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## 1 Introduction

This documentation is for **task3d-a** (integrated transport analysis suite for LHD experiment). There is a mailing list for users and developers of task3d-a. If you want to join, please contact M.Yokoyama (yokoyama @ LHD.nifs.ac.jp).

Its first version, **task3d-a01**, was introduced at the LHD Experiment Group Meeting in 24 September 2012, and documented with this material.

The names of the contact person on each module (Sec. 3) are given for detailed consultation if required. It should be noted that those names are not necessarily those of developers.

## 2 TASK3D-a Usage

task3d-a can be executed in one of two ways:

1. Remote desktop connection to ***tmap-task3d.lhd.nifs.ac.jp***
2. Mount the drive: ***T:¥¥trsnaphd1.lhd.nifs.ac.jp***  
(For execution of the program a windows PC must be used.)

ID: trsnap

password: trsnap

These machines can only be reached from ***within the LHD Experiment LAN***. When off-site, connections can be made by using a VPN connection.

### 2.1 Standard usage

- double click: pwwave.bat
- go, <shot#>

This will begin calculations using the standard settings, then automatically register the results with the eg system.

***The contents of go.pro should NOT be modified.***

The options explained below should NOT be used with the “go” command; using the default settings ensures that the calculation results registered with in **eg** use the same settings regardless of who initiates the task3d-a suite.

### 2.2 Personalized usage

- create your own directory at T: using your name (e.g. yokoyama).
- copy go-noreg.pro and pwwave.bat to your own directory
- double click: pwwave.bat
- go-noreg, <shot#>

**go-noreg.pro** does not perform eg-registration. The results including eg-format files are written out under your own directory. Thus, the contents of go-noreg.pro can be modified for your own purpose. The options explained below can be used.

## 2.3 Available options for personalized use

**time=[time1, time2, time3,,,,, ]**

(seconds)

Calculations will be done only at the specified time(s).

This will **override** the default timing settings.

(ex: time=[4.5, 4.633, 4.6, 5.8] → only these timings are calculated)

If this option is not set, calculations will be done for every time where the strong Thomson lasers are active.

**add\_time=[time1, time2, time3,,,,, ]**

(seconds)

Time(s) given will be **added** to the default calculation times (times with strong Thomson lasers)

(ex: add\_time=[4.5, 4.633, 4.6, 5.8] → default timings + add\_time)

If both the “time” and “add\_time” options are set, then all then given times will be used (no defaults).

### **cxs**

Ti profile from cxs7 is prepared as ti\_<#shot>t<time>.txt, and it is used for fit3d calculations. Otherwise, Ti=Te is employed for fit3d calculations. See, explanations for fit3d module.

**delay=[time]**

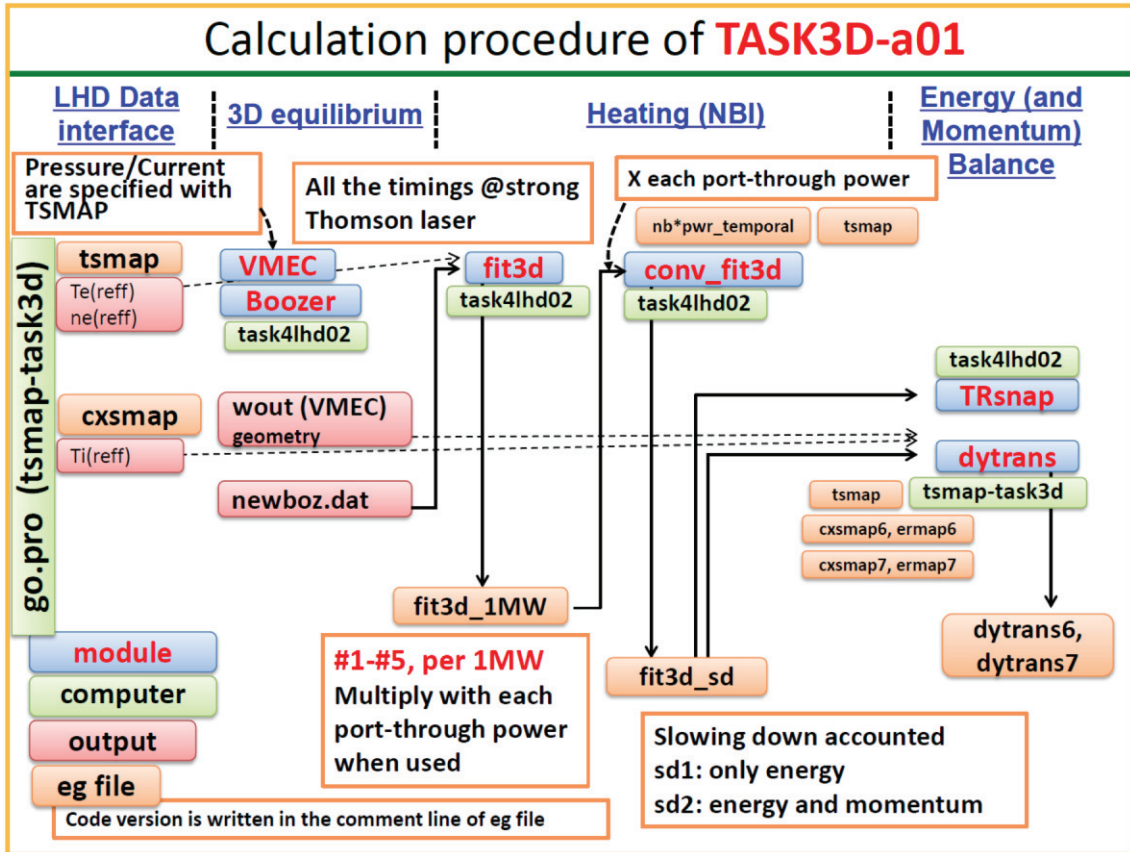
(seconds)

Specifies the duration for the task3d-a calculations to be performed after turning-off the NBI. This only has an effect if default timings are used (or add\_time).

