

Physics Aspects of the Dynamic Ergodic Divertor (DED)

FINKEN K. Heinz¹, KOBAYASHI Masahiro^{1,2},
ABDULLAEV S. Sadrilla¹, JAKUBOWSKI Marcin^{1,3}

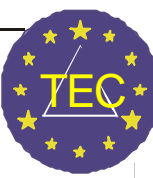
*¹Institut für Plasmaphysik, Forschungszentrum Jülich GmbH, EURATOM
Association,*

D-52425 Jülich, Germany, Partner in the Trilateral Euregio Cluster

*²Department of Energy Engineering and Science, Nagoya University, Nagoya,
Japan*

³University of Opole, Institute of Physics, Opole, Poland





Outline

Motivation, aims

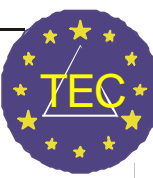
Experimental set-up

Ergodic zone

Laminar zone

Dynamic Aspect

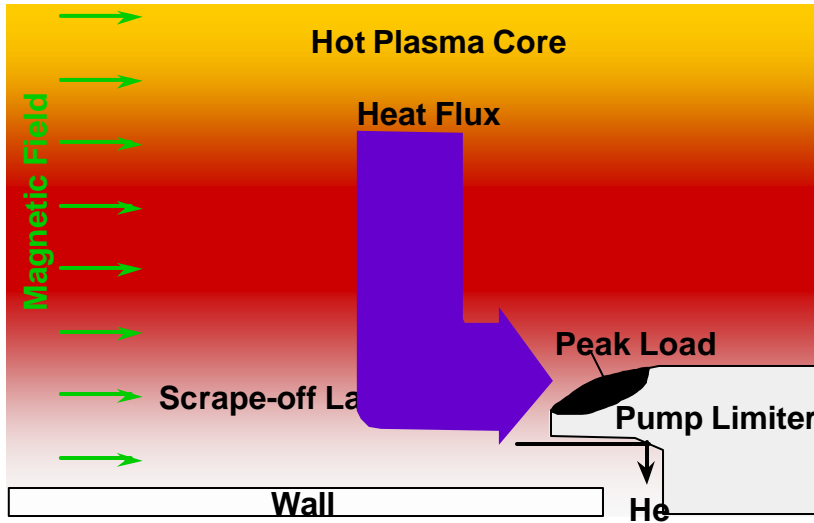




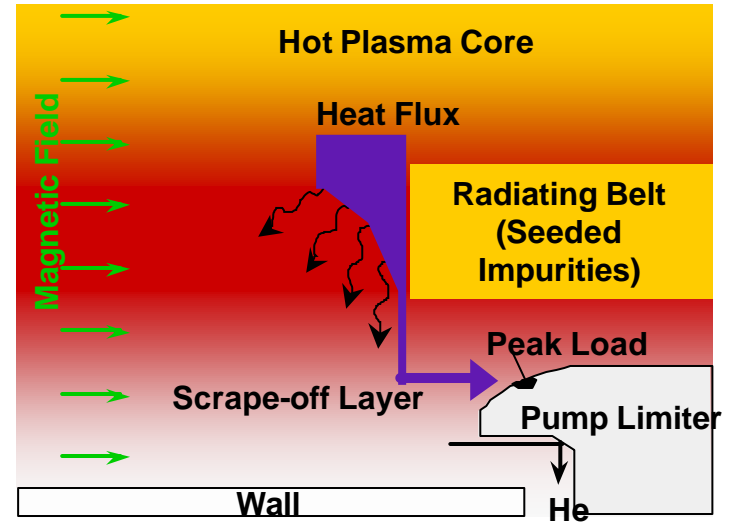
Motivation:

- **The next fusion device (ITER) will have a fusion power of about 1.5 GW**
- **====> 300 MW α -particle heating**
- **This power goes to divertor plates, if plasma edge is not radiatively cooled**
- **Assuming a divertor length of 30 m and a strike point width of 2 x 4 cm ==> power density of 12.5 kW/cm²**
- **For these power fluxes, no technical solutions are known**





Plasma Edge Radiation: too low
 Limiter Heat Load: excessive



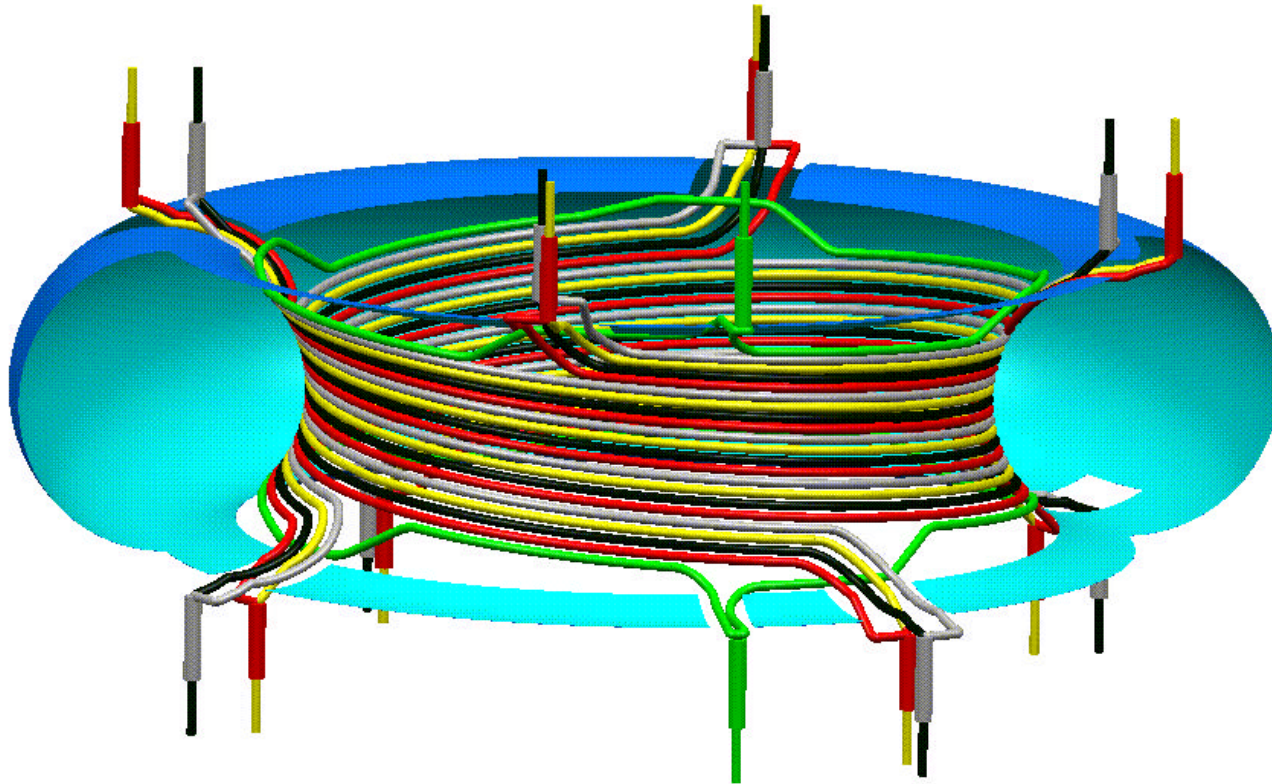
Plasma Edge Radiation: dominating
 Limiter Heat Load: tolerable



