* Phys. Rev. Lett. **90**, 075003 (2003)] O-X-B from LHS,
 $n_e = 10.5 \times 10^{19} \text{m}^{-3}$, $B_t = 2.15 \text{T}$, $f = 70 \text{ GHz}$,
 $T_e = 0.8 \text{ keV}$, $I_{\text{CD}} = 2 \text{ kA}$

Dimensionless CD efficiency :

$$\eta = 33 n_{20} I_A R_m / P(\text{W}) / T_e(\text{keV}) \sim 0.43$$



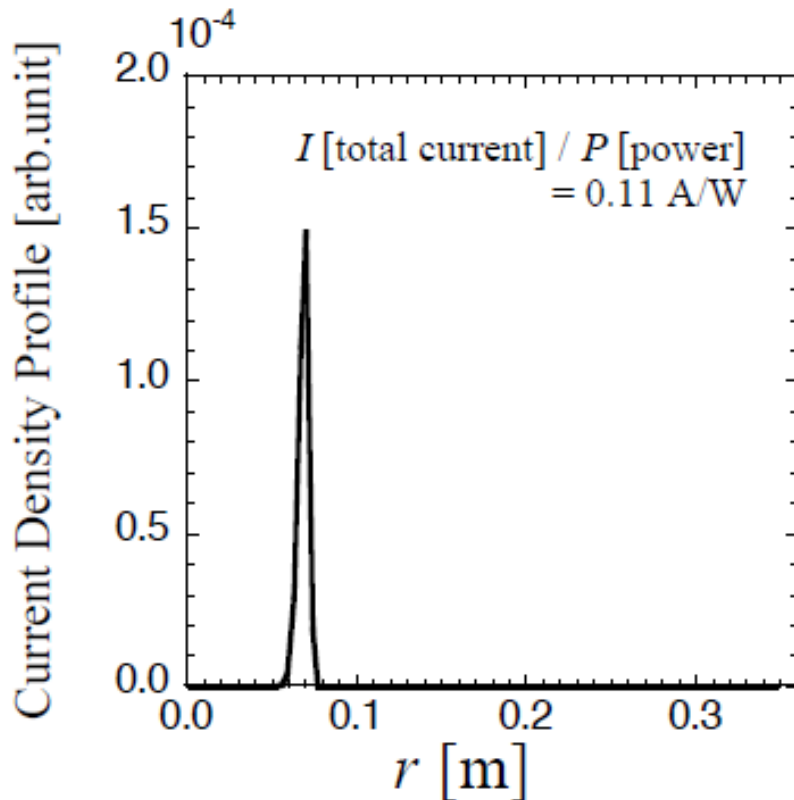
EBCD in QUEST

O-X-B from LHS,

$n_e = 0.2 \times 10^{18} \text{m}^{-3}$, $B_t = 0.25 \text{T}$, $f = 8.2 \text{ GHz}$,
 $T_e = 0.1 \text{ keV}$

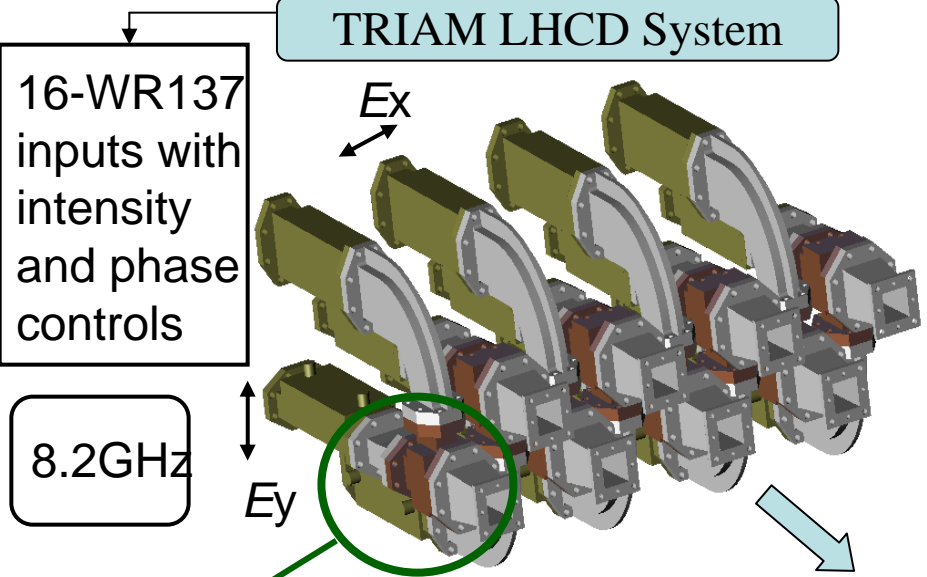
Dimensionless CD efficiency :

$$\eta = 33 n_{20} I_A R_m / P(\text{W}) / T_e(\text{keV}) \sim 0.46$$

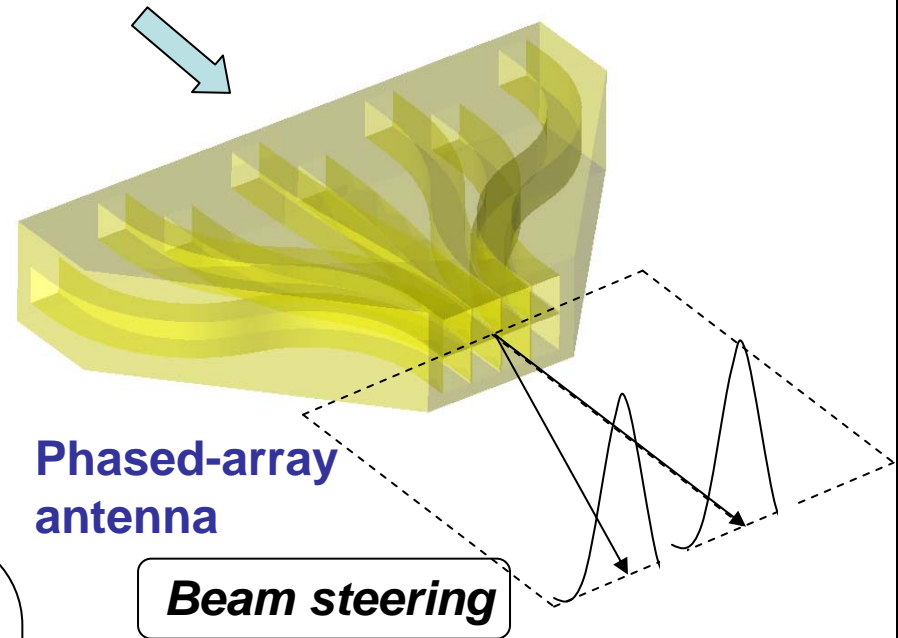
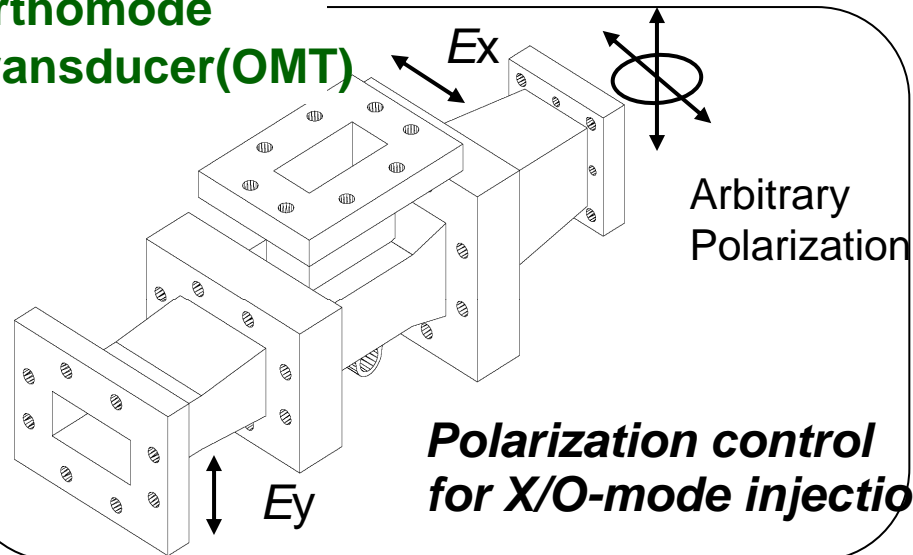


New Concept of Phased Array Antenna

QUEST, Advanced Fusion Research Center



Orthomode Transducer(OMT)



Control of Incident Polarization and Mode

—Orthomode Transducer—

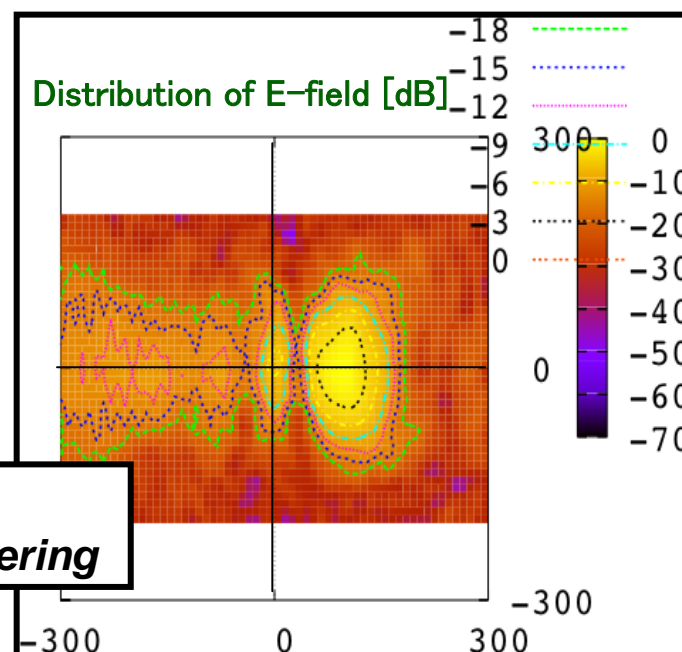
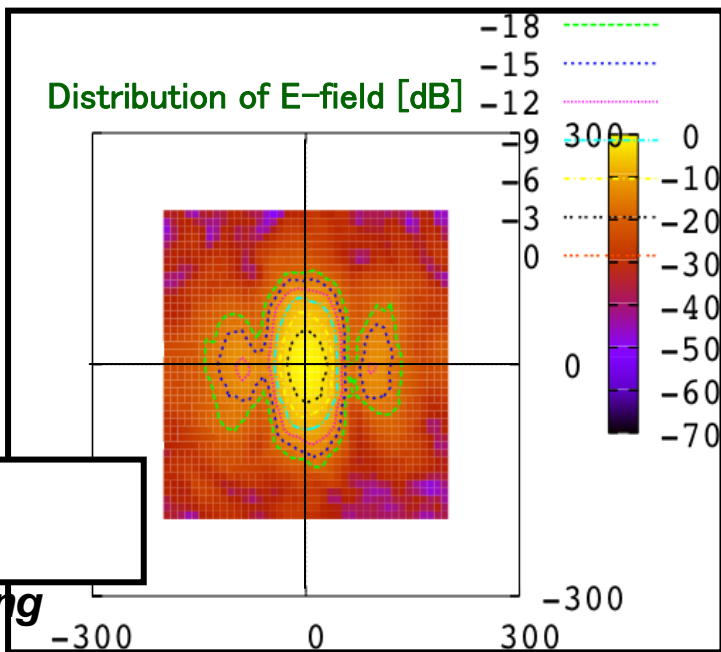
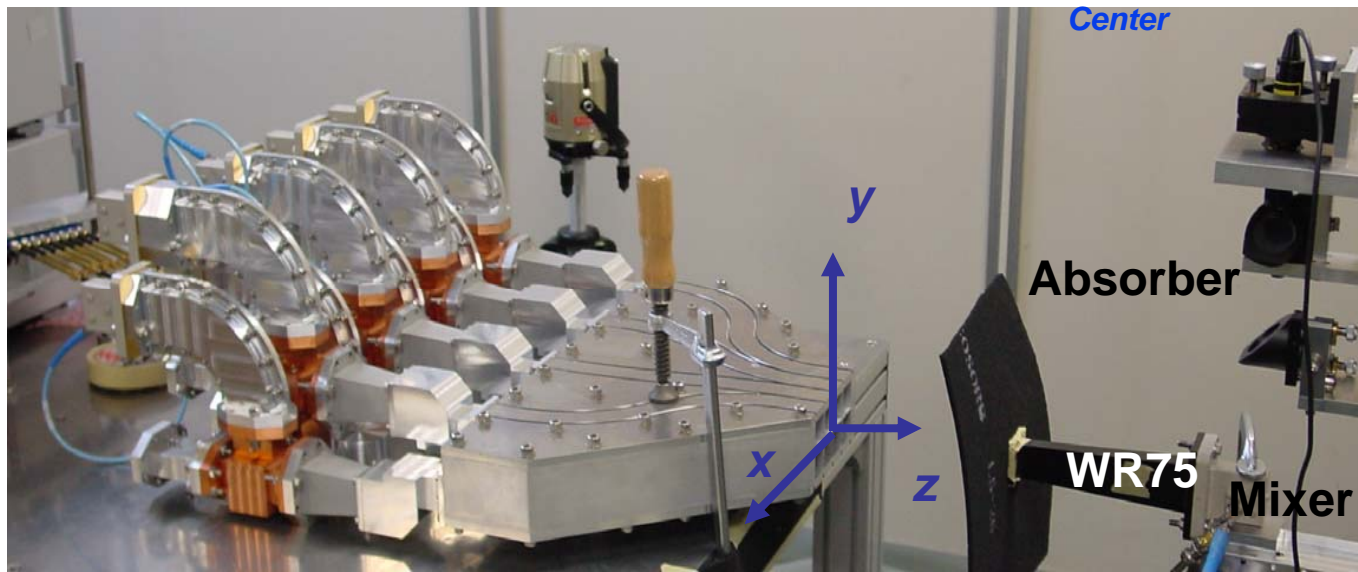
Control of Incident Angle and Beam Properties