Default value is 1.0 s.

Brief description for each module is given in Section 3 with the name of contact person.

Figure 1



### 3 Description on modules employed in task3d-a

#### 3.1 VMEC

Y.Suzuki

**VMEC2000\_6.90** is employed in task3d-a01. It calculates MHD equilibrium (fixed boundary calculation). The VMEC equilibrium database (VMEC-DB) for TSMAP has been prepared with VMEC2000\_8.0 by Y.Suzuki. Details for TSMAP can be found in Ref. [1]. The equilibrium solution used for each requested time slice is re-calculated by utilizing parameters of so-called "best-fit" TSMAP.

##### 3.1.1 Input

Inputs used for VMEC calculation:

- Last closed flux surface ( $R_{mn}$  and  $Z_{mn}$ ): taken from VMEC-DB corresponding to  $a_{99}$ . Here,  $a_{99}$  is the minor radius in which 99% of the total stored energy is confined.
- Pressure profile:  $p_0$  (peak beta value) and  $p_f$  (pressure peaking factor) are taken from "best-fit" TSMAP. These 2 values provide the functional form of pressure ("am" in the namelist). If  $a_{99}$  differs from the one corresponding to the minor radius in the VMEC-DB (say,  $a_{DB}$ ),  $\psi = (r/a_{99})^2$  is approximately used, instead of  $\psi = (r/a_{DB})^2$ .
- Current profile: "curtor" is provided with **eg: ip**. As for a profile, it is assumed to be proportional to  $1-\psi^2$ .

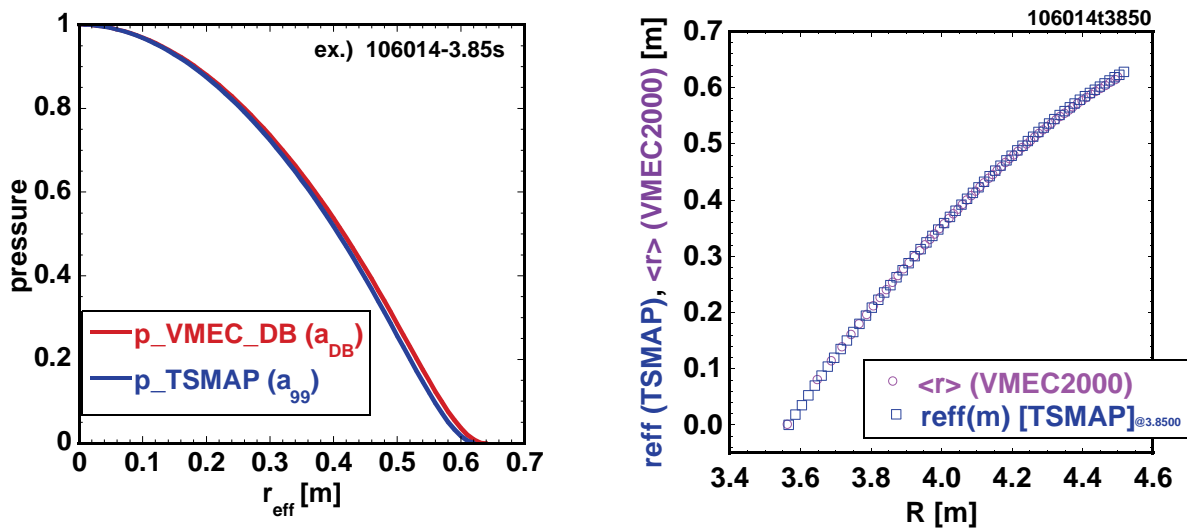
- “phiedge” is provided by  $\text{phiedge0} \cdot (a_{99}/a_{DB})^2$ , where  $\text{phiedge0}$  is the toroidal flux for a vacuum case in VMEC-DB. If  $\text{phiedge0}$  and  $a_{DB}$  do not exist in VMEC-DB (such as for  $R_{ax}=3.53\text{m}$ ), interpolation is performed with available data.
- The default setting for calculation conditions is as follows  
 $ns=61, nu=32, nv=32, mu=8, mv=6, (u = \text{theta}, v = \text{zeta}), \text{ftol}=1.e-15$

The VMEC input file can be found in the directory:

T:\¥equilibrium¥XXXXXXXX¥XXXXXXXXtYYYY

Since the “best-fit” TSMAP is defined by just satisfying “Thomson peak ( $T_{e,max}$ ) to the magnetic axis” and “in-out symmetry”, it does not necessarily mean all of the equilibrium properties are well reproduced. Thus, it should be considered that this approach is just one of practical approaches for providing equilibrium for experimental analysis. The “wout” file (produced by VMEC) can be replaced by that based on other equilibrium reconstruction approach to see/investigate the impact of equilibrium on the analyses.

Below, an example is shown on the comparison between the “best-fit” TSMAP ( $a_{99}\sim 0.62\text{m}$ ) and VMEC-DB ( $a_{DB}\sim 0.63\text{m}$ ) for a particular shot-timing.  $p\_TSMAP$  is given to the input of VMEC2000. The approximation,  $\psi=(r/a_{99})^2 \sim \psi=(r/a_{DB})^2$ , provides little impact on the mapping between  $r_{eff}$  (TSMAP),  $\langle r \rangle$  (VMC calc.) and  $R$ .



### 3.1.2 Output

The VMEC output files can be found in the directory:

T:\¥equilibrium¥XXXXXXXX¥XXXXXXXXtYYYY

**wout:** standard output generated from VMEC2000. The variables written out in this file depends on the version, and it is currently ver6.90.