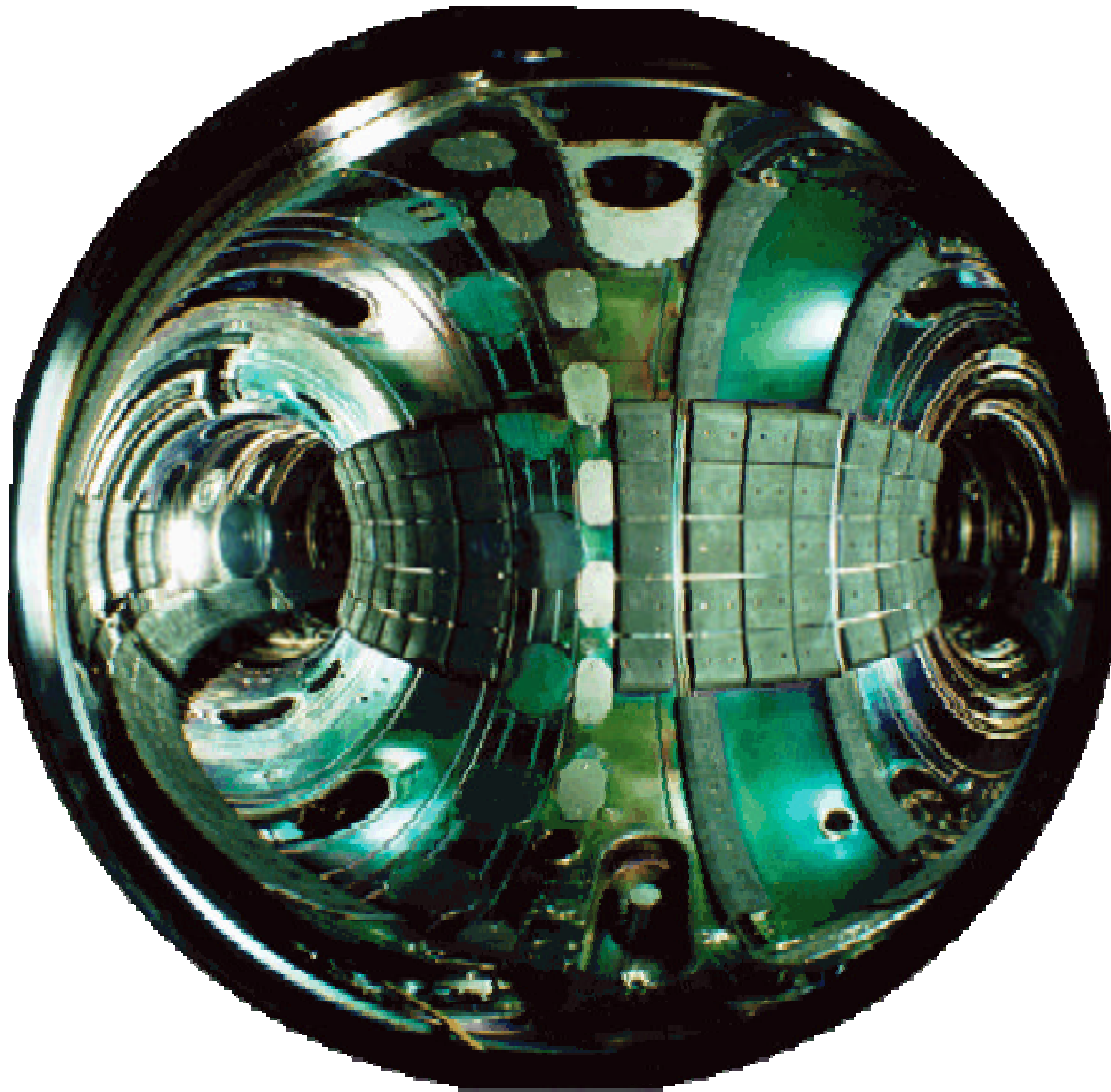
Set-up

- **4 quartets** of perturbation coils plus two compensation coils
- **4 Phases** \implies Rotation of perturbation field
- **f: DC, 50 Hz, band 1 kHz - 10 kHz**
- Arrangement at **HFS** with continuous winding in vessel
- Maximum perturbation current: 15 kA
- Resonance: $q(r_{\text{res}}) = 3$; $r_{\text{res}} = 0.43 \dots 0.46 \text{ m}$ ($a=0.46 \text{ m}$)
- **Base modes:** $m/n = 12/4; 6/2; 3/1$ and mixture of $12/4 + 6/2$