—Phased Array Antenna—

Development of Phased Array Antenna

QUEST, Advanced Fusion Research Center

Experiment in Low Power Test Device



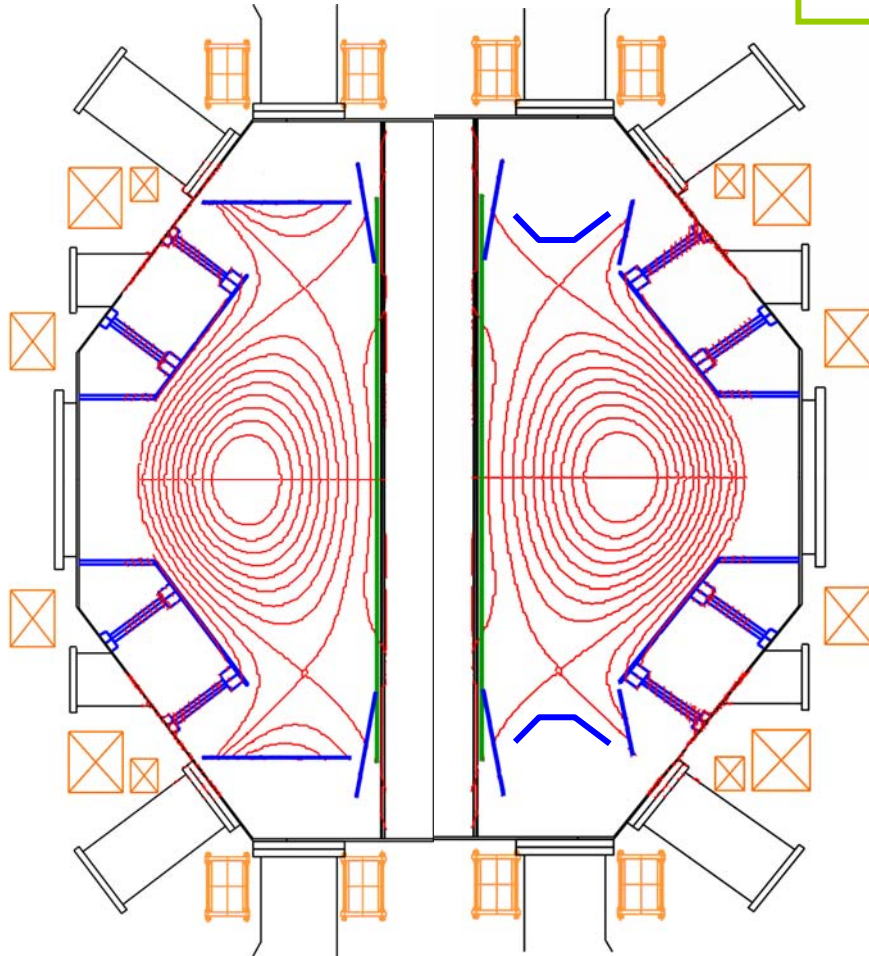
Schedule and Research items

fiscal year	05	06	07	08	09	10	11	12	13	14	further
items											
construction											
High β						>10% (1sec)				20%	
Plasma start-up				RF+OH		RF+OH+NBI					
Current drive				RF		RF(8.2GHz)+NBI				16GHz	
PWI				W		W, high Temp. wall				Control of Recycling	
Divertor				open		closed				advanced	
fueling				Gas puff		CT injection				pellet	


We are here.

Plan for divertor and 1st wall

Vacuum Vessel(SUS316L) 150°C



1st step

2nd step

1st Step (2009-10) (300~500 °C)

Flat Open divertor (W)
High temp. wall

Controllability of Magnetic flux

- Heat and Particle flux
- Diagnostics
- Simulation(SOLDOR)

2nd Step (2011-)

Closed Divertor (W)
High temp. wall

Controllability of particle flux

- Heat and Particle flux
- Diagnostics
- Simulation(SOLDOR)

Simulation of design of divertor structure

Using SOLDOR/NEUT2D, Investigation of the divertor structure of QUEST has been executed.

Issues for divertor design

Heat handling

Heating of 1MW will be executed on QUEST in steady state and Heating of 3M is planned in pulsed discharge.

➡ **Need to estimated heat flux on the divertor plate**

Particle handling

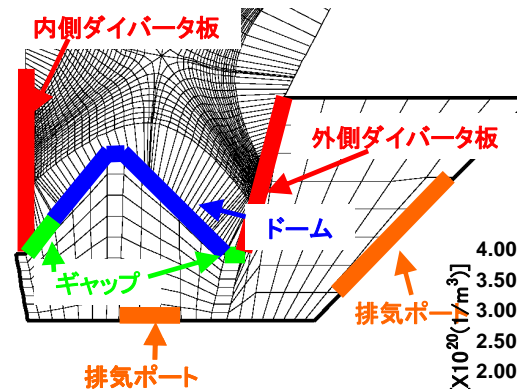
QUEST will be operated on the condition of $R=1$ due to high temperature wall and it is necessary to evacuate all of particle by pumping.

➡ **Need to estimated required particle exhaust**

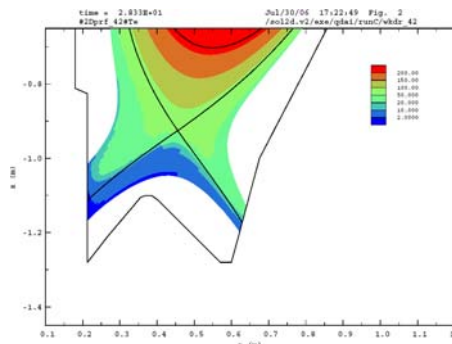
➡ **Comparison with experimental data on the flat divertor**

An example of the calculation of plasma parameters in divertor

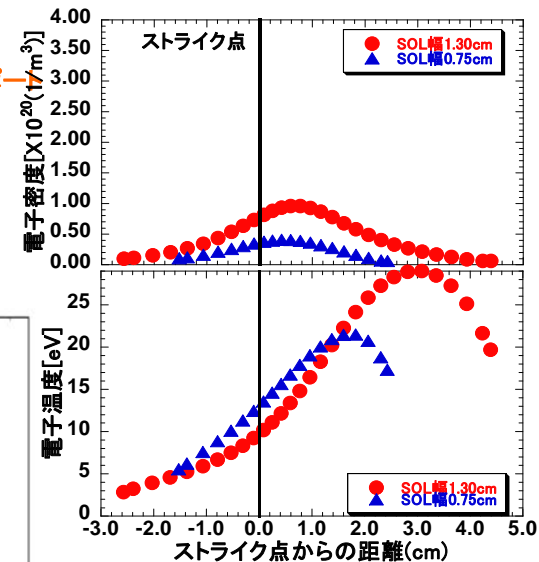
Mesh structure



Temperature distribution



Density and Temperature distribution along outer divertor plate

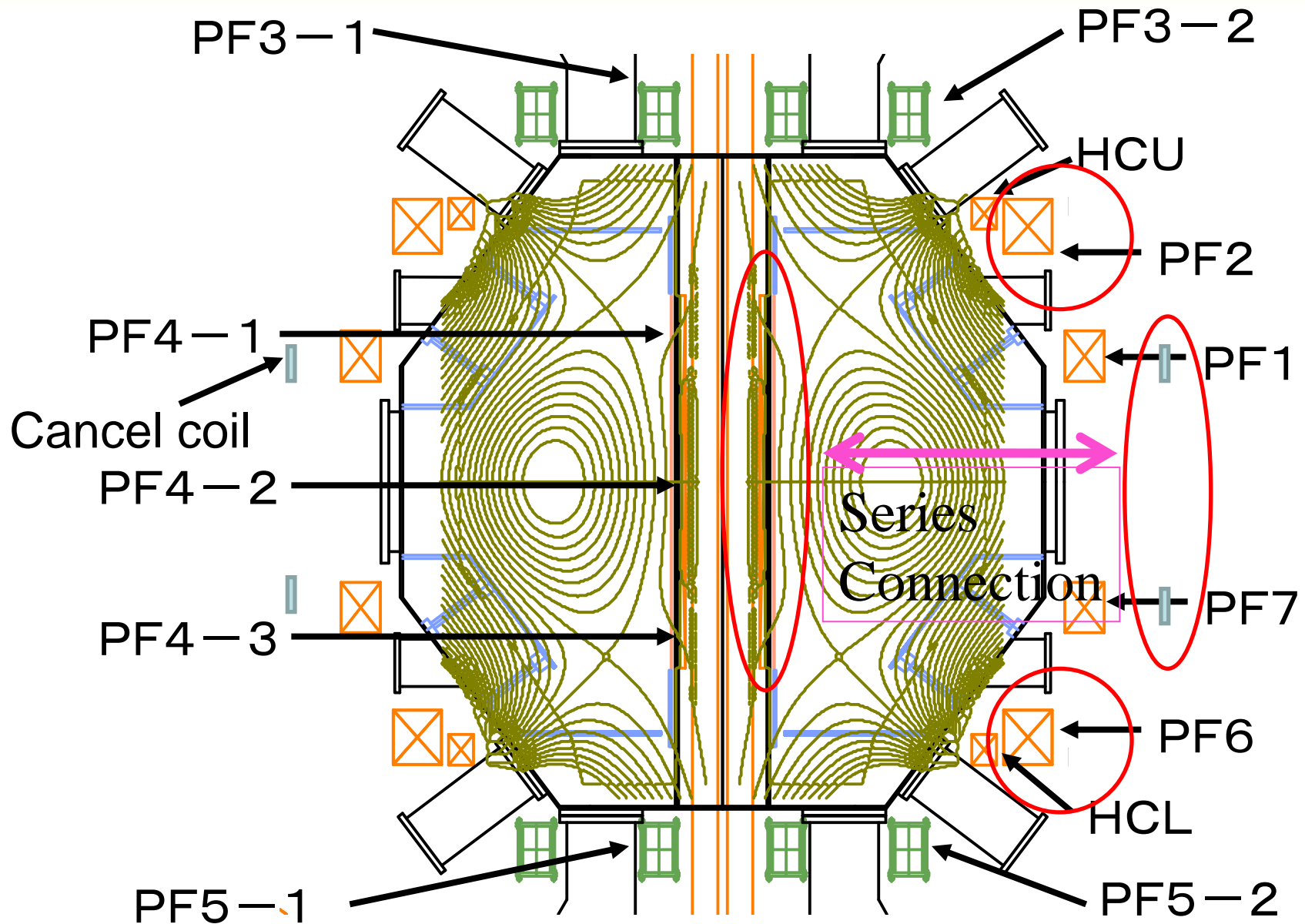


Schedule and Research items

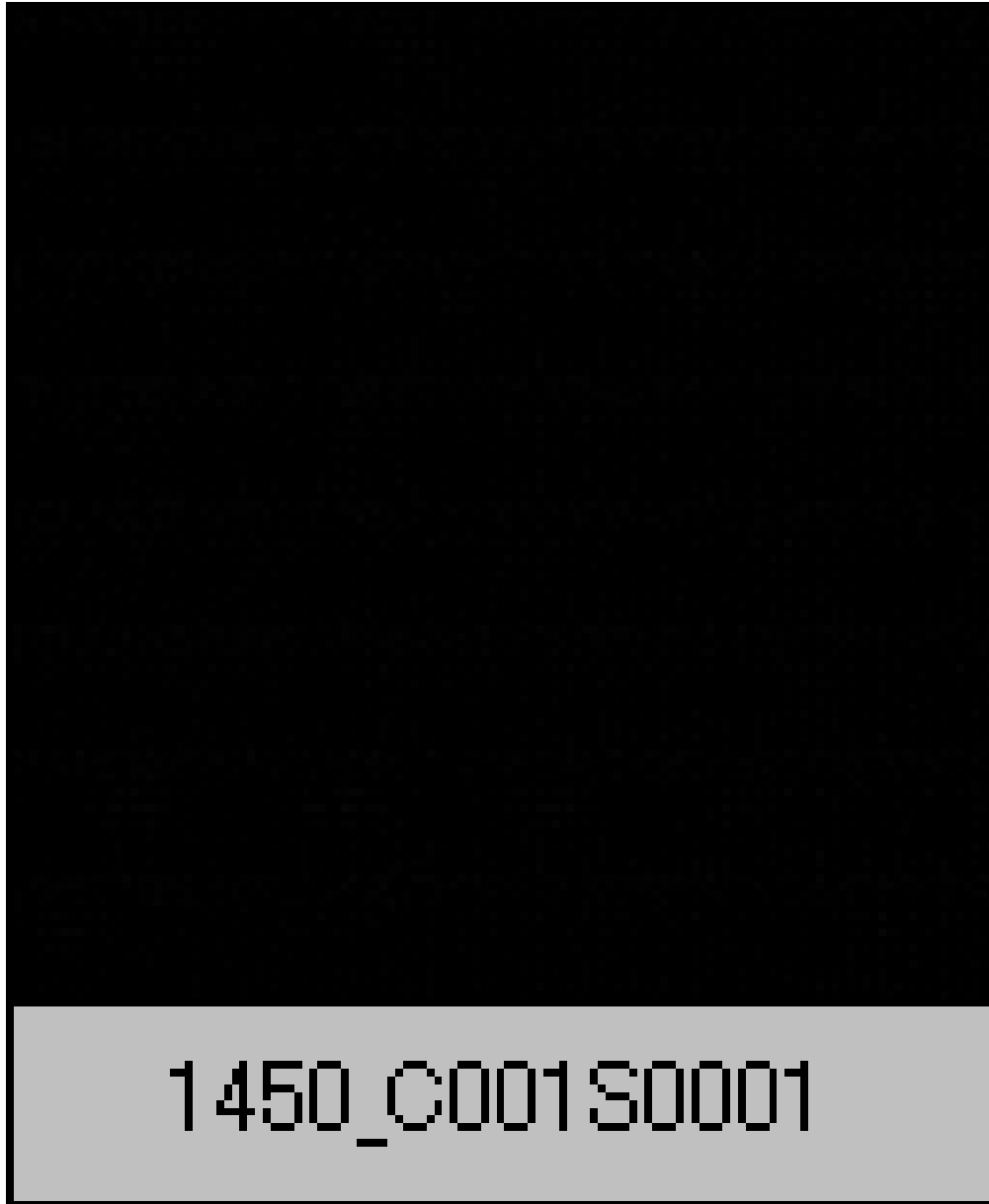
fiscal year	05	06	07	08	09	10	11	12	13	14	further
items											
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Current drive				RF		RF(8.2GHz)+NBI				16GHz	
PWI				W		W, high Temp. wall				Control of Recycling	
Divertor				open			closed			advanced	
fueling				Gas puff		CT injection				pellet	


We are here.