**threed1:** fundamental information (calculation evolution towards convergence, some equilibrium quantities etc.) are available.

**dia08**: it was a standard output in old versions of VMEC. It is also written out to be usable to some codes to read dia8 in previous days.

## 3.2 Boozer

### M. Yokoyama

*newboz* performs the mapping from VMEC coordinated to Boozer coordinates, so that equilibrium is described in Boozer coordinates.

#### 3.2.1 Input

The input is the VMEC wout file.

The default settings for mapping are as follows:

```
m_nbz = 64
nmax_nbz = 20
nmin_nbz = -20
ltsmap = .t.
lhs_to_rhs = .f.
nit_to_pit = .f.
vel_to_hel = .f.
```

- ***ltsmap*** was introduced to be compatible with VMEC-DB, where phiedge is given by negative value.

```
(in transform.f90)
!MY----- TSMAP -----
      if( ltsmap ) then
!MY -- ltsmap
! reversal of only wjs and wis (from original psi<0 -> psi>0 part)
      do i = 2, ns
        wjs(i) = -wjs(i)
        wis(i) = -wis(i)
      end do
! reversal of xiota, wjs, xnboz and pbozh (same as original iota<0 -> iota>0
part)
      do i = 2, ns
        xiota(i) = - xiota(i)
        wjs (i) = - wjs (i)
      end do
      do m = 1, nmboz
        xnboz(m) = - xnboz(m)
        do i = 2, ns
          pbozh(m,i) = - pbozh(m,i)
        end do
      end do
      print 1000
    endif
1000 format(/1x,' -----'
          /1x,'   transformation (TSMAP) done   '
          /1x,' -----'/)
      return
    endif
!MY---- TSMAP -----
```

#### 3.2.2 Output

The newboz output files can be found in the directory:

T:\equilibrium\XXXXXXXX\XXXXXXXXtYYYY

- **newboz\_a\_XXXXXXXXtYYYY.dat**: ascii
- **newboz\_b\_XXXXXXXXtYYYY.dat**: binary
- **newboz\_XXXXXXXXtYYYY.txt**: accuracy of the mapping can be checked by columns under “check of relation between VMEC and Boozer”, where the maximum value of the relative difference of  $B, R, Z, \phi$  between VMEC and Boozer coordinates on each flux surface is written out.

### 3.3 fit3d [2]

**S.Murakami (Kyoto University), R.Seki**

**fit3d** has been developed (“reduced” version of GNET) to evaluate radial profiles of NBI absorbed power, beam pressure, beam source and induced momentum. The calculation consists of three parts as follows.

- HFREYA: calculations of the birth profile (from the generation of the beam particles in the beam source to ionization in the plasma)
- MCNBI: birth-ions are followed (shorter than the energy slowing-down time, but longer than the orbit effects such as prompt loss can be reflected)
- Steady-state solution of Fokker-Plank equation is obtained analytically without orbit effects taken into account

Required inputs

- Density and Temperature profiles: automatically created from `afit_nT_coeff_XXXXXXXXtYYYY.txt` (T:\equilibrium\XXXXXXXX\XXXXXXXXtYYYY). The polynomial form,  $\underline{Y=c0+c1*ra^2+c2*ra^4+c3*ra^6}$  (here  $ra \equiv r_{\text{eff}}/a_{99}$ ), is employed for the fitting. The illustrative comparison with the standard deviation between measured data and the fitting curve is collectively found in `afit_summary_XXXXXXXX.pdf` (T:\equilibrium\XXXXXXXX\XXXXXXXXtYYYY) for all the timings. There, the standard deviation for fitting are written out, and “Te(or ne)<0 points” is remarked if the fitting raises temperature and/or density values <0.  
3D equilibrium (Boozer): made by boozer module: specified by “newboz\_file”.

NB.)

- Ti is not always measured for selected timings by default in task3d-a01 (@strong Thomson lasers). Thus, Ti=Te is assumed for a standard use of task3d-a01 (based on known rather weak impacts of Ti on the deposition properties)
- eg file is written by assuming Port-through power to be 1 MW for each beam line

#### 3.3.1 Input

Cf., Appendix

[a part in `input.trsnap_XXXXXXXXtYYYY.txt` (T:\trsnap\XXXXXXXX\XXXXXXXXtYYYY)]

#### 3.3.2 Output

**eg: fit3d\_1MW**

DimNo=3

time [s]

# of beam line	
reff/a99	
ValNo=17	
P_all [MW/m <sup>3</sup> ]:	total absorbed power
P_e [MW/m <sup>3</sup> ]:	absorbed power to electrons
P_i [MW/m <sup>3</sup> ]:	absorbed power to ions
Q_all [W]:	volume-integrated total absorbed power
Q_e [W]:	volume-integrated absorbed power to electrons
Q_i [W]:	volume-integrated absorbed power to ions
B_com [cm <sup>-3</sup> ]:	beam component density
com_per [Jcm <sup>-3</sup> ]:	perpendicular pressure of beam component
com_par [Jcm <sup>-3</sup> ]:	parallel pressure of beam component
en_perp [J]:	perpendicular energy of beam component
en_para [J]:	parallel energy of beam component
cur_dens [Acm <sup>-3</sup> ]:	beam current density
current [A]:	volume-integrated beam current
S [1/(s cm <sup>3</sup> )]:	beam source density
total_S [1/s]:	volume-integrated beam source
mom_e [kgm/s <sup>2</sup> cm <sup>-3</sup> =Ncm <sup>-3</sup> ]:	momentum input density to electrons
mom_i [kgm/s <sup>2</sup> cm <sup>-3</sup> =Ncm <sup>-3</sup> ]:	momentum input density to ions

### 3.4 conv\_fit3d

M. Osakabe, H.Lee

**conv\_fit3d** has been developed to evaluate the NBI absorbed power and induced momentum by taking the beam slowing down (SD) effect into account, based on **eg: fit3d\_1MW** (which does not include SD).