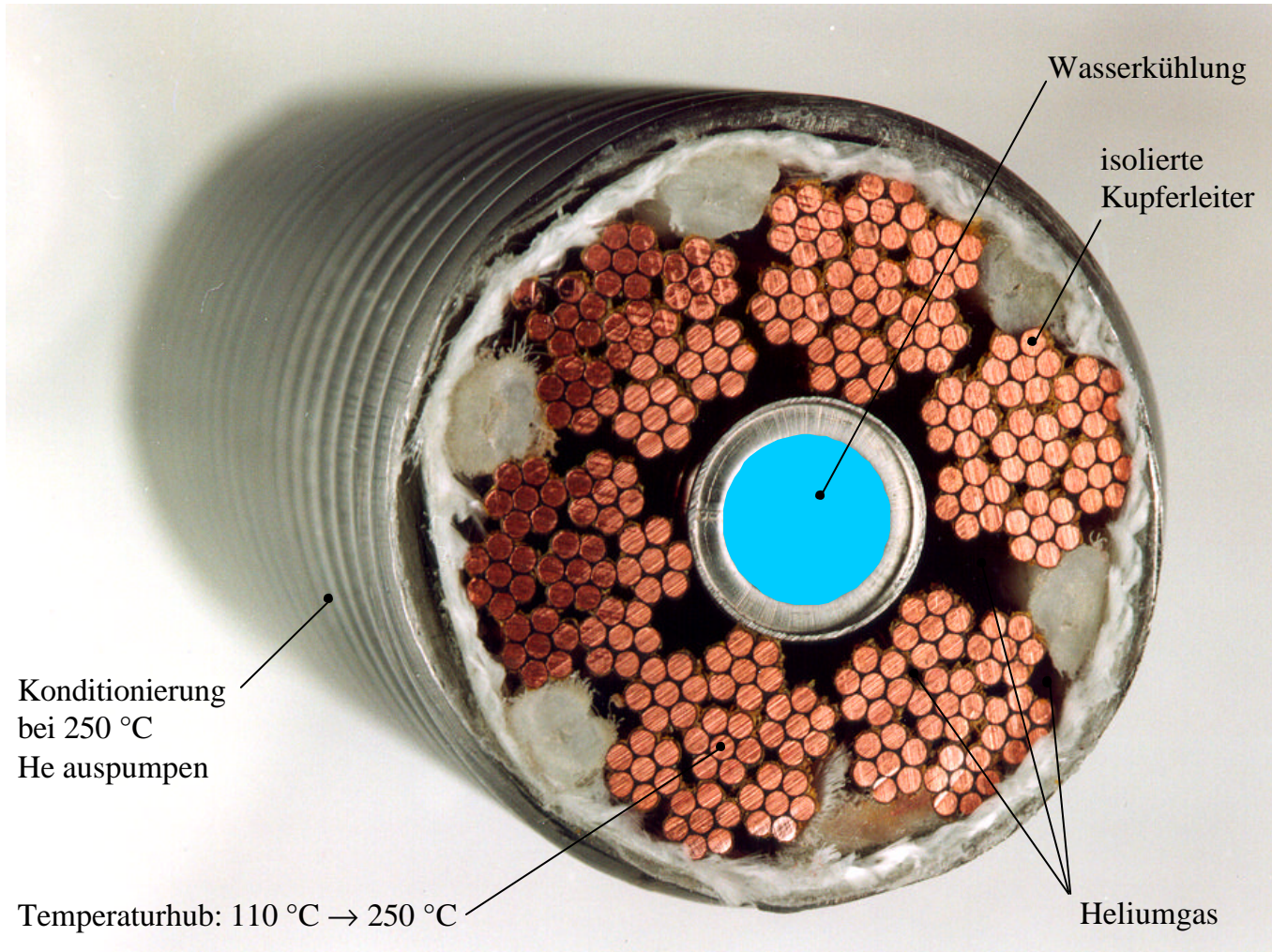




Final coil design



DED - Spulenkühlung





Scientific aims for DED program

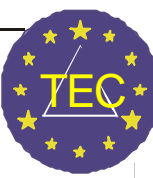
DC-operation

- Comparison to other ergodization experiments
- Optimisation of the radiation belt
- Optimisation of particle exhaust
- Investigation of a helical divertor

Low frequency operation:

- Smearing out of local peaks of heat flux



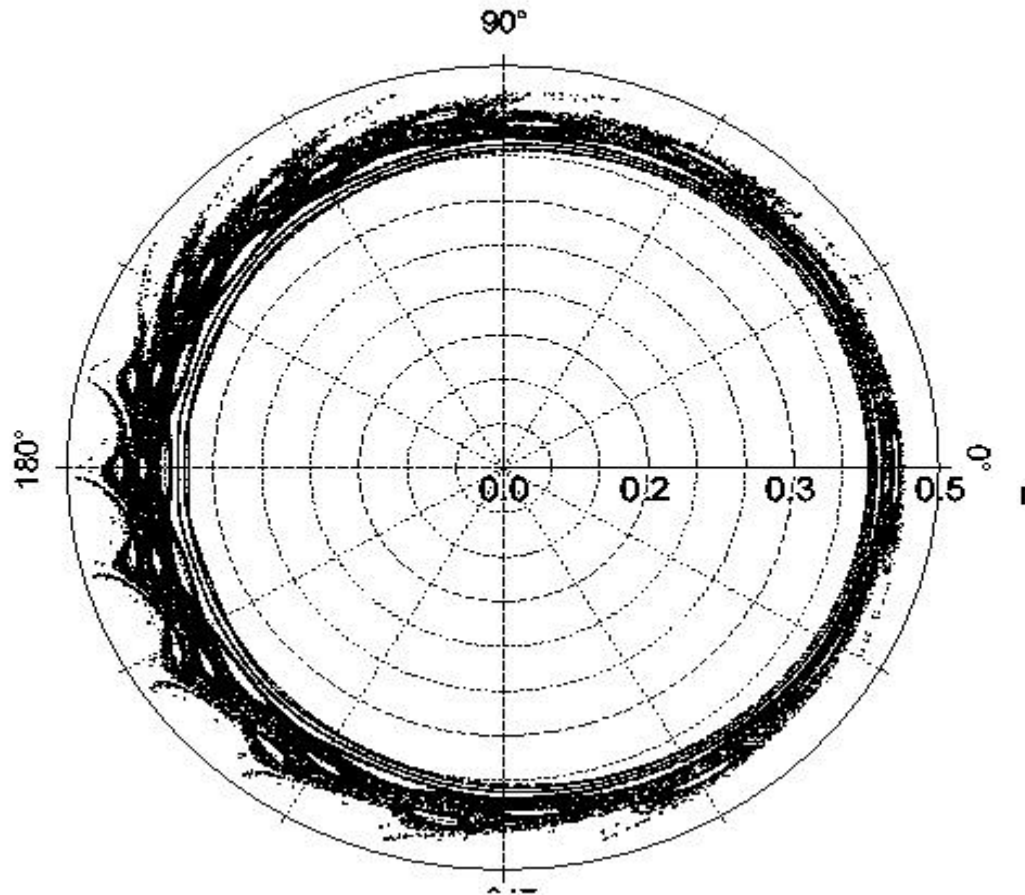


1 kHz - 10 kHz operation

- **Smearing out of local heat fluxes**
- **Generation of temporal ergodization**
- **Generation of a differential plasma rotation**
- **Improvement of plasma confinement**
- **Delay of disruption limit**
- **Plasma compression in front of pump limiter**