PF coils layout and connection

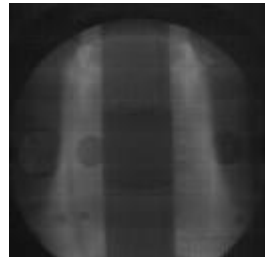
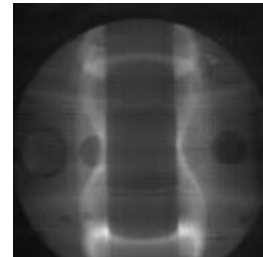
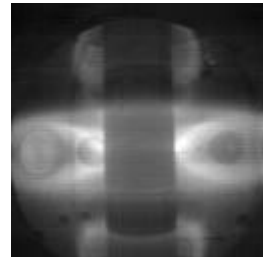
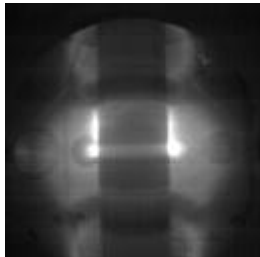
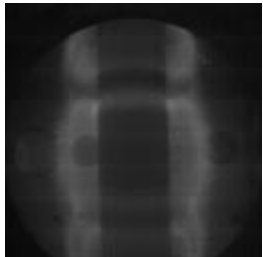
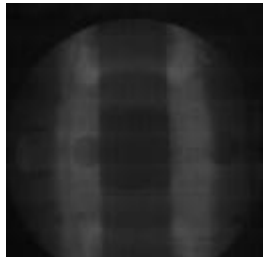
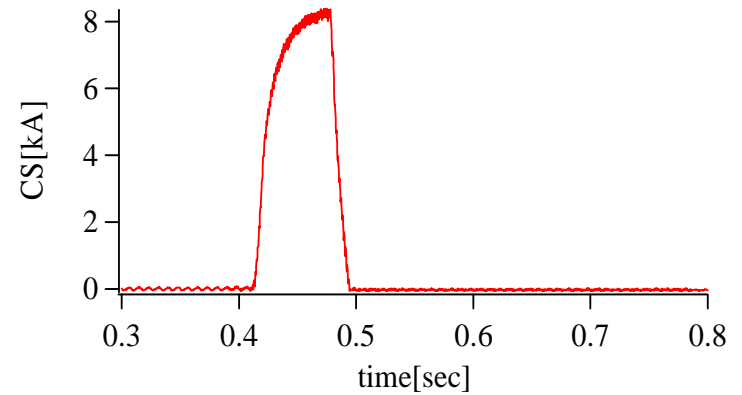
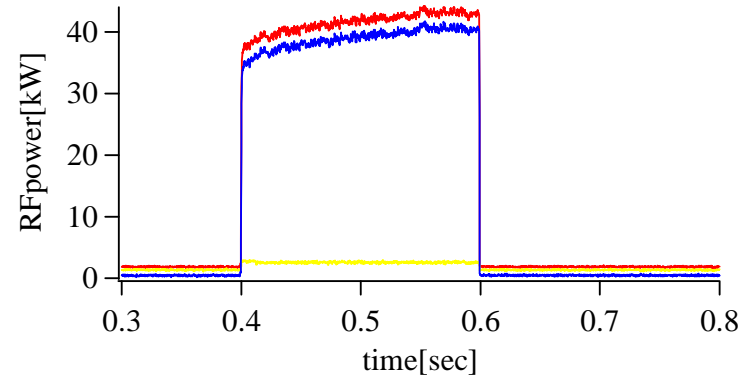
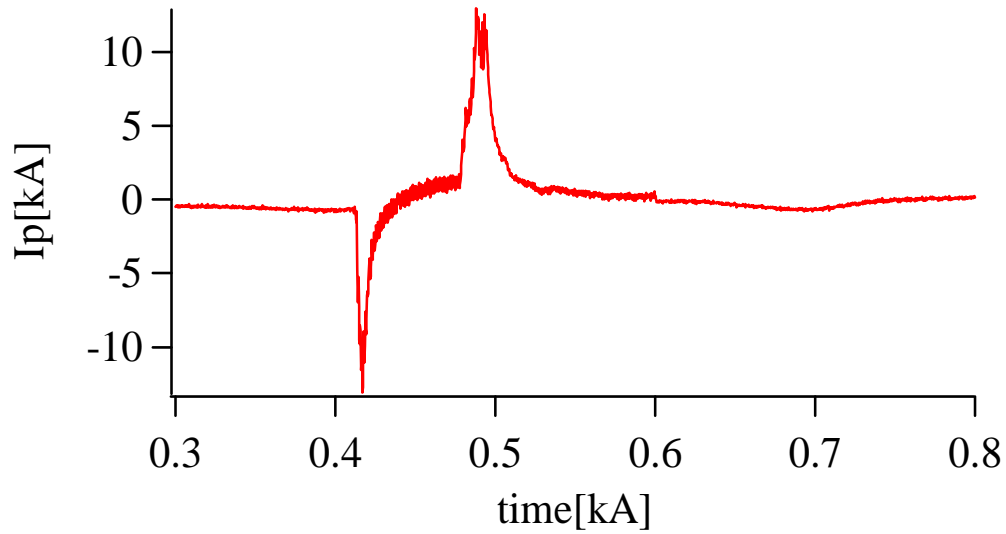


First formation of Tokamak configuration



[QUEST] Formation of closed flux surface in OH + RF

#1450



0.4545sec

0.486675sec

0.4923sec

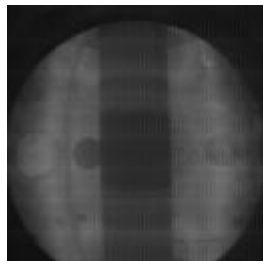
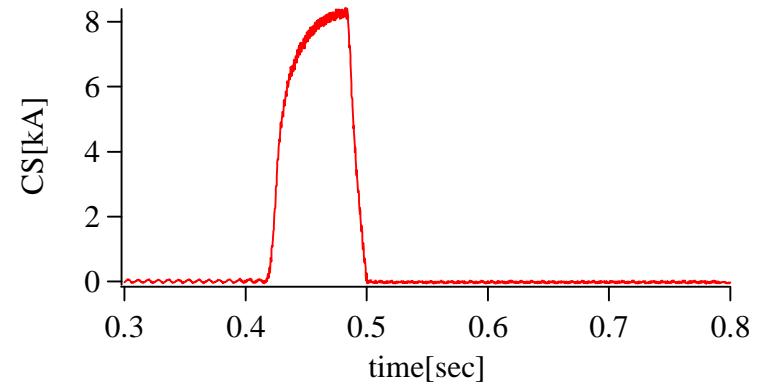
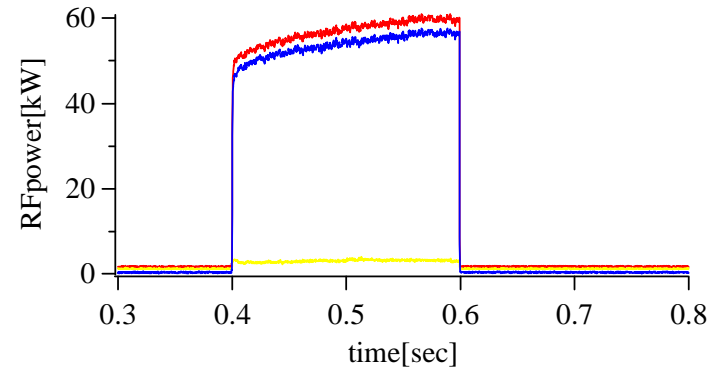
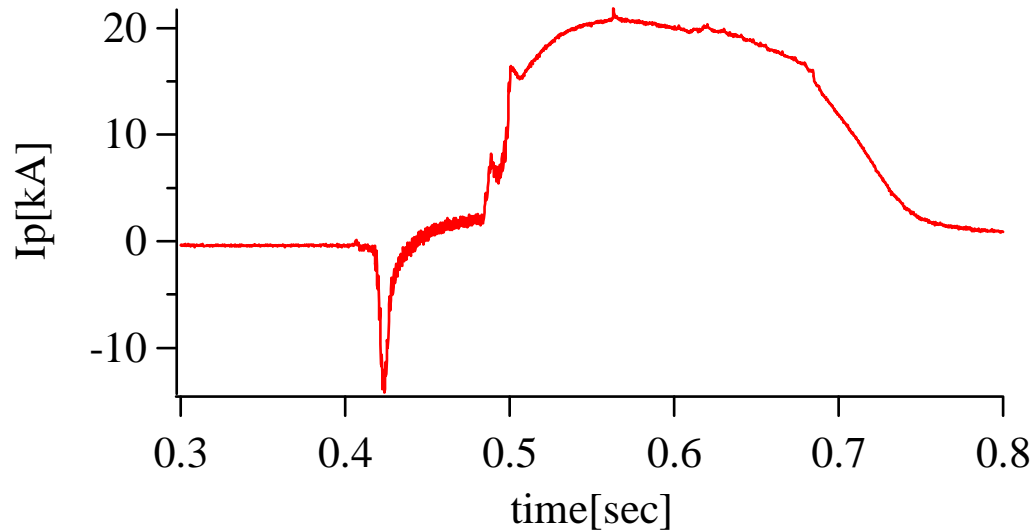
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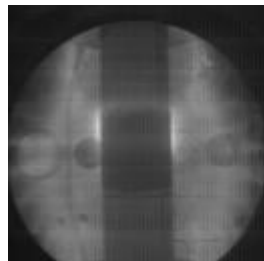
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[QUEST] Formation of closed flux surface in OH + RF

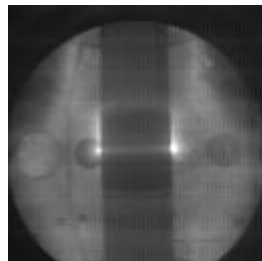
#1456



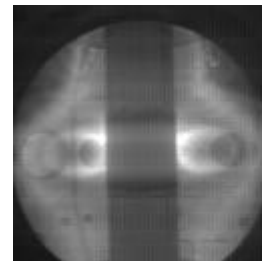
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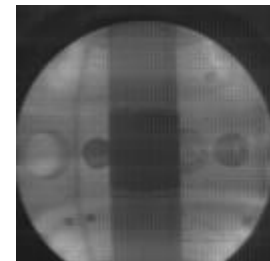
0.5025sec



0.50385sec



0.505275sec

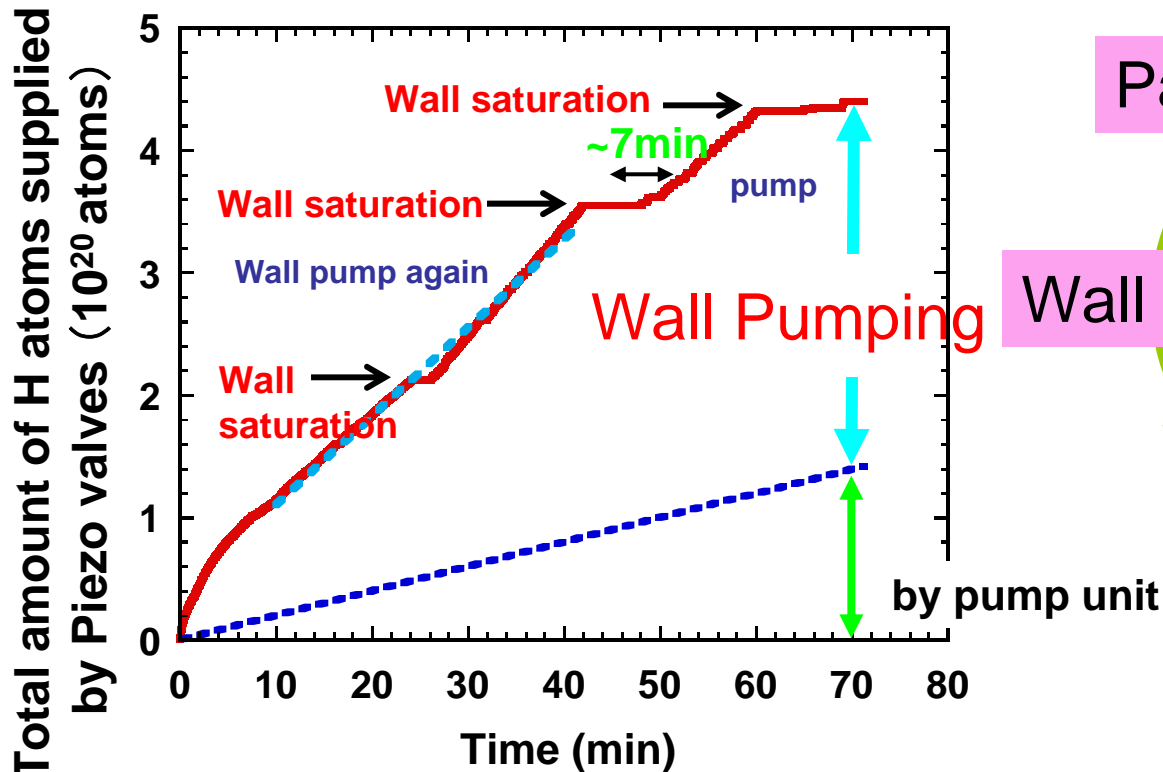


0.53sec

summary

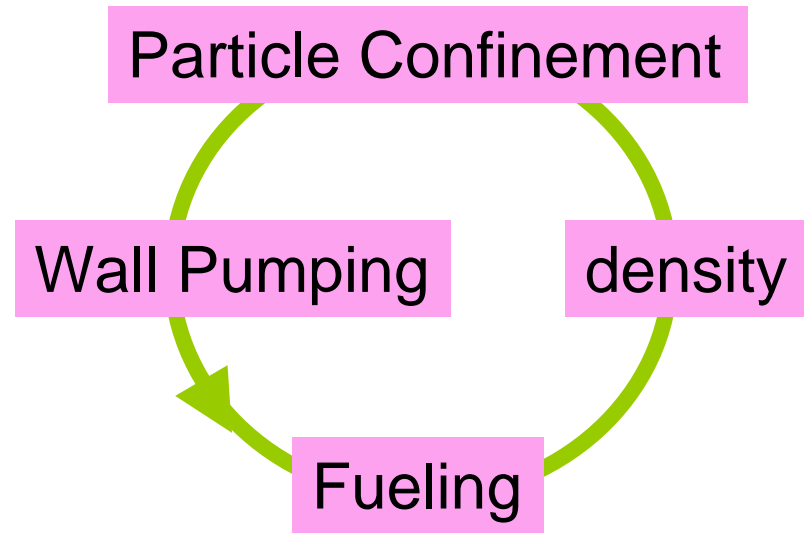
- The QUEST program starts from 2005 to develop the scientific basis for achieving a steady state condition at sufficiently high beta ($\sim 20\%$), with high confinement and low collisionality, in a longer term program that contains three Phases of R&D.
- The first experimental data could be obtained. In next experimental campaign, we would like to obtain steady-state plasma.