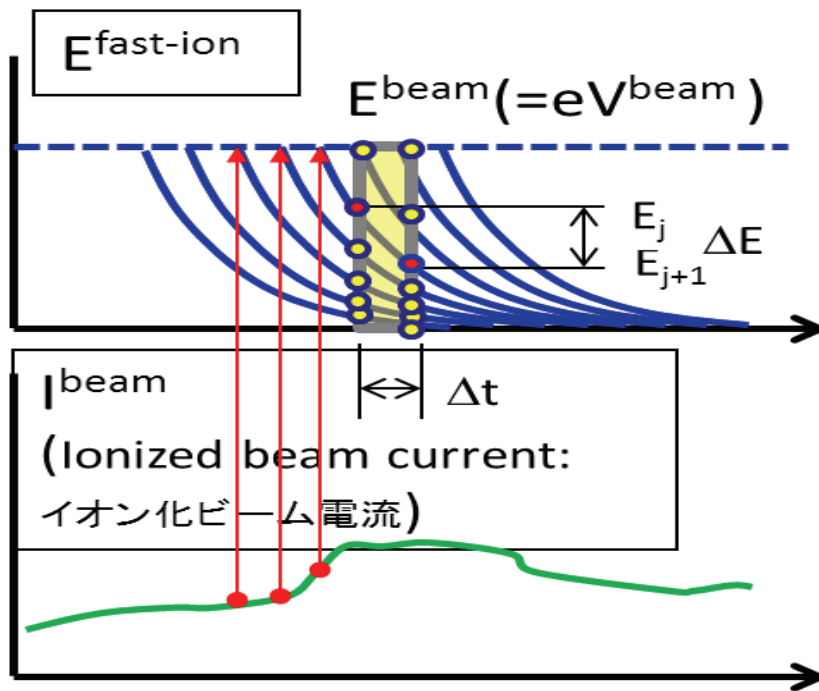
- It is assumed that the ions with the injection energy ( $E_{inj}$ ) are produced with typically  $\Delta t=100\text{ms}$  (corresponding to the interval of selected timings at fit3d calculations) during NBI injection. Those ions are followed until their energy becomes zero. Heating power is evaluated with considering ions with energy above  $T_i(=T_e)$ .
- Slowing down process for ions with  $E_{beam}$  at each timing is evaluated.
- Suffix j indicates that ions were injected at "j-th" previous time-steps from  $t_i$ . Thus, the ion energy injected at  $t=t_i$  is expressed by  $E_{i,0}(=E_{beam})$ . In a similar way, ion energy expressed by  $E_{i,j}$  at  $t=t_i$  is denoted by  $E_{i+1,j+1}$  at the next timing,  $t=t_{j+1}$ .
- Relationship between  $E_{i,j}$  at  $t=t_i$  and its energy at the next time-step,  $E_{i+1,j+1}$  at  $t=t_{j+1}$  is deduced from

$$E_{i+1,j+1} = \left[ E_{i,j}^{3/2} \exp\left(-\frac{3\Delta t}{\tau_{se}}\right) - E_c^{3/2} \left\{ 1 - \exp\left(-\frac{3\Delta t}{\tau_{se}}\right) \right\} \right]^{2/3}$$

- Heating power within 1 time-step is calculated by the sum of  $\Delta E_{i,j}=E_{i,j}-E_{i+1,j+1}$  by weighting the ionized beam current,  $I_{i,j}^{beam}$ .

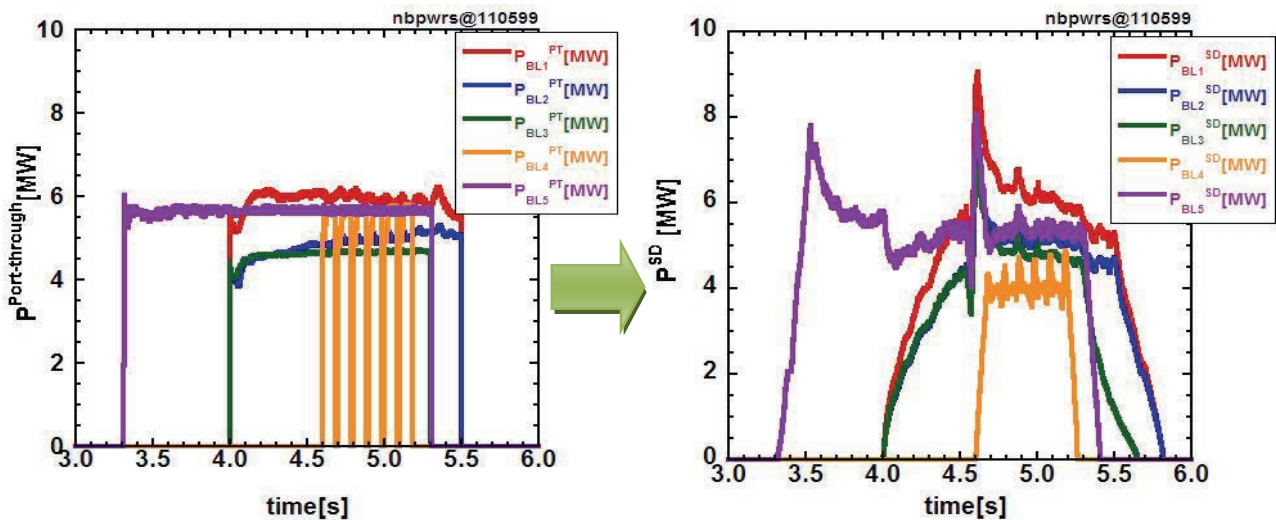
This evaluation process is schematically shown below.