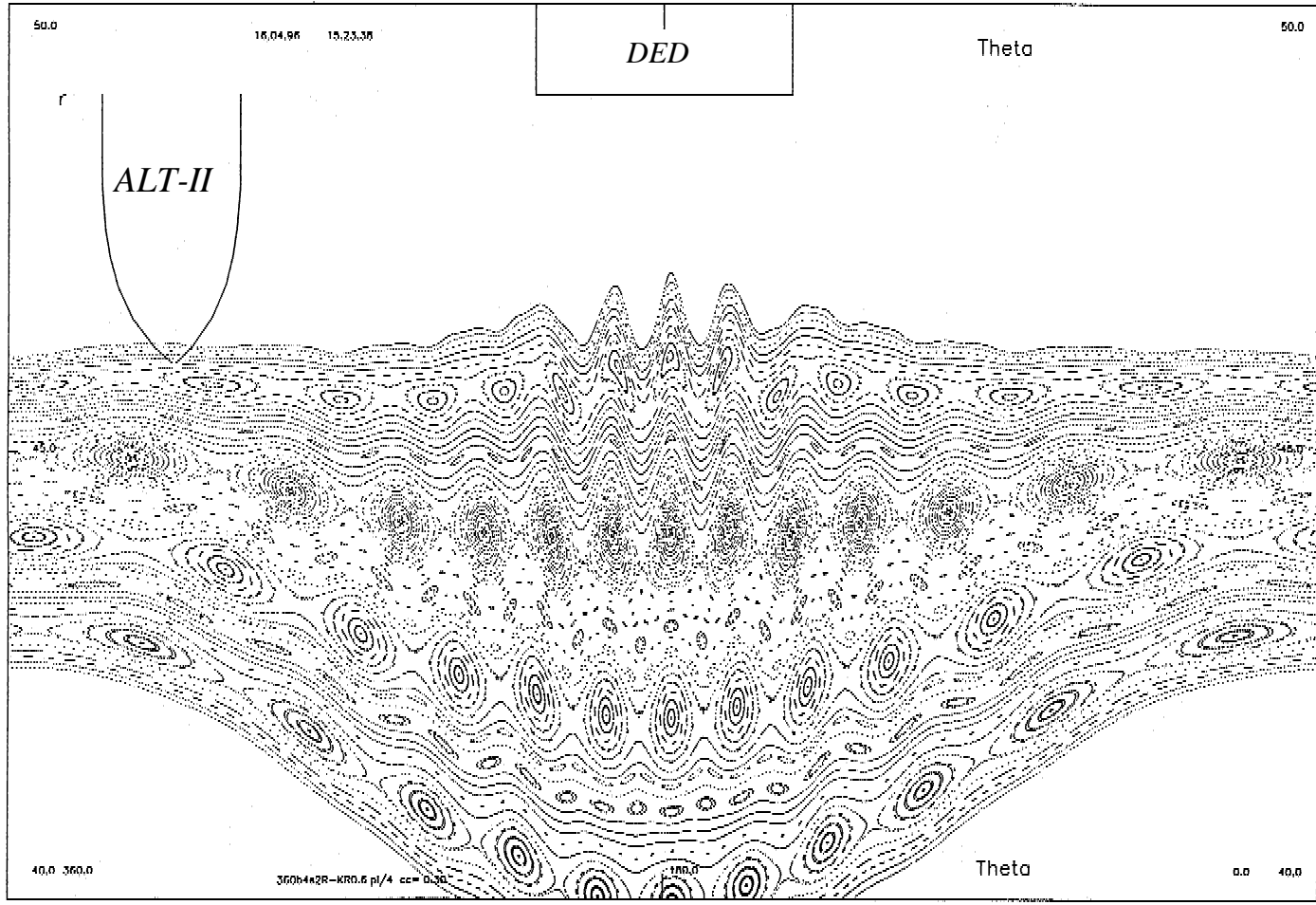


$I_{\text{pol}} = 480 \text{ kA}$, $r_{\text{res}} = 44.26 \text{ cm}$





$r=0.5\text{ m}$



$r=0.4\text{ m}$

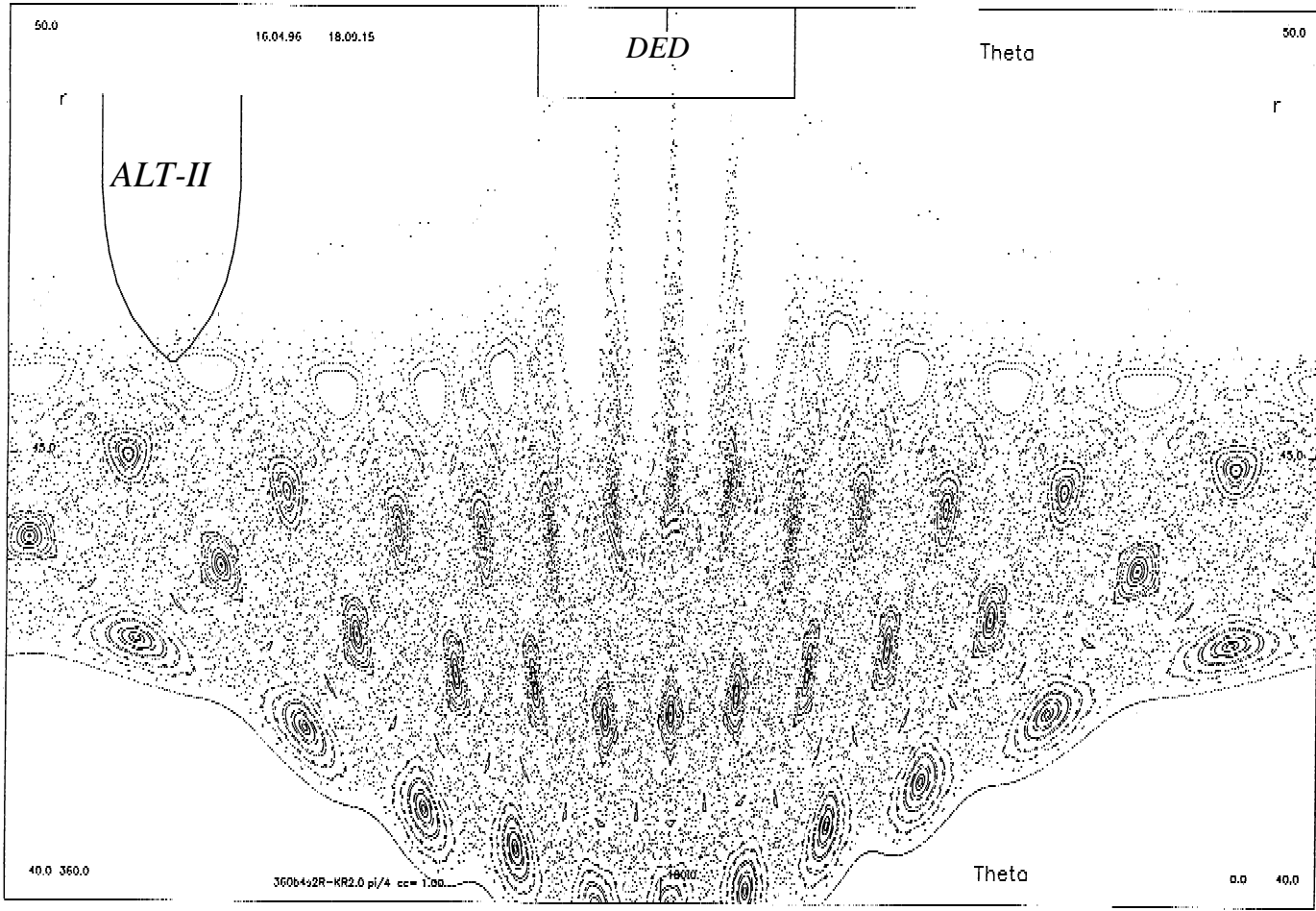