Controllability of Wall Pumping

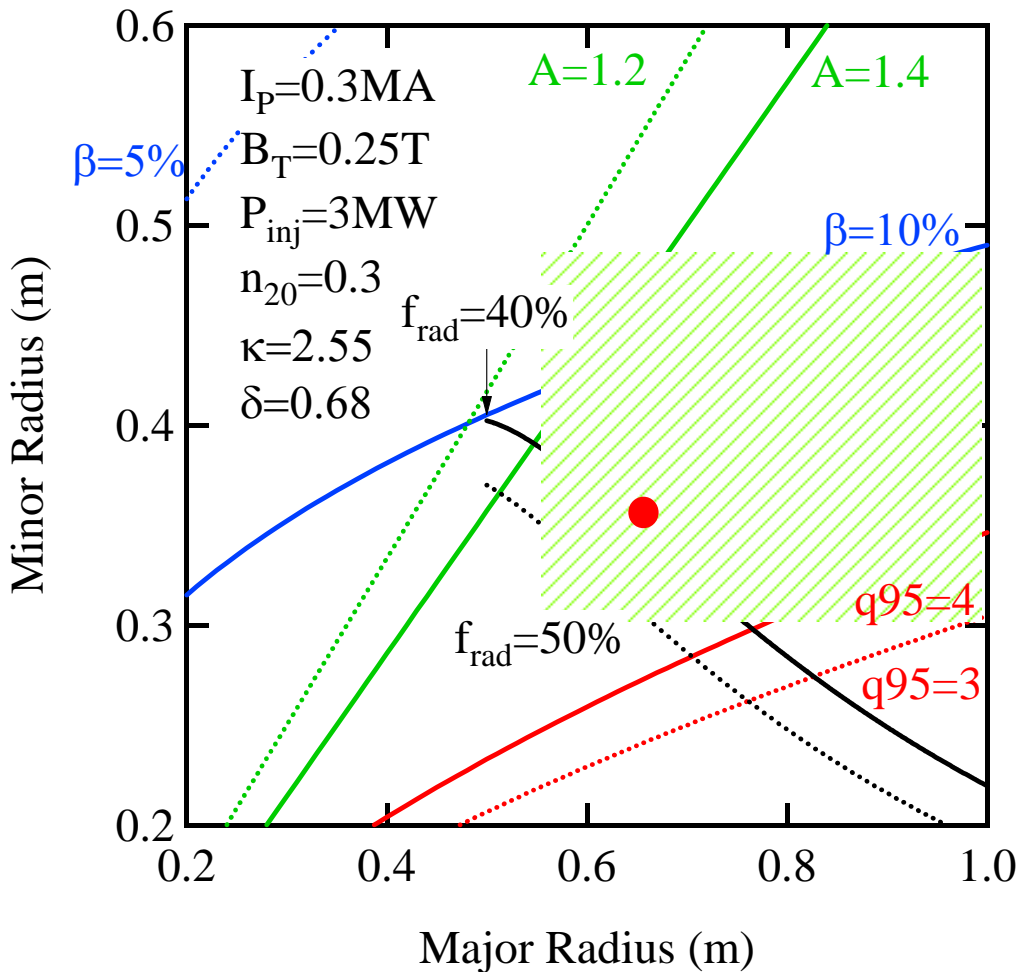


Wall pumping rate

$$\sim 1.5 \times 10^{16} \text{ atoms m}^{-2}\text{sec}^{-1}$$



Feasibility of the Mission

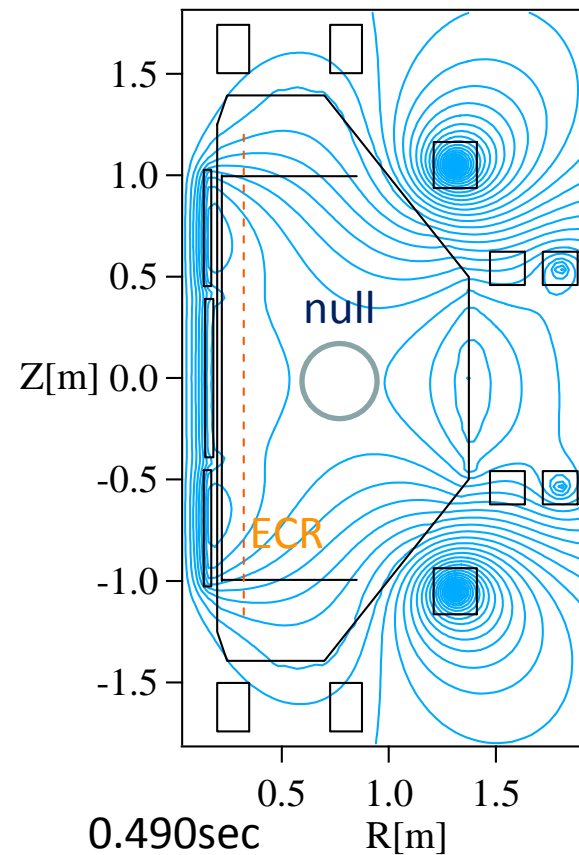
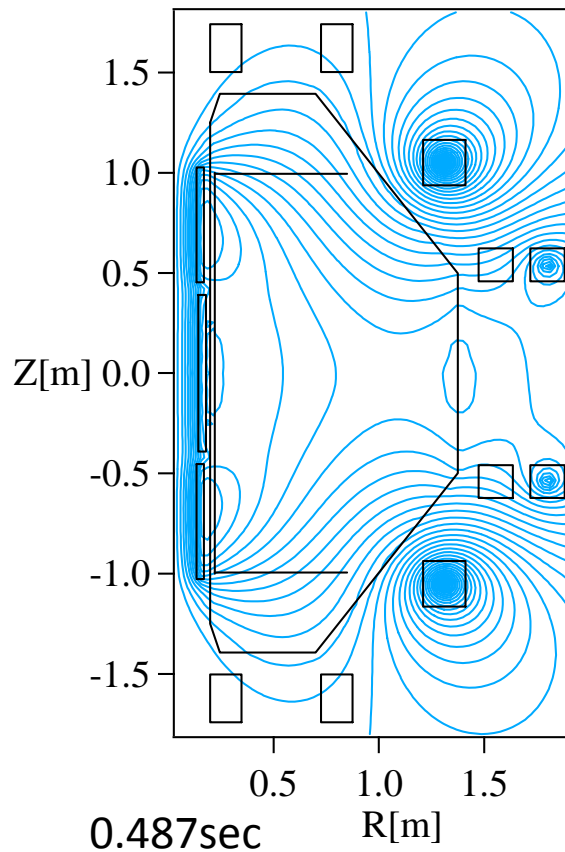
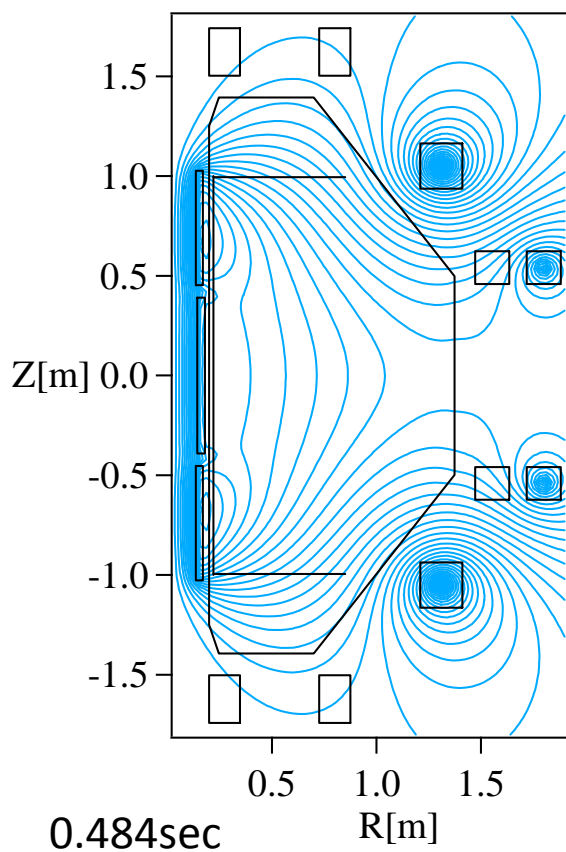
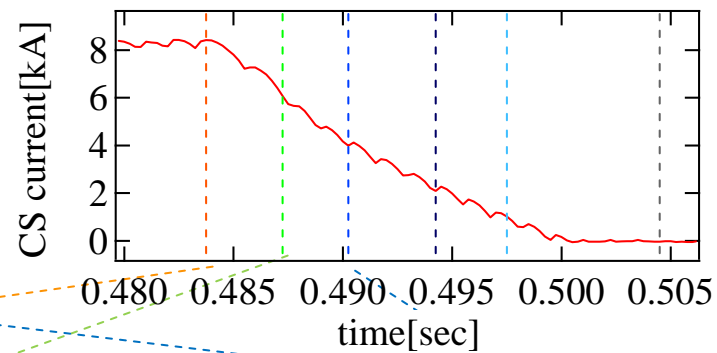
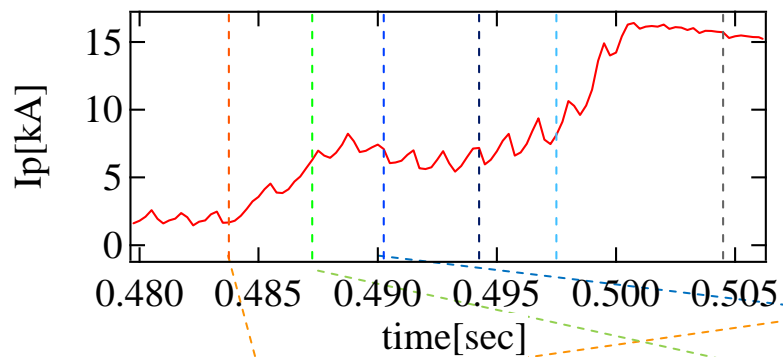