A particular example (calculated for #110599, pellet@~4.55s) is shown below.

- Temporal change of the density and temperature is taken into account (through dataset of sequential fit3d\_1MW).
- Energy slowing down time is evaluated with the density and temperature @  $r_{\text{eff}}/a_{99}=0.5$ .
- SD-Momentum is evaluated in a similar way.



### 3.4.1 Input

Sequential series (typically with  $\Delta t=100\text{ms}$ ) of **eg: fit3d\_1MW**, and **eg: tsmap, nb1pwr\_temporal, nb2pwr\_temporal, nb3pwr\_temporal, nb4apwr\_temporal, nb4bpwr\_temporal, nb5apwr\_temporal, nb5bpwr\_temporal**

### 3.4.2 Output

**eg: fit3d\_sd** (slowing down)

DimNo=3  
time [s]

# of beam line (1-5)

reff/a99

ValNo=23

Pfit3d [MW/m<sup>3</sup>]: total absorbed power (**SD is not taken into account**)  
 [= (P\_all in eg:fit3d\_1MW)\*(Port-through power)]

P\_all [MW/m<sup>3</sup>]: total absorbed power with **SD taken into account**

P\_e [MW/m<sup>3</sup>]: absorbed power to electrons with SD taken into account

P\_i [MW/m<sup>3</sup>]: absorbed power to ions with SD taken into account

Q\_all [W]: volume-integrated total absorbed power

Q\_e [W]: volume-integrated absorbed power to electrons

Q\_i [W]: volume-integrated absorbed power to ions

Cf\_tot: correction factor for the total absorbed power  
 [Total absorbed power: SD/no-SD]

Cf\_e: correction factor for the absorbed power to electrons  
 [Absorbed power to electrons: SD/no-SD]

Cf\_i: correction factor for the absorbed power to ions  
 [Absorbed power to ions: SD/no-SD]

B\_com [cm<sup>-3</sup>]: beam component density (as it is in eg:fit3d\_1MW)

com\_per [J/cm<sup>3</sup>]: perpendicular pressure of beam component (as it is in eg:fit3d\_1MW)

com\_par [J/cm<sup>3</sup>]: parallel pressure of beam component (as it is in eg:fit3d\_1MW)

en\_perp [J]: perpendicular energy of beam component (as it is in eg:fit3d\_1MW)

en\_para [J]: parallel energy of beam component (as it is in eg:fit3d\_1MW)

cur\_dens [A/cm<sup>3</sup>]: beam current density (as it is in eg:fit3d\_1MW)

Current[A]: volume-integrated beam current (as it is in eg:fit3d\_1MW)

S [1/(s cm<sup>3</sup>)]: beam source density (as it is in eg:fit3d\_1MW)

total\_S [1/s]: volume-integrated beam source (as it is in eg:fit3d\_1MW)

mom\_SS [kg/m<sup>2</sup>s<sup>2</sup>=N/m<sup>3</sup>]: momentum input without SD taken into account  
 = ( mom\_e+mom\_i) in eg:fit3d\_1MW ) \* (Port-through power)]

mom\_SD [kg/m<sup>2</sup>s<sup>2</sup>=N/m<sup>3</sup>]: momentum input with SD taken into account

F\_SS [N]: volume-integrated momentum input (without SD taken into account)

F\_SD [N]: volume-integrated momentum input (with SD taken into account)

### 3.5 TRsnap [3]

R.Seki, original: TASK/TR (A.Fukuyama, Kyoto University)

$$\frac{1}{V'} \frac{\partial(n_e V')}{\partial t} = -\frac{1}{V'} \frac{\partial}{\partial \rho} (V \Gamma_j) + S_j$$

$$\frac{1}{V'^{5/3}} \frac{\partial}{\partial t} \frac{3}{2} (n_j T_j V'^{5/3}) = -\frac{1}{V'} \frac{\partial}{\partial \rho} (V' Q_j) + P_j \quad V' = dV / d\rho, \quad \rho \equiv r_{\text{eff}} / a_{99}$$

$$Q_j = -\langle |\nabla \rho|^2 \rangle \chi_j n_j \frac{\partial T_j}{\partial \rho} + \langle |\nabla \rho \rangle u_j n_j T_j + \frac{3}{2} \Gamma_j T_j$$

$$\Gamma_j = -\langle |\nabla \rho|^2 \rangle D_j \frac{\partial n_j}{\partial \rho} + \langle |\nabla \rho \rangle u_j n_j$$

$$P_e = -\frac{n_e T_e}{\tau_{ei}} + \frac{n_i T_i}{\tau_{ie}} + P_{in,e} = P_{ie} + P_{in,e}$$

$$P_i = \frac{n_e T_e}{\tau_{ei}} - \frac{n_i T_i}{\tau_{ie}} + P_{in,i} = P_{ei} + P_{in,i}$$

$$\chi_j = -\frac{\int P_j \rho dV' - \langle |\nabla \rho \rangle u_j n_j T_j - \frac{3}{2} \Gamma_j T_j}{\langle |\nabla \rho|^2 \rangle n_j \frac{\partial T_j}{\partial \rho}}$$

**TRsnap** has been modified based on TASK/TR (A.Fukuyama) to evaluate steady-state energy balance.

NB.) currently (in task3d-a01),

- $P_{in,e(i)}$  is evaluated just from FIT3D (NBI). ECH and ICH have not been available. Other losses (=negative contribution, like radiation loss) have not been included.
- For  $\chi_j$ , only the first term of denominator is considered.
- 3/2 in energy-transfer term.