$\Theta = 360^\circ$

30 % perturbation current

$\Theta = 0^\circ$



$r=0.5$ m

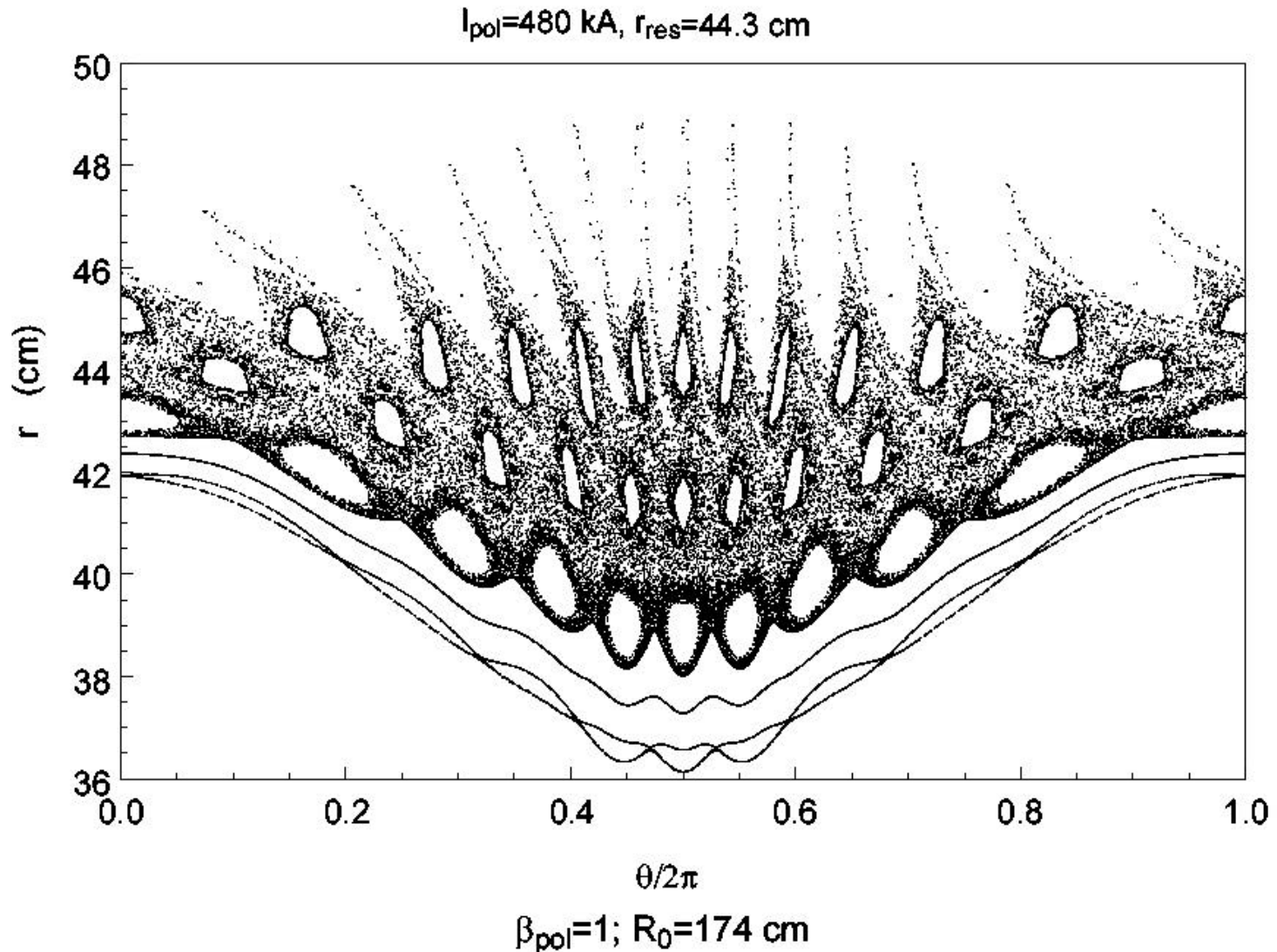


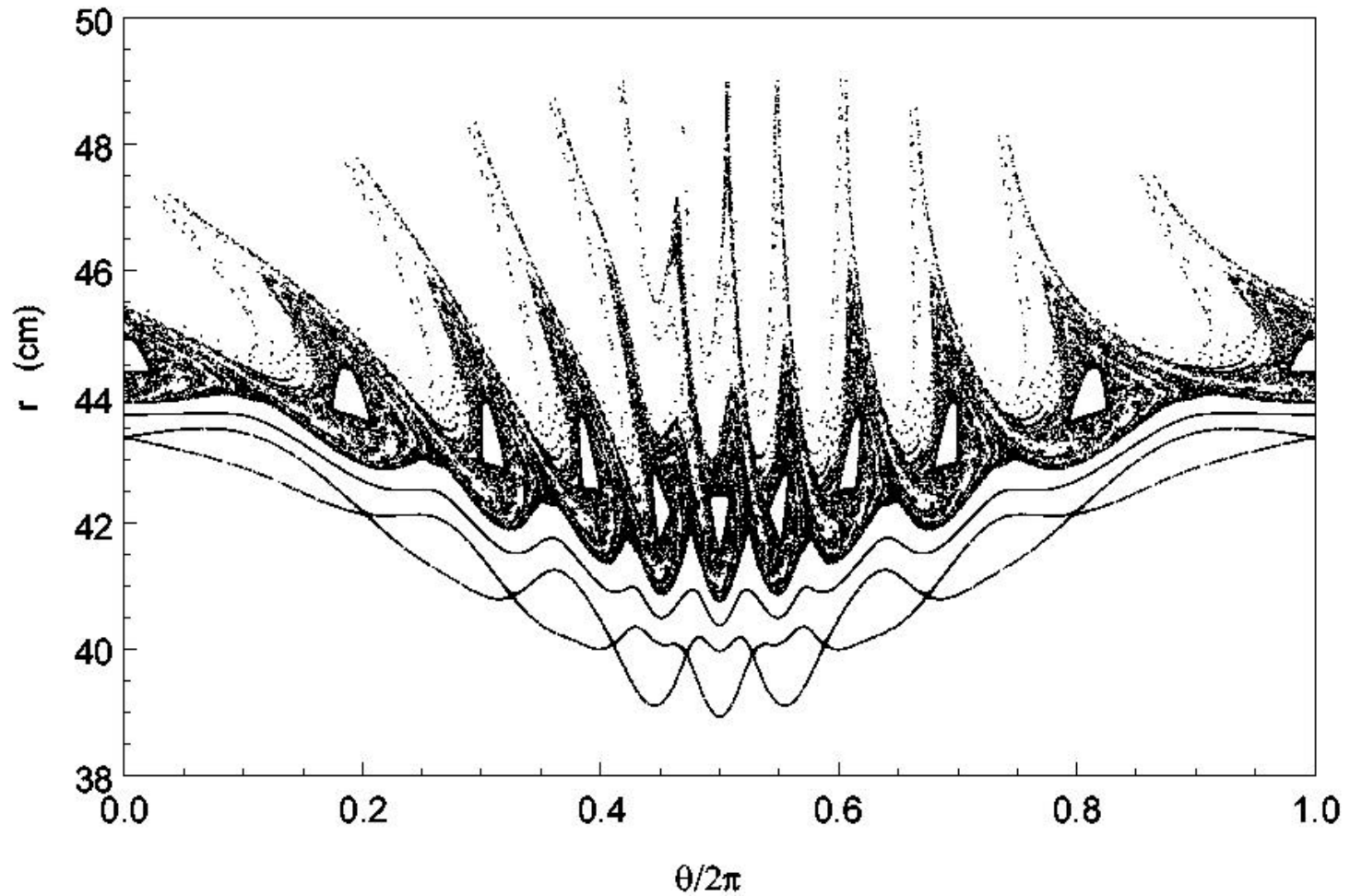
$r=0.4$ m

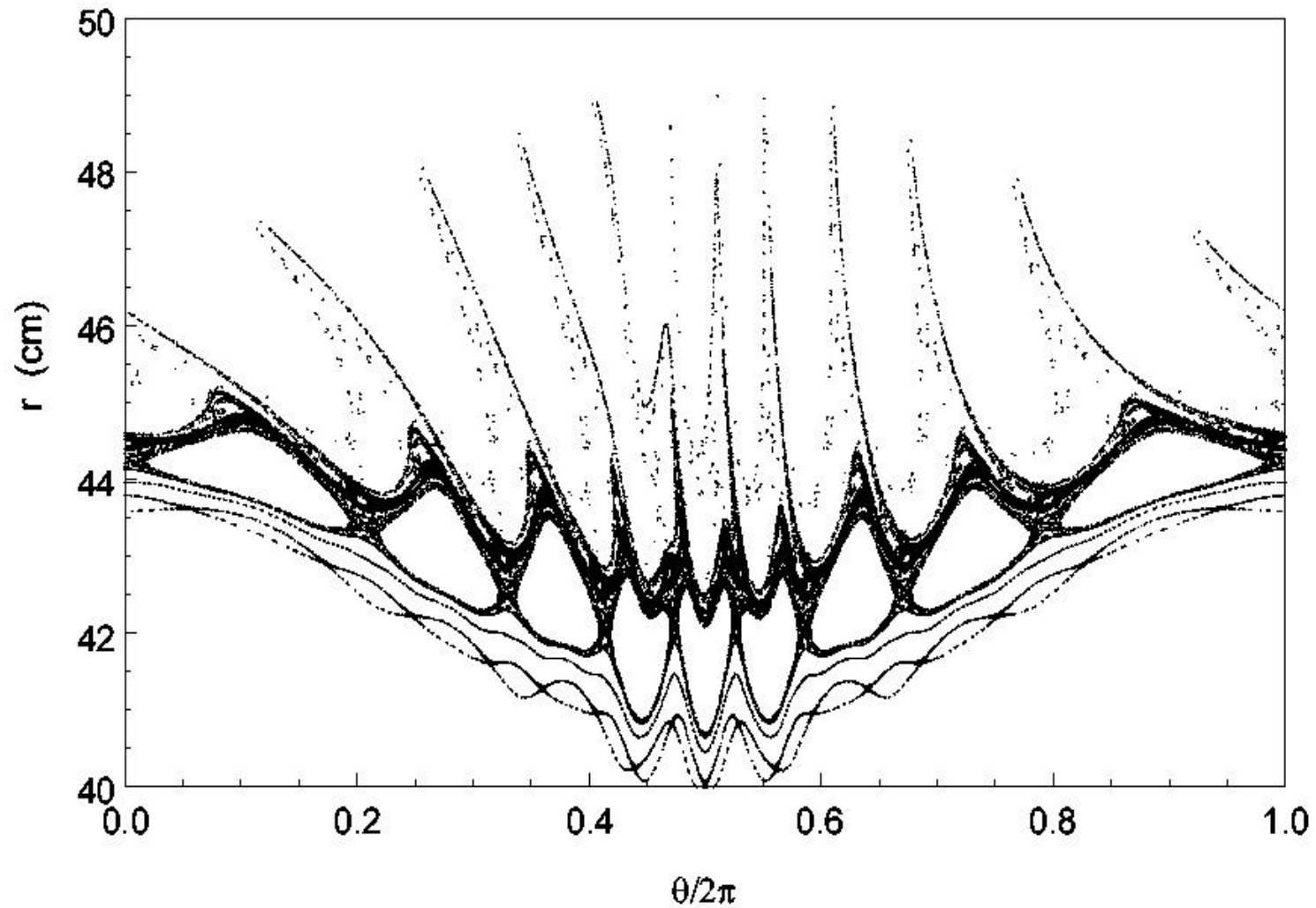