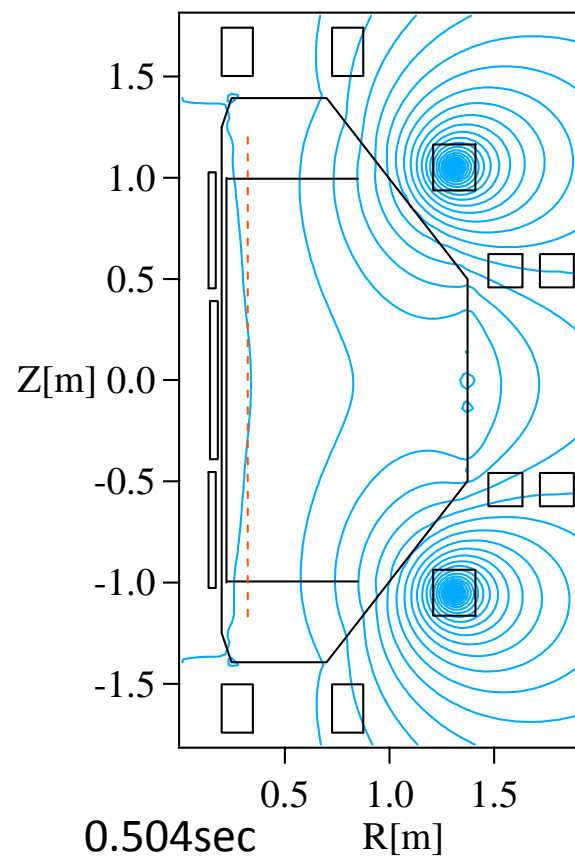
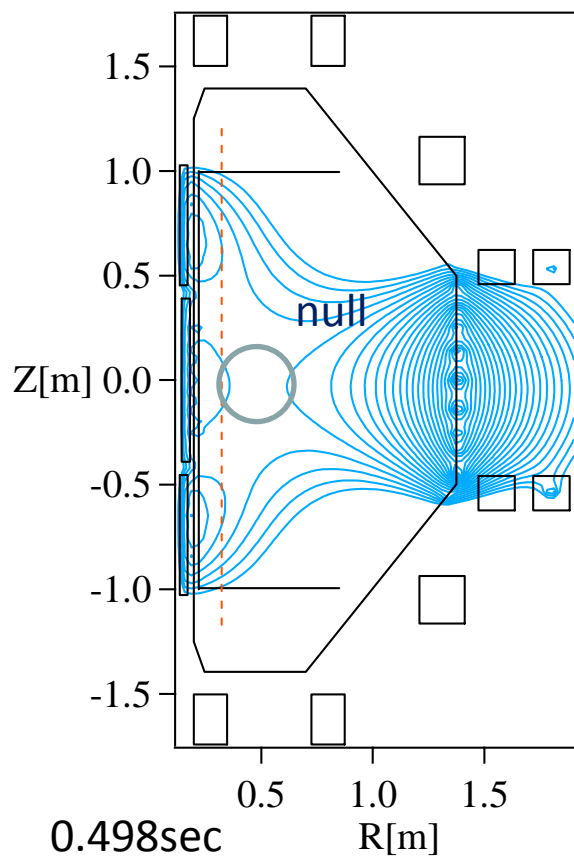
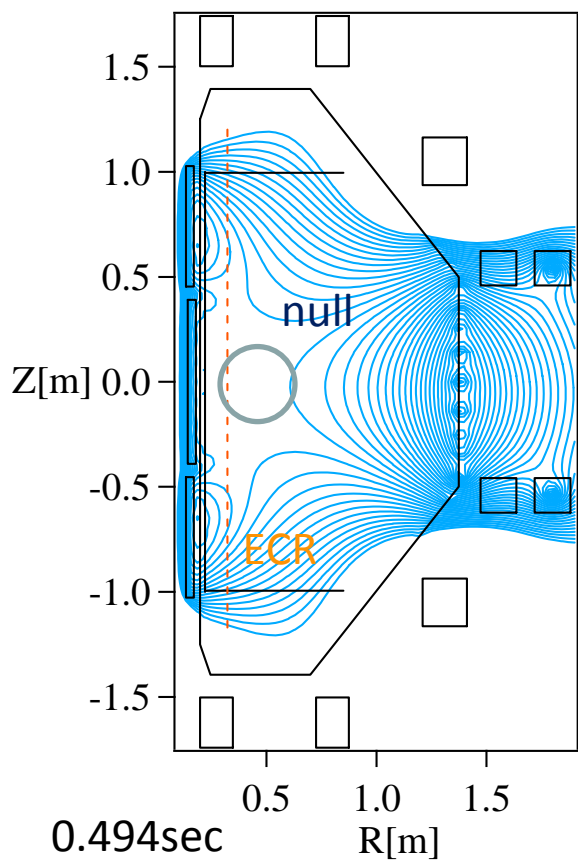
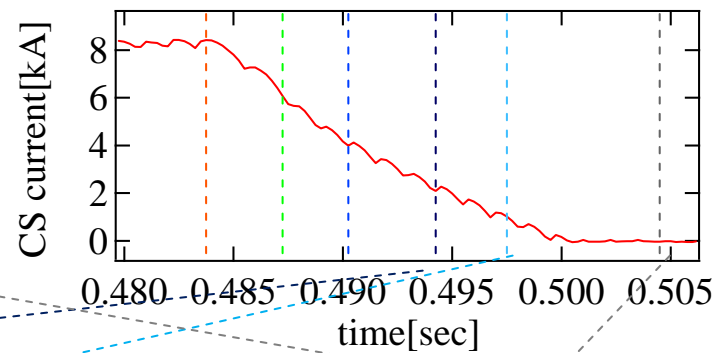
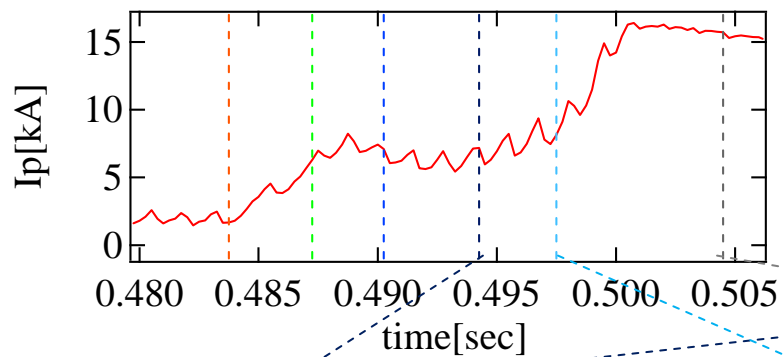
Mission in phase I

- plasma current 20kA in steady state

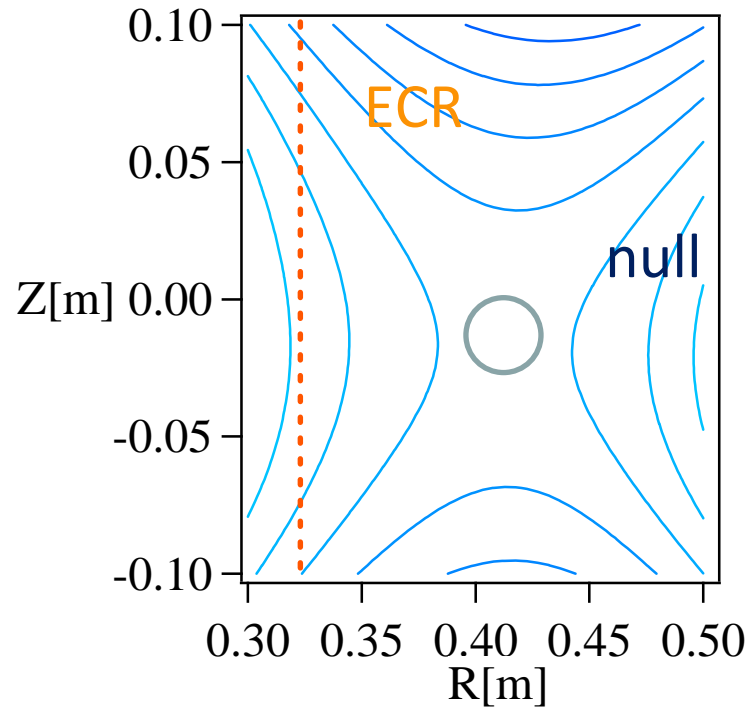
Mission in phase II

- plasma current 100kA in steady state
- plasma current 300kA at $\beta > 10\%$ 1 sec