### 3.5.1 Input

```
[a part in input.trsnap_XXXXXXtYYYY.txt (T:\trsnap/XXXXXX/XXXXXXtYYYY)]
&fit3dparam
ipg=0:                ion species (0: H, 1: He, 2: Ne)
npart=103000:        default is 8000, varied for extreme low density cases (like EGAM shots)
                    so as to be npart~ 1.28*1023/n0[m-3]-43000 (based on advice from R.Seki)
cn0=1.0e16:          edge neutral density: n0=cn0*exp[-(1-ra)/0.1], ra≡reff/a99
newboz_comp='local'
newboz_file='T:\equilibrium\109027\109027t5800\newboz_b_109027t5800.dat'
inbi1='on'
enbi1= 0.0000, pnbi1= 1.0000
                    enbi* : read from eg: nb*pwr_temporal (zero for no injection)
                    pnbi* : all set for 1 MW (for eg: fit3d_1MW)

inbi2='on'
enbi2= 0.0000, pnbi2= 1.0000
inbi3='on'
enbi3=176.4790, pnbi3= 1.0000
inbi4='on'
```

### 3.5.2 Output

The results are written out at the directory: T:\trsnap/XXXXXX/XXXXXXtYYYY with the suffix as follows (with/without SD)

- **\_SS** : deposition power without SD consideration (eg:fit3d\_1MW x Pport-through for each beam line) is used for energy balance.
- **\_sd** : deposition power with SD consideration (eg:fit3d\_sd) is used for energy balance.

**tr\_snap\_XXXXXXtYYYY.113** (T:\trsnap/XXXXXX/XXXXXXtYYYY)

```
# NR :                radial mesh number
rho:                  reff/a99
chi_e_exp [m2/s]:     $\chi_e$ 
chi_i_exp [m2/s]:     $\chi_i$ 
ne [1020 m-3]:        electron density
ni [1020 m-3]:        ion density (=ne, at this moment)
Te [keV]:             electron temperature
Ti [keV]:             ion temperature
Pin_e [MW/m3]:        power input density to electron (currently only NBI)
Pin_i [MW/m3]:        power input density to ion (currently only NBI)
heat_flux_e [MW/m2]:  electron energy flux
heat_flux_i [MW/m2]:  ion energy flux
heat_flux_in_e [MW/m2]: electron energy flux (corresponding only to heating source such as NBI)
heat_flux_in_i [MW/m2]: ion energy flux (corresponding only to heating source such as NBI)
inte_Pe [MW]:         volume-integrated Pe
inte_Pi [MW]:         volume-integrated Pi
inte_Pin_e [MW]:      volume-integrated Pin,e
inte_Pin_i [MW]:      volume-integrated Pin,i
inte_Pie [MW]:        volume-integrated Pie
inte_Pei [MW]:        volume-integrated Pei (=inte_Pie)
dTe/drho:             electron temperature gradient
```

dTi/drho: ion temperature gradient  
 dne/drho: electron density gradient  
 dni/drho: ion density gradient  
 <lnabla rho>:  $\langle |\nabla\phi| \rangle$   
 <lnabla rho^2>:  $\langle |\nabla\phi|^2 \rangle$   
 dV/drho:  $dV/d\rho(=V')$   
 inte\_Pin\_e\_nbi1 [MW]: volume-integrated deposited power to electron and ion from NBI#1-5  
 inte\_Pin\_i\_nbi1 [MW]  
 inte\_Pin\_e\_nbi2 [MW]  
 inte\_Pin\_i\_nbi2 [MW]  
 inte\_Pin\_e\_nbi3 [MW]  
 inte\_Pin\_i\_nbi3 [MW]  
 inte\_Pin\_e\_nbi4 [MW]  
 inte\_Pin\_i\_nbi4 [MW]  
 inte\_Pin\_e\_nbi5 [MW]  
 inte\_Pin\_i\_nbi5 [MW]

## 3.6 Dytrans [4]

H.Lee, K.Ida, M.Yoshinuma

**dytrans** evaluates “dynamic transport”, in which energy flows due to the temporal variation of plasma profiles are also taken into account.

### 3.6.1 Input

**eg: fit3d\_sd, cxsmmap6(7), tsmmap, [ermap6(7), if exists]**

### 3.6.2 Output

**eg: dytrans6\_sd or dytrans7\_sd** (using cxs6 or cxs7)  
 (due to the faster temporal resolution in cxs6 that cxs7, dytrns6\_sd is appropriate)

DimNo = 2  
 Time [s]  
 R [m]  
 ValNo = 88

reff [m]: minor radius  
 rho: reff/a99

Ti [keV]: ion temperature  
 Ti\_fit [keV]: ion temperature profile fitted with polynomial function  
 Tier [arb]: error of ion temperature  
 Te [keV]: electron temperature  
 Te\_fit [keV]: electron temperature profile fitted with polynomial function  
 Vc [km/s]: toroidal rotation velocity  
 Vcer [arb]: error of toroidal rotation velocity  
 <Er> [kV/m]: flux-averaged radial electric field  
 Ne [ $10^{19} \text{ m}^{-3}$ ]: electron density  
 Ne\_fit [ $10^{19} \text{ m}^{-3}$ ]: electron density profile fitted with polynomial function

#### Gradient /dR

dTi/dr [keV/m]: dTi/dR  
 dTi/dr\_fit [keV/m]: dTi\_fit/dR  
 dTe/dr [keV/m]: dTe/dR  
 dTe/dr\_fit [keV/m]: dTe\_fit/dR  
 dVc/dr [ $10^3/s$ ]: dVc/dR  
 d<Er>/dr [ $\text{kV/m}^2$ ]: d<Er>/dR

dNe/dr [ $10^{19} \text{ m}^{-4}$ ]: dNe/dR  
dNe/dr\_fit [ $10^{19} \text{ m}^{-4}$ ]: dNe\_fit/dR