$\Theta = 360^\circ$

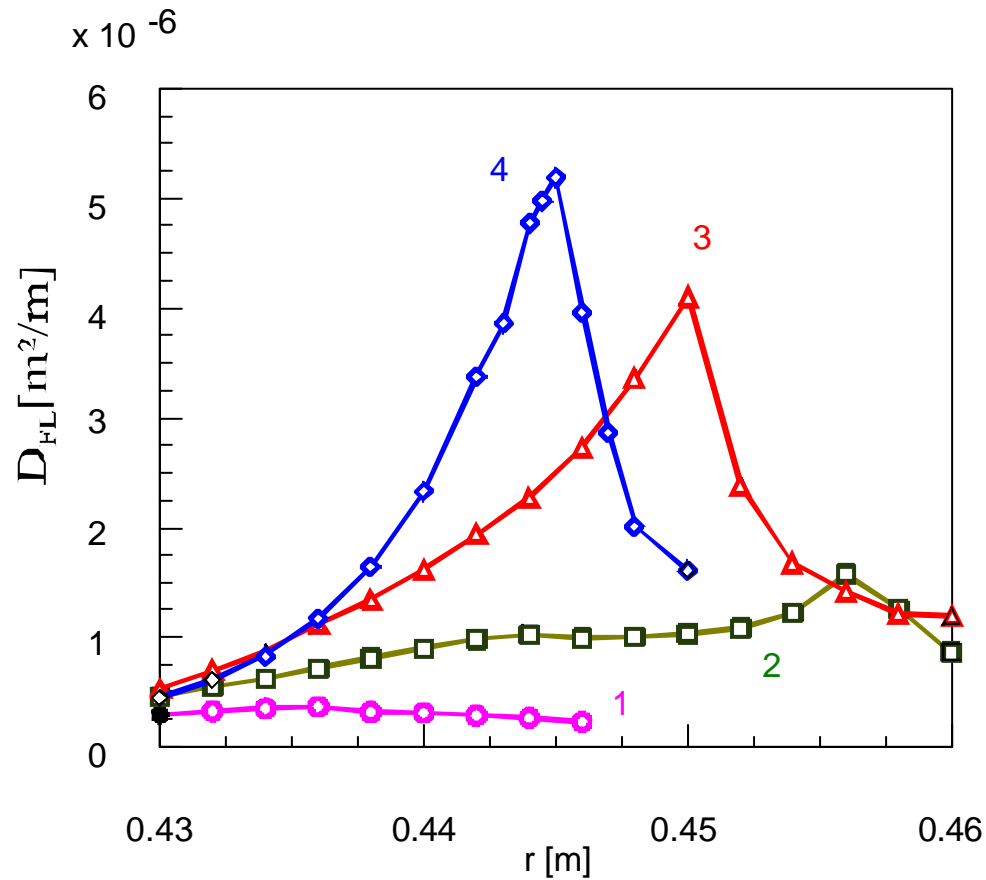
100 % perturbation current

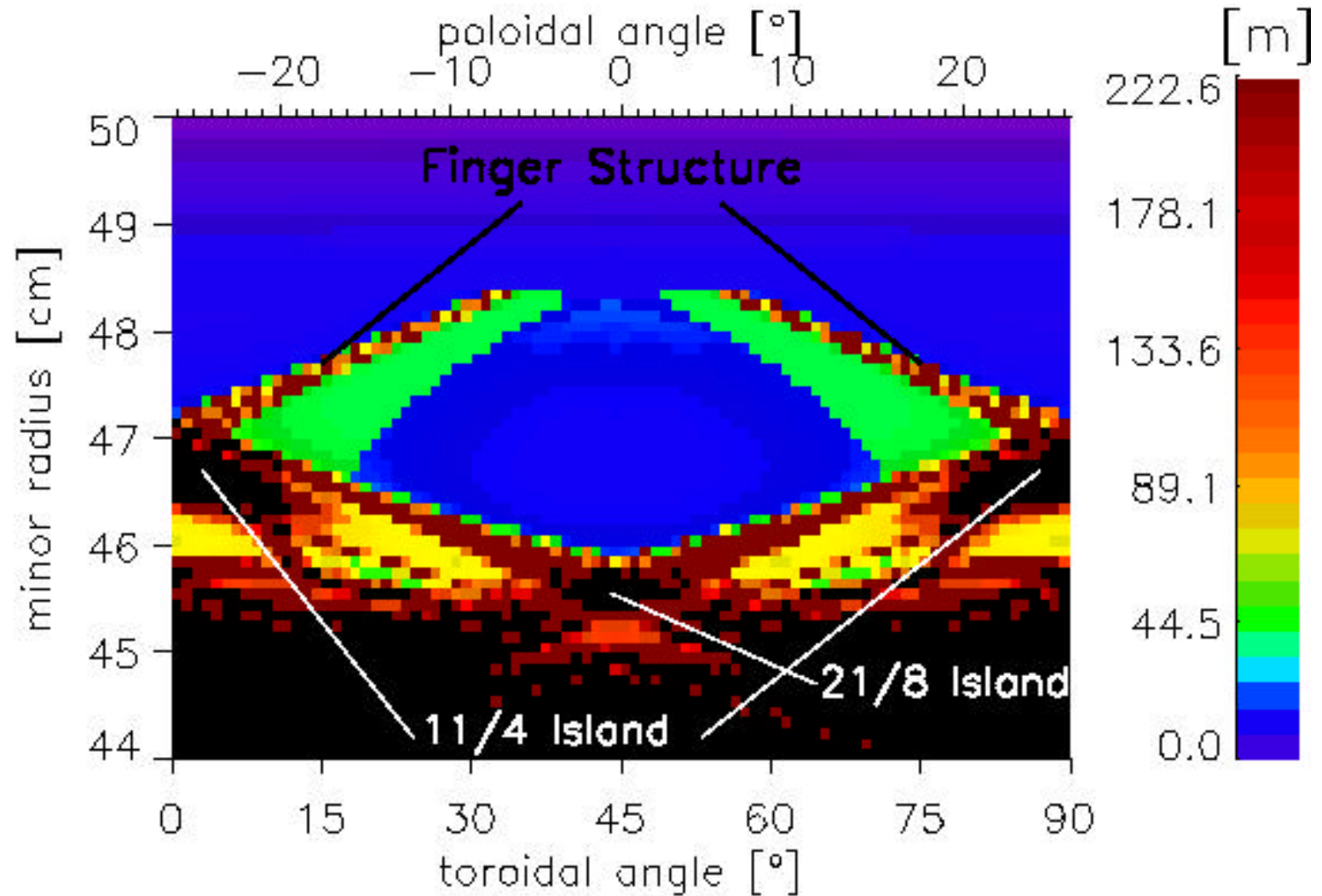
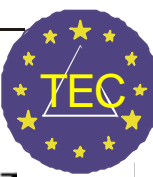
$\Theta = 0^\circ$