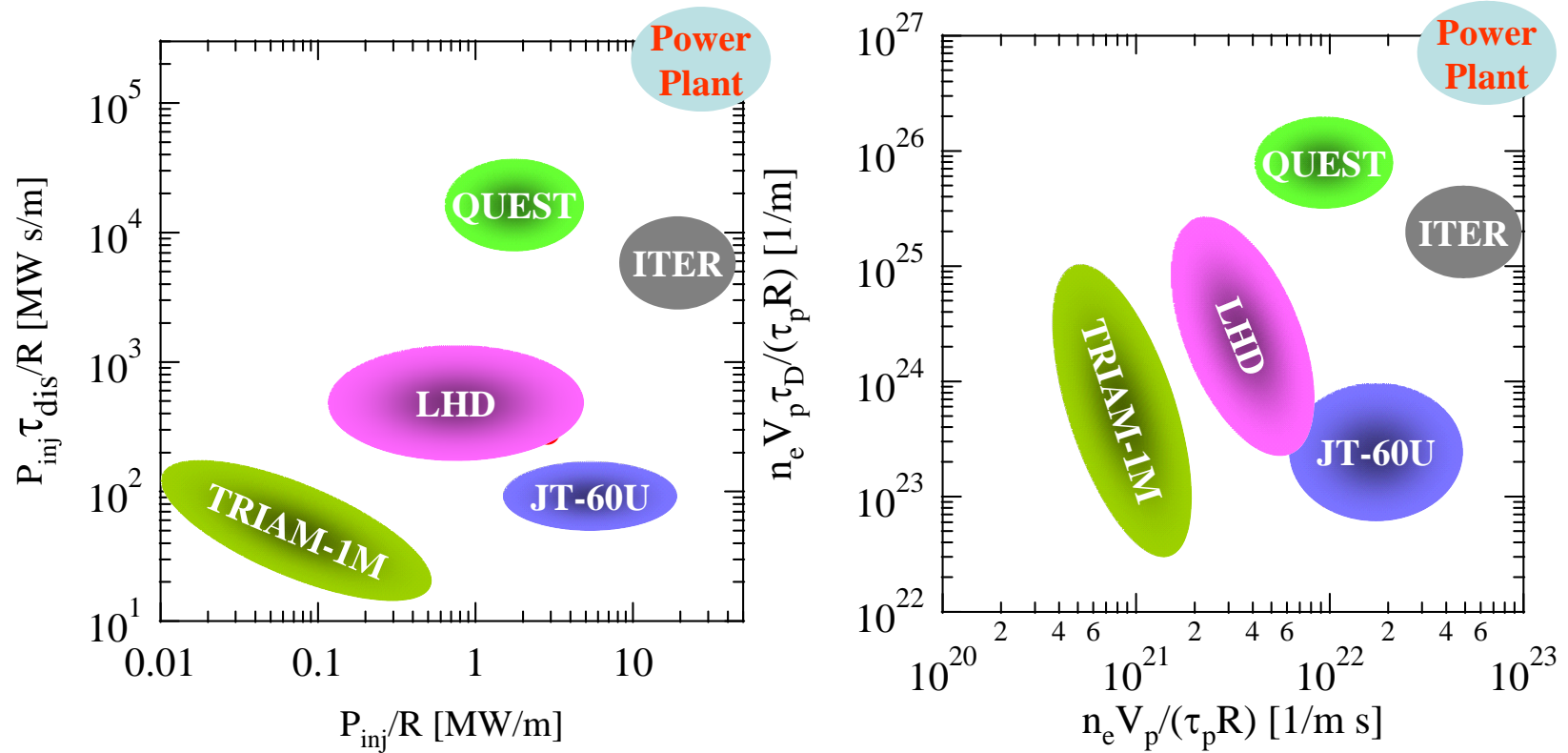




0.494secのときのnull点
(0.41,-0.02)
上下非対称性は渦電流の
非対称性による。

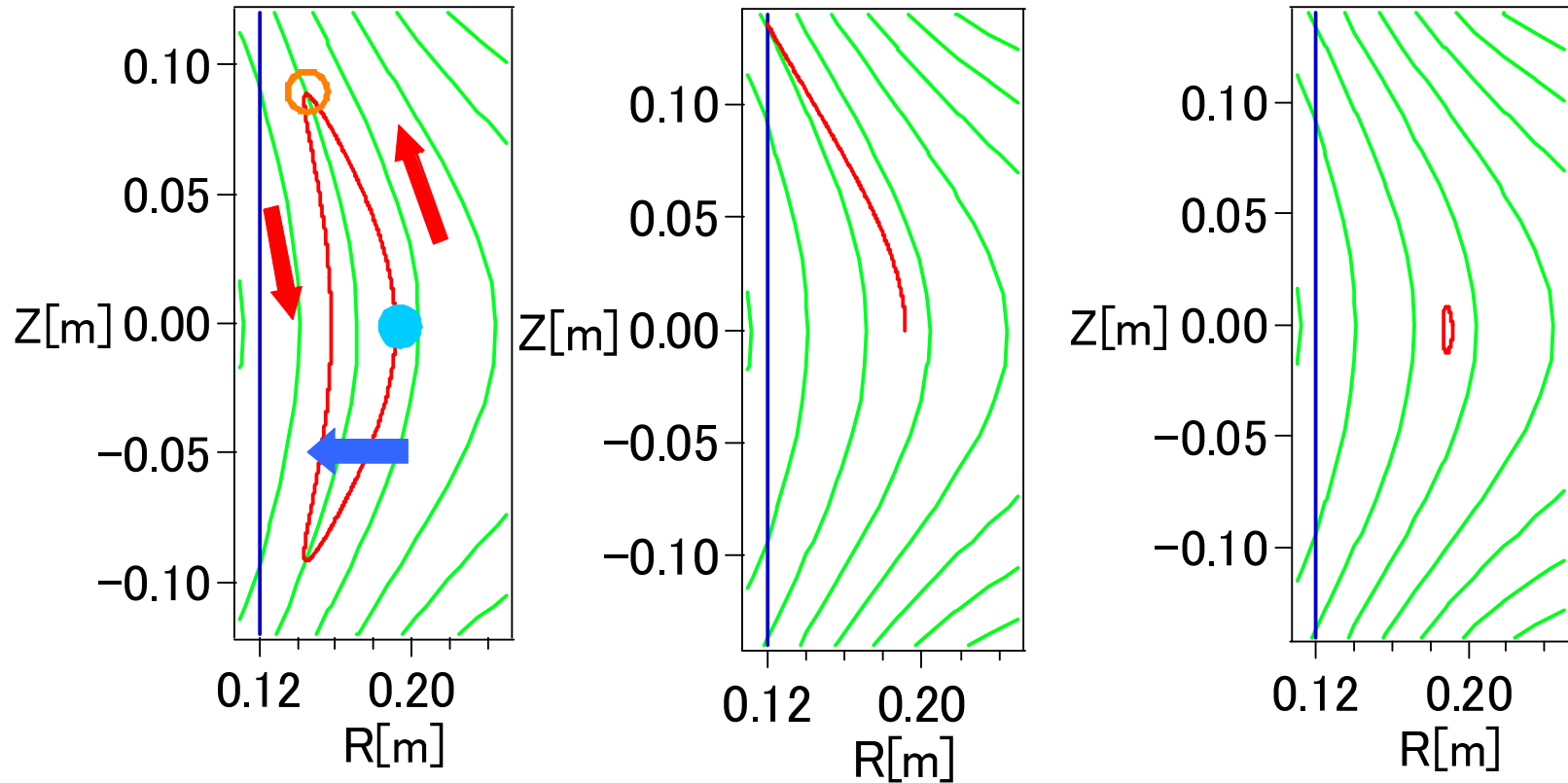


Heat and Particle load on QUEST



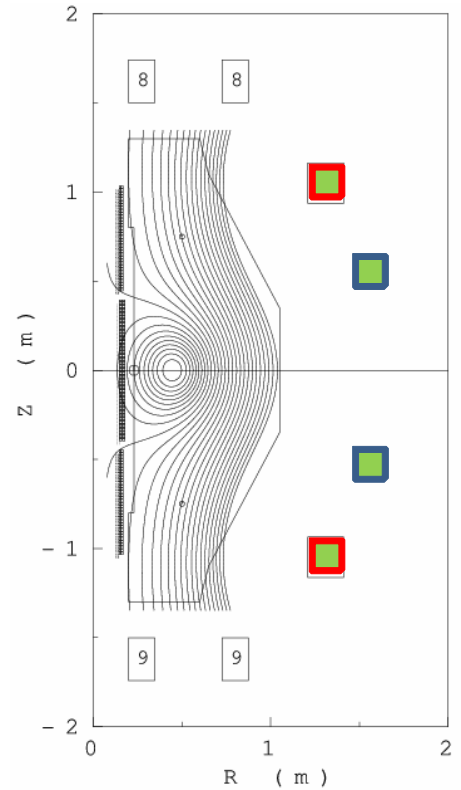
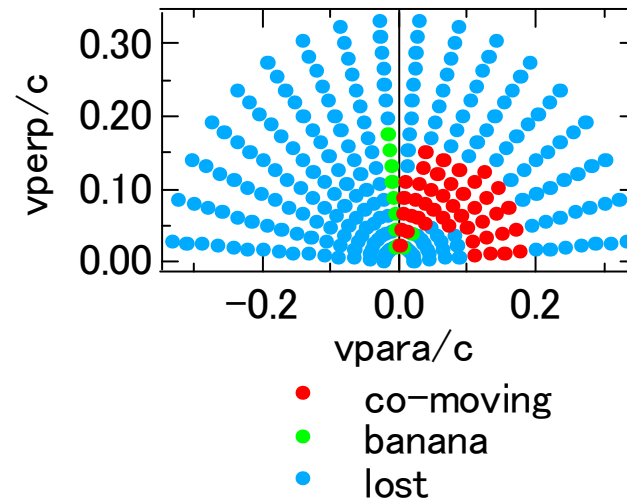
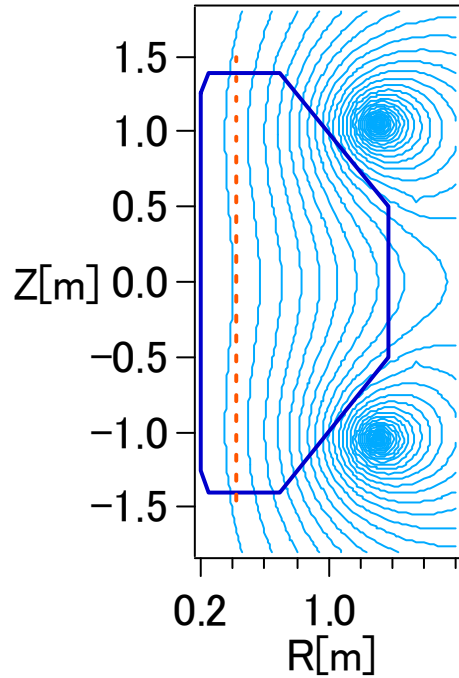
Operation region of QUEST on heat (left) and particle (right) handling. Left: The vertical axis is approximately proportional to heat load to divertor and the horizontal axis is approximately proportional to heat flux to the divertor. Right: The vertical axis is approximately proportional to fluence to the divertor and the horizontal axis is approximately proportional to particle flux, where we assume particle confinement time equals energy confinement time.

Plasma start-up scenario I



Typical orbit of energetic electron in open magnetic field

Plasma start-up scenario II



Heating and Current drive

- Power and Required current drive efficiency

Phase I 20-30kA at low density

RF (0.45MW)

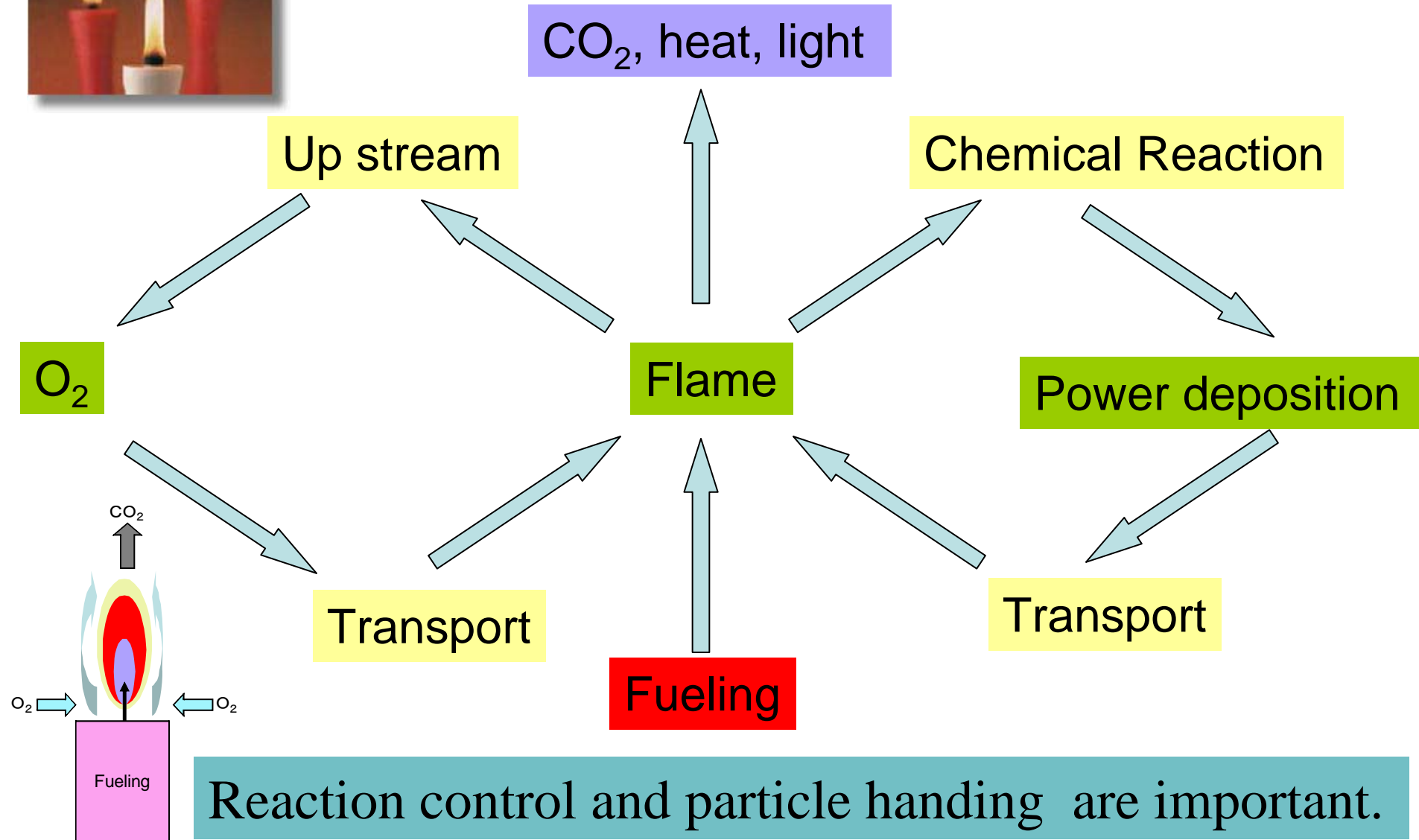
Phase II (SS) 0.026×10^{19} A/W/m²

RF (1MW) [+ NB (2MW)]

Phase II (1sec) 0.19×10^{19} A/W/m²

RF (1MW) + NB (2MW) with OH

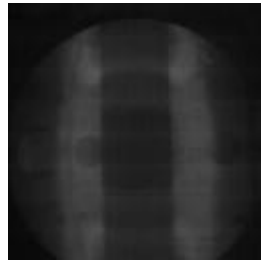
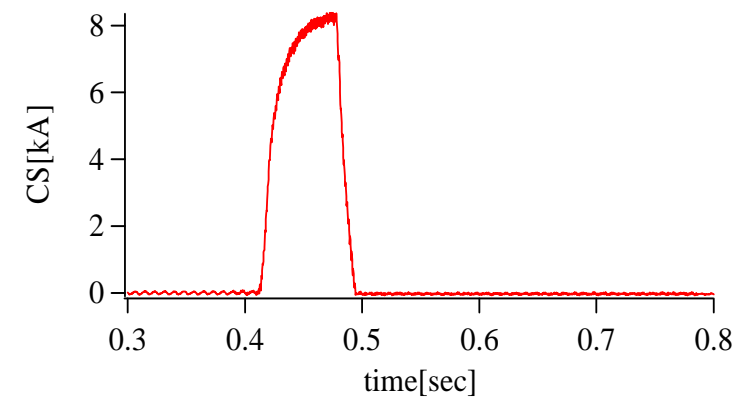
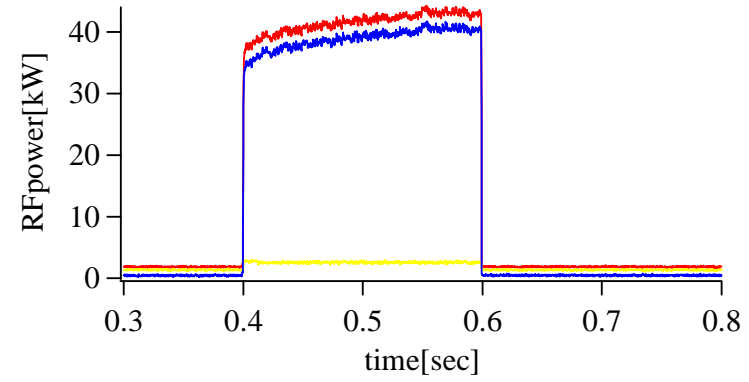
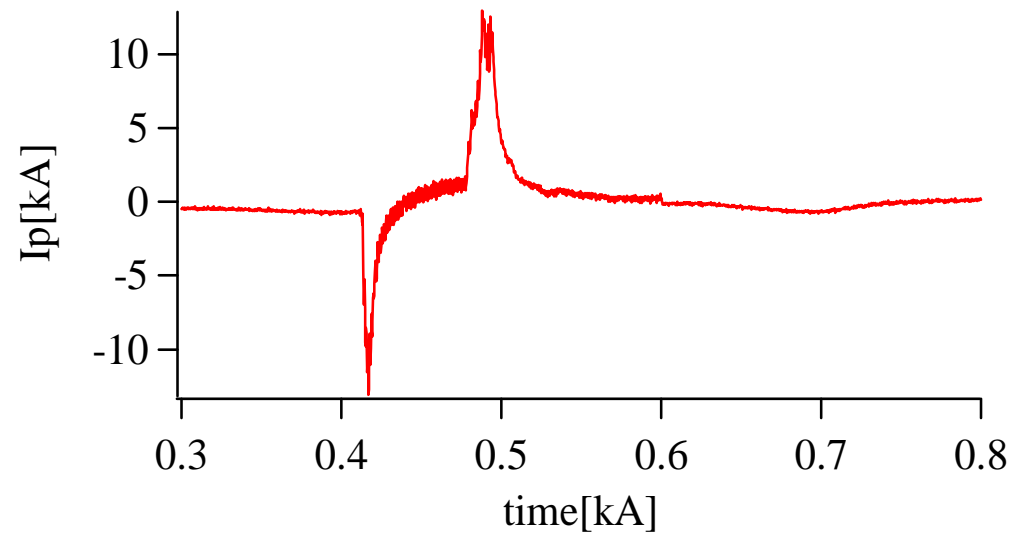
Steady state chemical burning



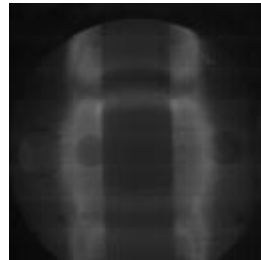
[QUEST]

#1450

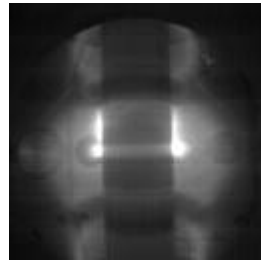
PF4-123CC(1turn):8.33kA 「PGS」01.2605sec 「AT5」0.350sec
RF:3.3V(0.4-0.6sec) RF on
PF17: +000A
PF26: +000A==>+058A==>+175A==>+000A
(0.478s,0.438s,0.446s,1.000s)
TF: 27.5kA
gas 30ms@0.3ms power on



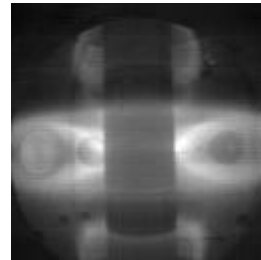
0.4545sec



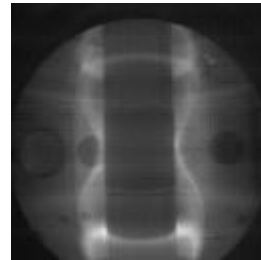
0.486675sec



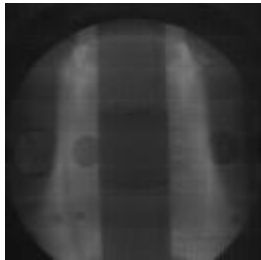
0.4923sec



0.49365sec



0.49875sec



0.50595sec

[QUEST]