Gradient /dreff

dTi/dreff' [keV/m]: dTi/d(reff)  
dTi/dreff\_err [keV/m]  
dTi/dreff\_fit [keV/m]  
dTe/dreff [keV/m]: dTe/d(reff)  
dTe/dreff\_fit [keV/m]  
dVc/dreff [ $10^3$ /s]: dVc/d(reff)  
dVc/dreff\_err [ $10^3$ /s]  
d<Er>/dreff [kV/m<sup>2</sup>]: d<Er>/d(reff)  
dNe/dreff [ $10^{19} \text{ m}^{-4}$ ]: d(ne)/d(reff)  
dNe/dreff\_fit [ $10^{19} \text{ m}^{-4}$ ]

Gradient /drho (rho=reff/a99)

dTi/drho [keV]: dTi/d(rho)  
dTi/drho\_fit [keV]  
dTe/drho [keV]: dTe/d(rho)  
dTe/drho\_fit [keV]  
dVc/drho [km/s]: dVc/d(rho)  
d<Er>/drho [kV/m]: d<Er>/drho  
dNe/drho [ $10^{19} \text{ m}^{-3}$ ]: dne/d(rho)  
dNe/drho\_fit [ $10^{19} \text{ m}^{-3}$ ]

Time derivative terms

dTi/dt [keV/s]: dTi/dt  
dTi/dt\_fit [keV/s]:  
dTe/dt [keV/s]: dTe/dt  
dTe/dt\_fit [keV/s]  
dVc/dt [km/s<sup>2</sup>]: dVc/dt  
d<Er>/dt [kV/(ms)]: d<Er>/dt  
dNe/dt [ $10^{19} \text{ m}^{-3}$ /s]: dne/dt  
dNe/dt\_fit [ $10^{19} \text{ m}^{-3}$ /s]

Wpi [kJ]: volume averaged plasma ion energy with Ti and Ne  
Wpi\_fit [kJ]: volume averaged plasma ion energy with Ti\_fit and Ne\_fit  
Wpe [kJ]: volume averaged plasma electron energy with Te and Ne  
Wpe\_fit [kJ]: volume averaged plasma electron energy with Te\_fit and Ne\_fit

Wpiflx [kJ/m<sup>2</sup>]: Wpi/S(reff)  
Wpiflx\_fit [kJ/m<sup>2</sup>]: Wpi\_fit/S(reff)  
Wpeflx [kJ/m<sup>2</sup>]: Wpe/S(reff)  
Wpeflx\_fit [kJ/m<sup>2</sup>]: Wpe\_fit/S(reff)

Change in heat flux due to the change in temperature and density

delQi/Ne [keV m/s]:  
delQi/Ne\_fit [keV m/s]: with Ti\_fit and Ne\_fit  
delQe/Ne [keV m/s]:  
delQe/Ne\_fit [keV m/s]: with Ti\_fit and Ne\_fit

Heat flux normalized density ion-electron energy exchange included

(QinbioverNe and QexoverNe are not included in the output file)  
Qi/Ne [keV m/s]: QinbioverNe - QexoverNe  
Qi/Ne\_fit [keV m/s]: QinbioverNe\_fit - QexoverNe\_fit  
Qe/Ne [keV m/s]: QinbioverNe + QexoverNe  
Qe/Ne\_fit [keV m/s]: QinbioverNe\_fit + QexoverNe\_fit

Thermal diffusivity (steady state)

Chi\_i [m<sup>2</sup>/s]: (Qi/Ne+delQi/Ne)/(dTi/dreff)  
Chi\_i\_fit [m<sup>2</sup>/s]: (Qi/Ne\_fit+delQi/Ne\_fit)/(dTi/dreff\_fit)

Chi\_e [m<sup>2</sup>/s]: (Qe/Ne+delQe/Ne)/(dTe/dreff)  
Chi\_e\_fit [m<sup>2</sup>/s]: (Qe/Ne\_fit+delQi/Ne\_fit)/(dTe/dreff\_fit)

Heat flux normalized density ion-electron energy exchange included and delta Q/n

Qi/Ne+delQi/Ne [keV m/s]:  
Qi/Ne\_fit+delQi/Ne\_fit [keV m/s]:  
Qe/Ne+delQe/Ne [keV m/s]:  
Qe/Ne\_fit+delQe/Ne\_fit [keV m/s]:

Thermal diffusivity include delta Q

Chi\_i\_dy [m<sup>2</sup>/s]: -(Qi/Ne+delQi/Ne)/(dT/dreff)  
Chi\_i\_dy\_fit [m<sup>2</sup>/s]: -(Qi/Ne\_fit+delQi/Ne\_fit)/(dT/dreff\_fit)  
Chi\_e\_dy [m<sup>2</sup>/s]: -(Qe/Ne+delQe/Ne)/(dTe/dreff)  
Chi\_e\_dy\_fit [m<sup>2</sup>/s]: -(Qe/Ne\_fit+delQe/Ne\_fit)/(dTe/dreff\_fit)

Torque density

P/MiNe [e3 m<sup>2</sup>/s<sup>2</sup>]  
P/MiNe\_fit [e3 m<sup>2</sup>/s<sup>2</sup>]

Perpendicular viscosity

mu\_tor [m<sup>2</sup>/s<sup>2</sup>]  
mu\_tor\_fit [m<sup>2</sup>/s<sup>2</sup>]

Ion heat flux only due to NBI normalized by fitted electron density

QinbioverNe\_fit [keV m/s]