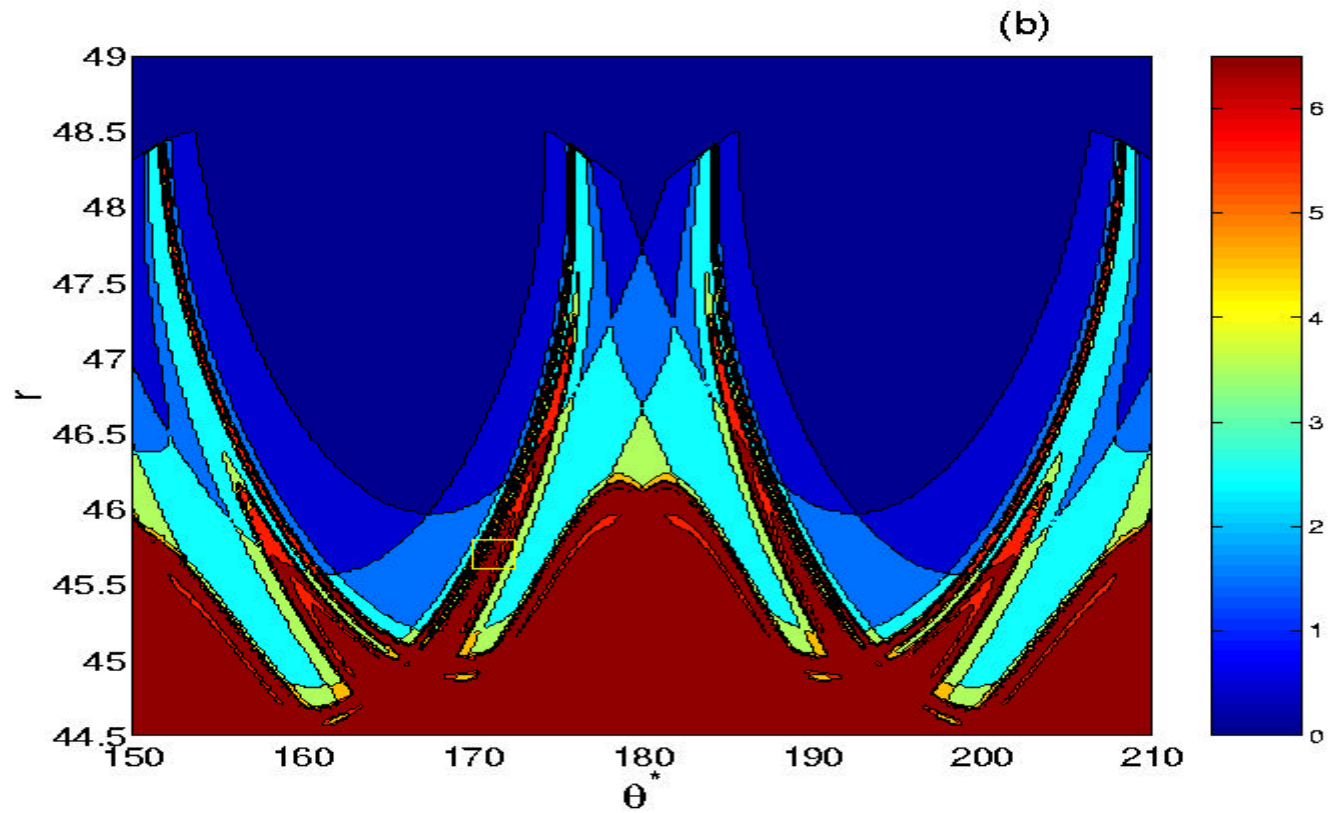


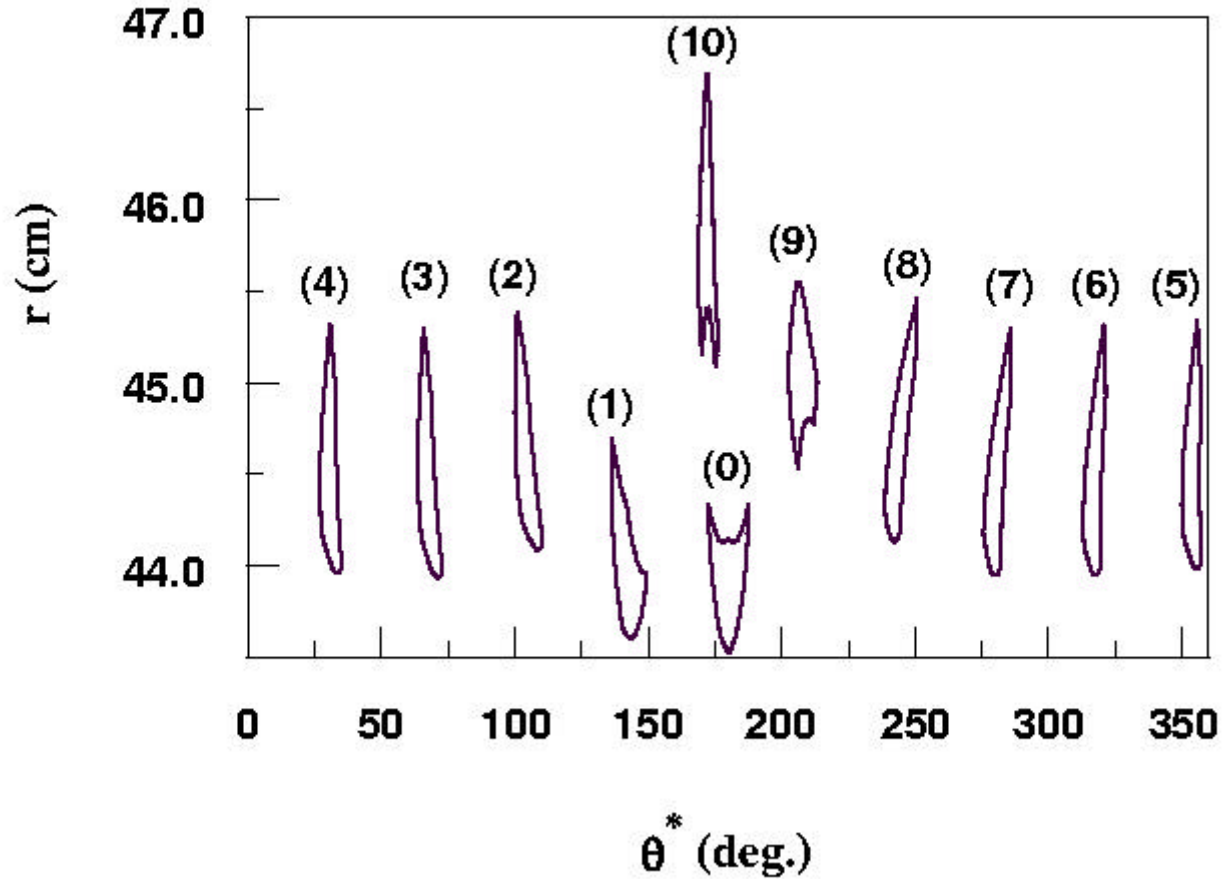
$I_{\text{pol}} = 550 \text{ kA} , r_{\text{res}} = 46.7 \text{ cm}$  $\beta_{\text{pol}}=1; R_0=174 \text{ cm}$

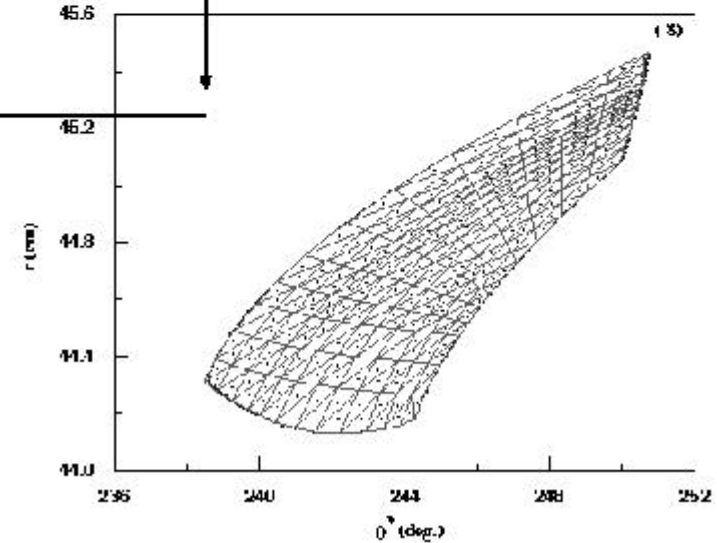