#1456

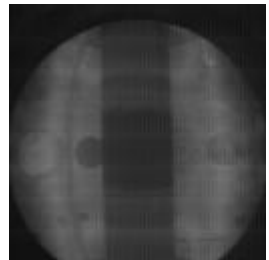
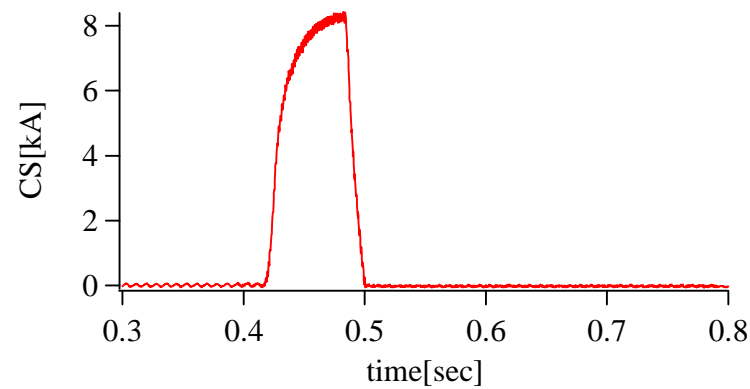
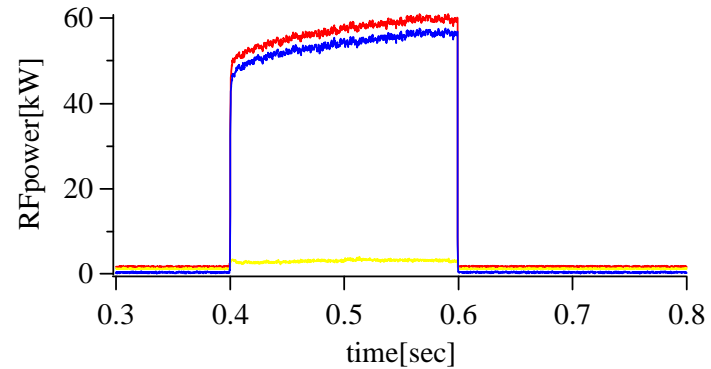
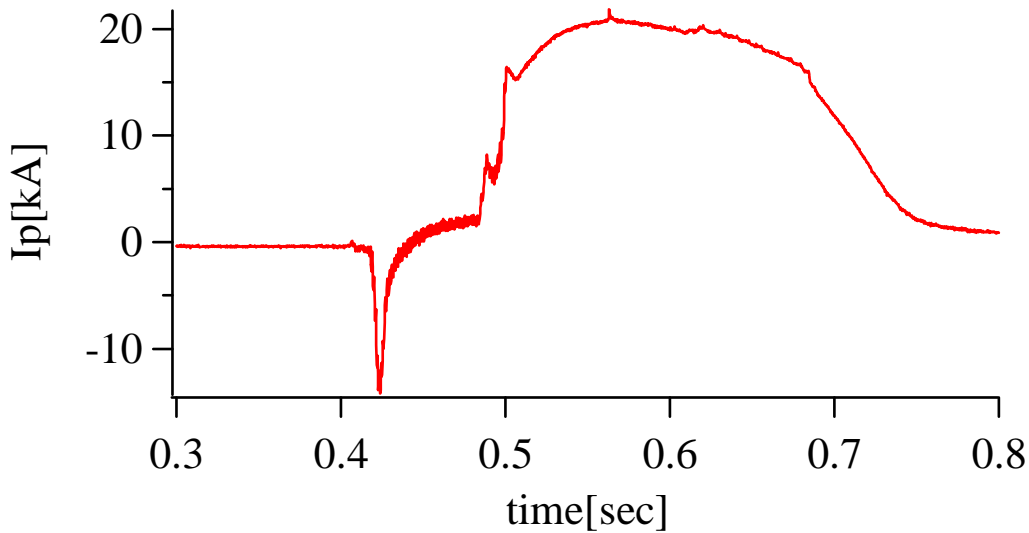
PF4-123CC(1turn):8.33kA 「PGS」0.2605sec 「AT5」0.350sec

RF:4.3V(0.4-0.6sec) RF on

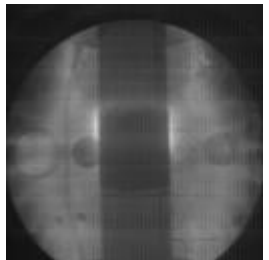
PF17: +000A

PF26: +000A==>+058A==>+475A==>+000A (0.438s,0.446s,1.000s)

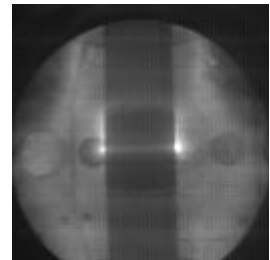
TF: 30.0kA gas 30ms@0.3ms power on



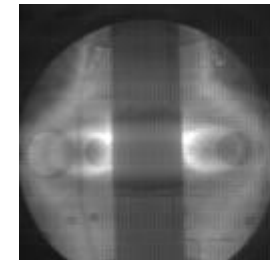
0.49sec



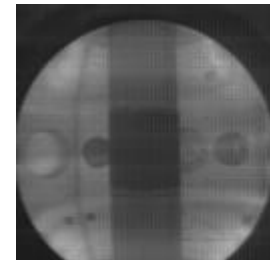
0.5025sec



0.50385sec

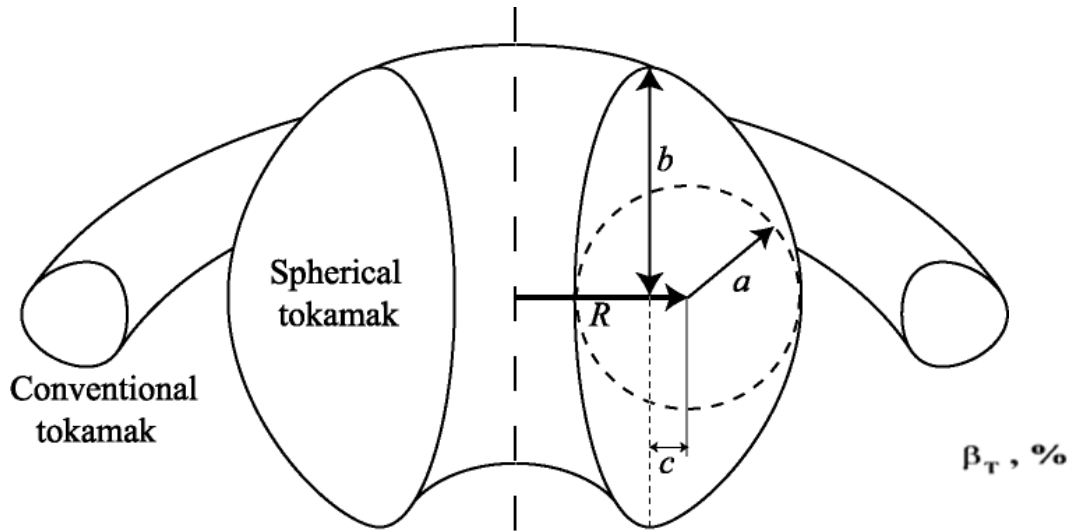


0.505275sec

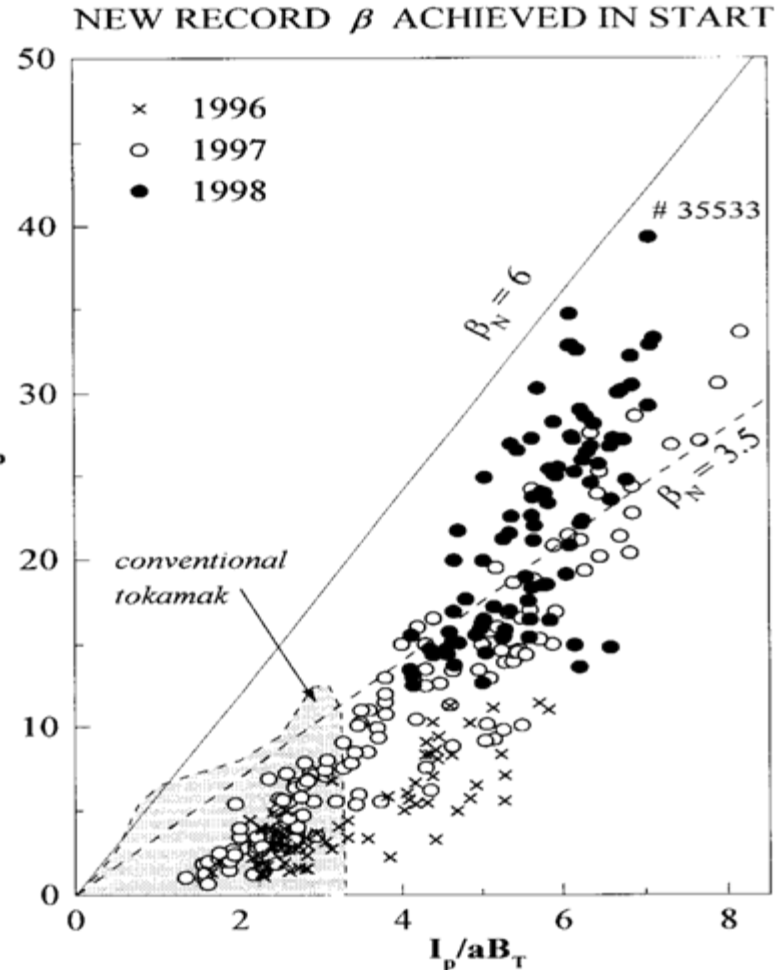


0.53sec

Spherical tokamaks (ST)



Spherical tokamaks (ST) have the possibility to realize cost-effective fusion power plants. High β ($\sim 10\%$) is the indispensable target in QUEST.



Required research items of QUEST

- Plasma start-up
- Non-inductive current drive
- Divertor Research
- Plasma wall interaction
- Achievement of medium or high β
- Particle and heat handling
- Innovative concept

Mainly focus on the technological issue for SSO

Simulation of design of divertor structure

Using SOLDOR/NEUT2D, Investigation of the divertor structure of QUEST has been executed.

Issues for divertor design

Heat handling

Heating of 1MW will be executed on QUEST in steady state and Heating of 3M is planned in pulsed discharge.

➡ **Need to estimated heat flux on the divertor plate**

Particle handling

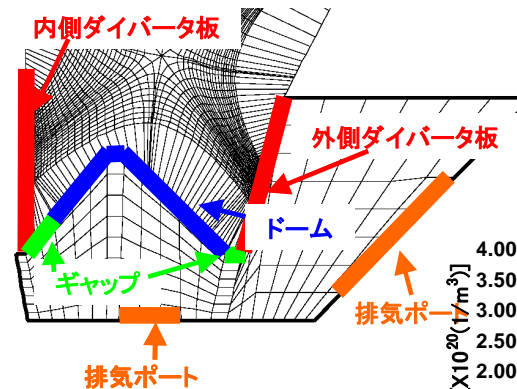
QUEST will be operated on the condition of $R=1$ due to high temperature wall and it is necessary to evacuate all of particle by pumping.

➡ **Need to estimated required particle exhaust**

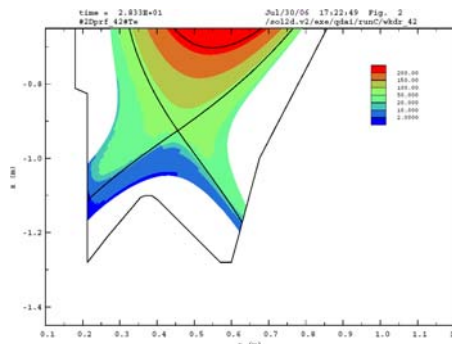
➡ **Comparison with experimental data on the flat divertor**

An example of the calculation of plasma parameters in divertor

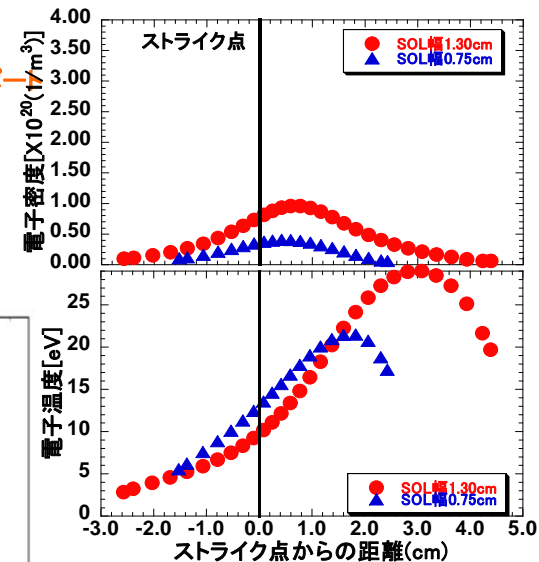
Mesh structure



Temperature distribution



Density and Temperature distribution along outer divertor plate



EBW アンテナ開発計画

X-EBW（垂直入射）、O-X-EBW（斜め入射）、混合モードシナリオによる加熱・電流駆動のために低周波数（ $\sim 8\text{GHz}$ ）高周波コンポーネント開発が必要