Electron heat flux only due to NBI normalized by fitted electron density

QenbioverNe\_fit [keV m/s]

Ne\_fit normalized ion-electron energy exchange calculated with Ti\_fit, Te\_fit, and Ne\_fit

QexoverNe\_fit [keV m/s]

Temperature ratio

Te/Ti  
Te\_fit/Ti\_fit

Normalized thermal diffusivity

Chi\_i\_dy/Ti<sup>3/2</sup> [m<sup>2</sup>/s/keV<sup>1.5</sup>]  
Chi\_i\_dy/Ti<sup>3/2</sup>\_fit [m<sup>2</sup>/s/keV<sup>1.5</sup>]  
Chi\_e\_dy/Te<sup>3/2</sup> [m<sup>2</sup>/s/keV<sup>1.5</sup>]  
Chi\_e\_dy/Te<sup>3/2</sup>\_fit [m<sup>2</sup>/s/keV<sup>1.5</sup>]

Surface

dV/dreff' [m2]: dV/d(reff) = S(reff) : consistency checked with that in TRsnap

*\_fit : using fitting curve (functional form is same as that for fit3d)*

## References

- [1] C.Suzuki et al., to appear in Plasma Phys. Control. Fusion (2012).
- [2] S. Murakami et al., Trans. Fusion Technol. **27** (1995) 256.
- [3] R.Seki et al., Plasma Fusion Res. **6** (2011) 2402081
- [4] H.Lee, K.Ida et al., to appear in Plasma Phys. Control. Fusion (2012).

## [Appendix] shell and input for fit3d & trsnap

input.trsnap\_XXXXXXtYYYY.txt (T:\trsnap\XXXXXX\XXXXXXtYYYY)

```
&modules  
mod_name[1] = 'fit3d_2010_1'  
mod_name[2] = 'tr_snap_2010'  
&end
```

```

&comp_env
local_work_dir = './work_dir/'
local_code_dir = './bin/'
comp_name[1] = 'task4lhd'
comp_ip[1] = 'task4lhd02.LHD.nifs.ac.jp'
comp_user[1] = 'yokoyama'
comp_work_dir[1] = '/work2/yokoyama/W_W'
comp_code_dir[1] = '/work/seki/TASK4LHD'

local_result_dir = 'T:\trsnap\109027\109027t5800'
plus_name='109027t5800'
&end

&graphic
graphic = 'on'
graphic_file = 'result.ps'
graphic_close='on'
&end

&finalize_process
delete_local_tmp_dir = 'no'
delete_remote_work_dir = 'no'
&end

&t3dparam
B0= 1.38,
rmaj0= 3.75,
ra = 0.59403,
zi=1
&end

&neprof
nepfn='T:\trsnap\109027\109027t5800\ne_109027t5800.txt',
;;nepfun='(ne0-nea)*(1.0-rho**2)+nea', ne0=1.0e1, nea=0.0e-2, ;; (10e19m-3)
&end
Point-series based on fitting
Functional form

&teprof
tepfm='T:\trsnap\109027\109027t5800\Te_109027t5800.txt',
;;tepfun='(te0-tea)*(1.0-rho**2)+tea', te0=3.0e0, tea=0.0e-2,;; (keV)
&end

&zeffprof
zeff=1, zimp=6,
zeffpfm="",
zeff_pfun="", zeff0=2.0, zeffa=2.0,
&end
zeff=2 (radially constant) is assumed by default

&tiprof
tipfn='T:\trsnap\109027\109027t5800\Ti_109027t5800.txt',
;;tipfun="", ti0=1.0e0, tia=1.0e-2,;; (keV)
&end

&timpfprof
timpfpm="",
timpf_pfun="", timp0=1.0e0, timpa=1.0e-2,;; (keV)
&end

&fit3dparam
ipg=0
npart=103000
cn0=0.0
newboz_comp='local'
newboz_file='T:\equilibrium\109027\109027t5800\newboz_b_109027t5800.dat'
inbi1='on'
enbi1= 0.0000, pnbi1= 1.0000
inbi2='on'
enbi2= 0.0000, pnbi2= 1.0000

```

```
inbi3='on'  
enbi3=176.4790, pnbi3= 1.0000  
inbi4='on'  
enbi4= 0.0000, pnbi4= 1.0000  
inbi5='on'  
enbi5= 0.0000, pnbi5= 1.0000  
&end
```

```
&fit3d_output  
fit_data.out = 'no'  
fit_data.out10 = 'yes'  
fit_data.out11 = 'no'  
fit_data.out20 = 'yes'  
fit_data.out21 = 'no'  
fit_data.out30 = 'yes'  
fit_data.out31 = 'no'  
fit_data.out40 = 'yes'  
fit_data.out41 = 'no'  
mcnbi_data.out = 'no'  
data.out6 = 'yes'  
data.out7 = 'yes'  
data.out9 = 'yes'  
data.out15 = 'no'  
data.out20 = 'no'  
data.out21 = 'yes'  
data.out30 = 'no'  
data.out40 = 'no'  
&end
```

```
&tr_snap_param  
nrmax=60  
wout_comp='local'  
wout_file='T:\equilibrium\109027\109027t5800\wout_109027t5800.vmec'  
trparam_file=""  
;;nbi_power_file[1]="  
;;nbi_power_file[2]="  
;;nbi_power_file[3]="  
;;nbi_power_file[4]="  
;;nbi_power_file[5]="  
;;ech_power_file[1]="  
;;ich_power_file[1]="  
;;rloss_file[1]="  
&end
```

**wout**

```
&tr_snap_output  
tr_snap.101='yes'  
tr_snap.102='yes'  
tr_snap.111='yes'  
tr_snap.112='yes'  
tr_snap.113='yes'  
&end
```