1. X/Oモード励起 — Orthogonal Mode Transducer (OMT)の開発 —

平成18年度:高電力仕様に向けた試作・開発、低電力試験

平成18年度:CPD/RF 伝送路での高電力試験

2. 入射角制御 — Steering アンテナの開発 —

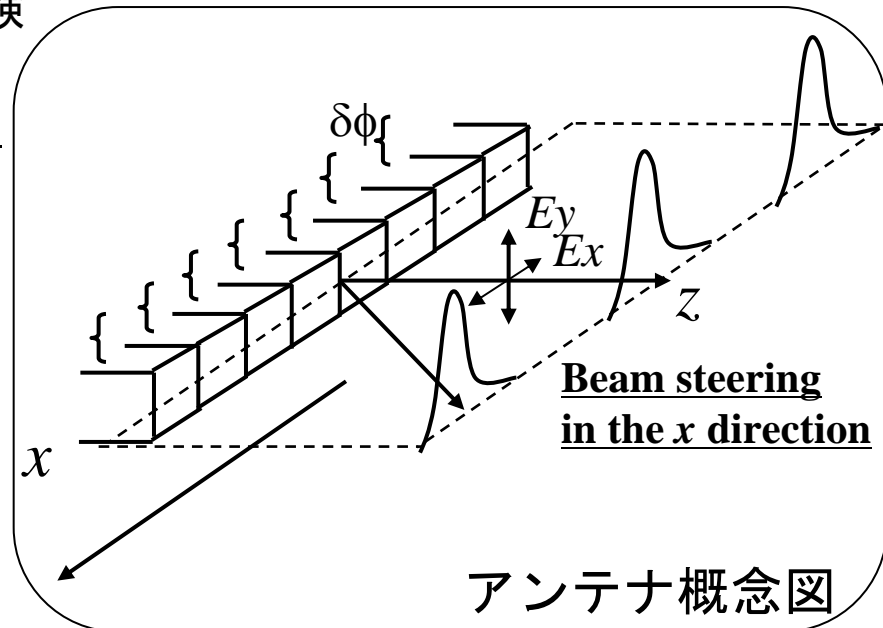
平成18年度:概念設計、高周波設計

平成18年度:低電力仕様での試作、動作確認

平成19年度:新規 CPD アンテナ 製作

平成19年度:QUEST アンテナの詳細設計
(熱設計を含む)

平成19~20年度:QUEST アンテナの製作



EBWCD

Experimental Observations

- 100kA at 60 GHz 600kW on COMPASS-D
- 15kA at 5 GHz 200kW on LATE
- 4 kA at 8.2GHz 170 kW on TST-2
- 1.2 kA at 140 GHz on W7-AS

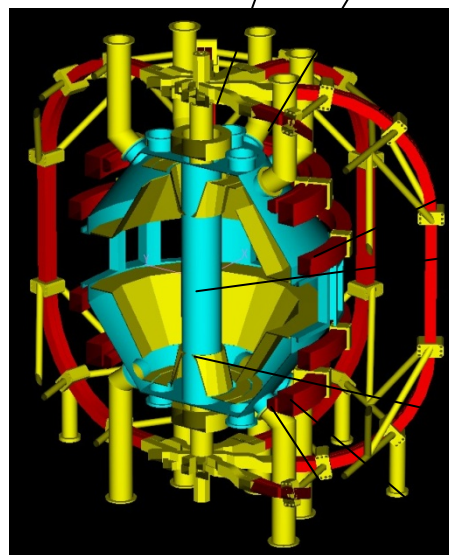
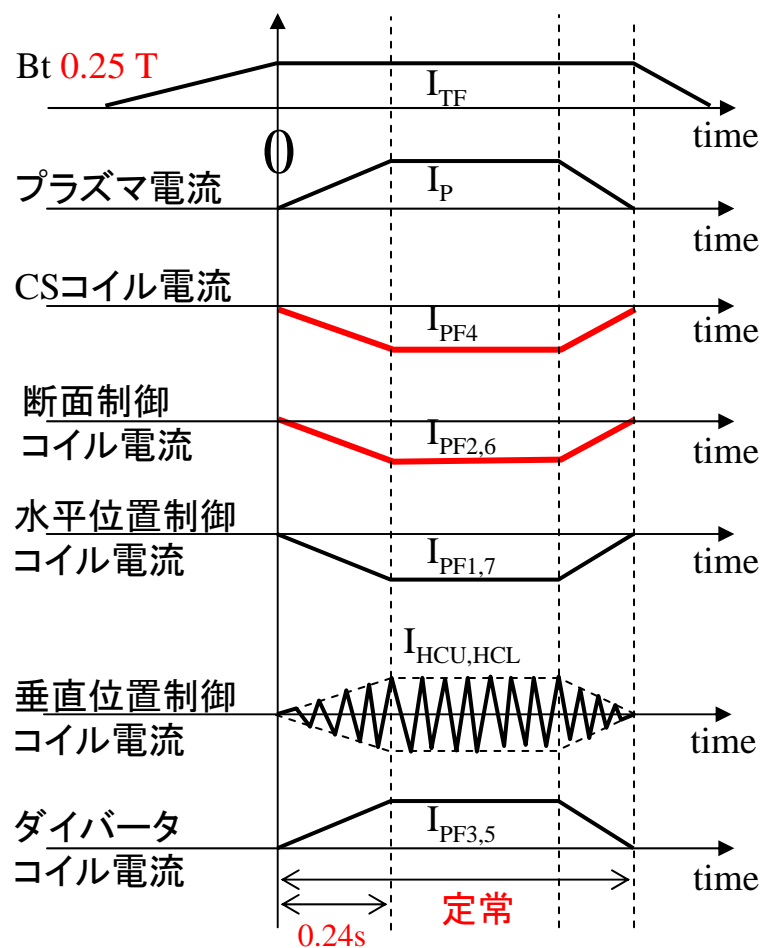
Simulation

- 30kA at 15 GHz, 1MW on NSTX, but no optimization

- EBWCD in ST has the potential to attain the high current drive efficiency comparable to ECCD on conventional tokamaks.
- Even in ST, wave propagation of EBW has no limitations such as cut-off.
- The collaboration with LATE group will start in 2005.

磁場コイル電源の活用(定常運転時)

TRIAM-1Mの磁場コイル電源を活用する。
 新設の磁場コイル電源は定常運転を重視する。



PF3-1コイル電源
 (旧SPコイル電源)

PF3-2コイル電源
 (旧SNコイル電源)

トロイダル磁場コイル電源
 (平成19年度納入予定)

PF1,7コイル電源
 (平成19年度調達)

PF4-2コイル電源
 (旧CTコイル電源)

PF4-1,4-3コイル電源
 (平成18年度納入予定)

PF2,6コイル電源
 (旧BH-FBコイル電源)

HCU,Lコイル電源
 (旧BH-FB(1)コイル電源)

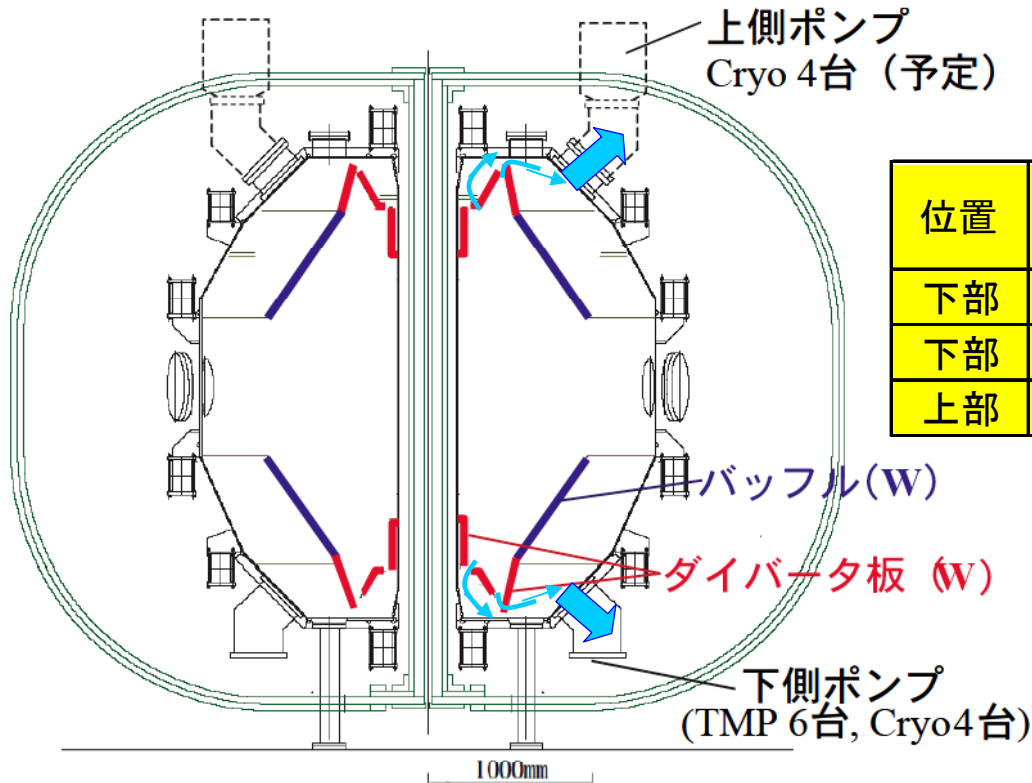
NBCD

TRIAM Advanced Fusion Research Center

- 40keV NB can be deposited at $3 \times 10^{19} \text{m}^{-3}$.
- Plasma current of 100kA can be expected by 40keV 2MW NBI.
- There are no NBI in Kyushu University at present.
- Bootstrap current is not sufficient to maintain the plasma current in steady state.

Particle exhaust (divertor pumping)

TRIAM Advanced Fusion Research Center



位置	ポンプ	単体排気速度 $\text{m}^3/\text{s}(\text{H}_2)$	台数	総排気速度 $\text{m}^3/\text{s}(\text{H}_2)$
下部	TMP	~2.3	6	13.8
下部	CRYO	10	4	40
上部	CRYO	10	4	40

(上部排気に関しては設置予定)

Steady state operation
 $P=0.1$ (Pa)
 $\Rightarrow 9.4$ (Pa m^3/s)

Pulse operation
 $P=1$ (Pa)
 $\Rightarrow 94$ (Pa m^3/s)

Outline of divertor (under consideration of best position of poloidal field coils)

Thermal desorption of D from W

Twall = 300C

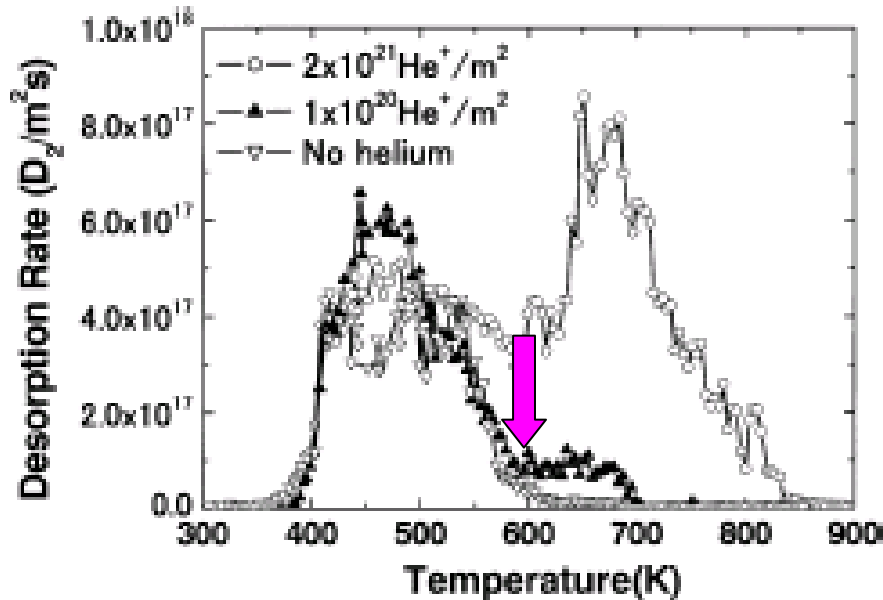


Fig. 1. Thermal desorption spectra of deuterium for samples without pre-irradiation and with pre-irradiation of 8 keV-He⁺ to doses of 1.0×10^{20} and 2.0×10^{21} He⁺/m² at room temperature.

He – irradiation
D-Fluence

Twall = 600C

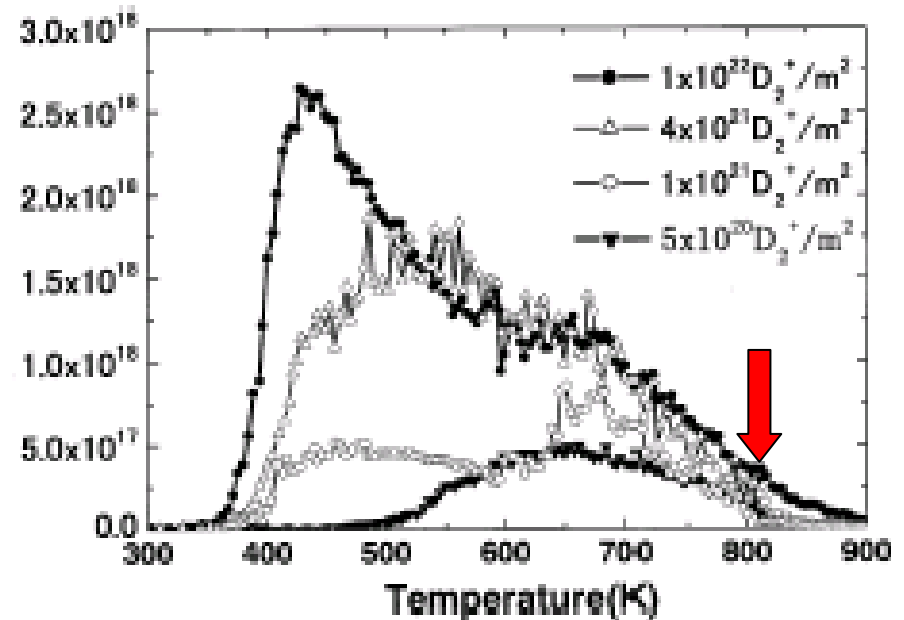


Fig. 2. Thermal desorption spectra of deuterium for tungsten irradiated with 8 keV-He⁺ to 2×10^{21} He⁺/m² at room temperature for deuterium doses ranging from 5×10^{20} to 10^{22} D₂⁺/m² introduced at room temperature.