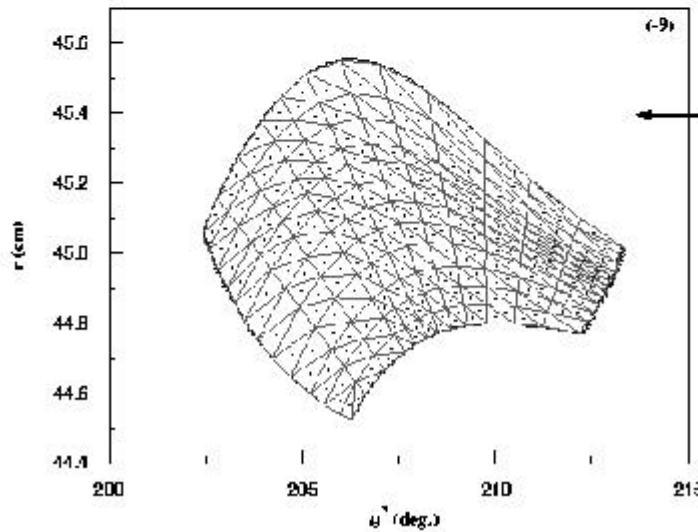
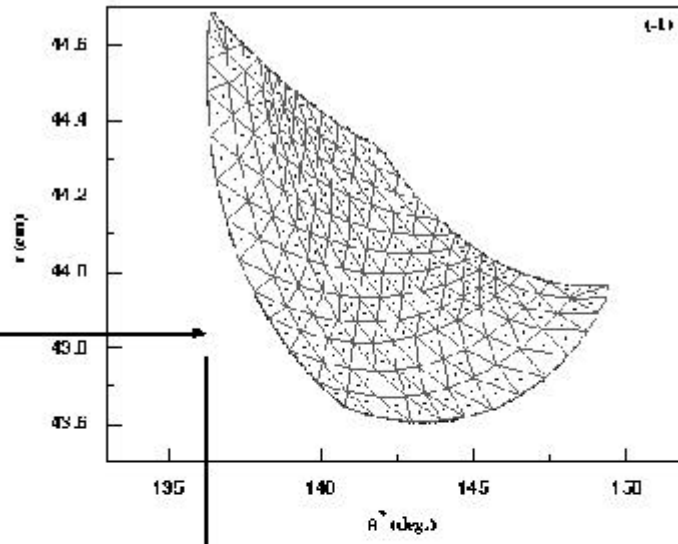
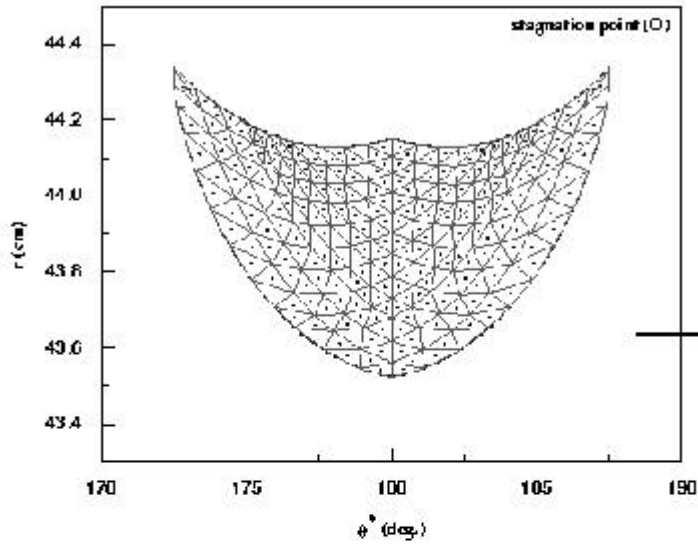
$I_{pol} = 600 \text{ kA}, r_{res} = 48.33 \text{ cm}$  $\beta_{pol}=1; R_0=174 \text{ cm}$

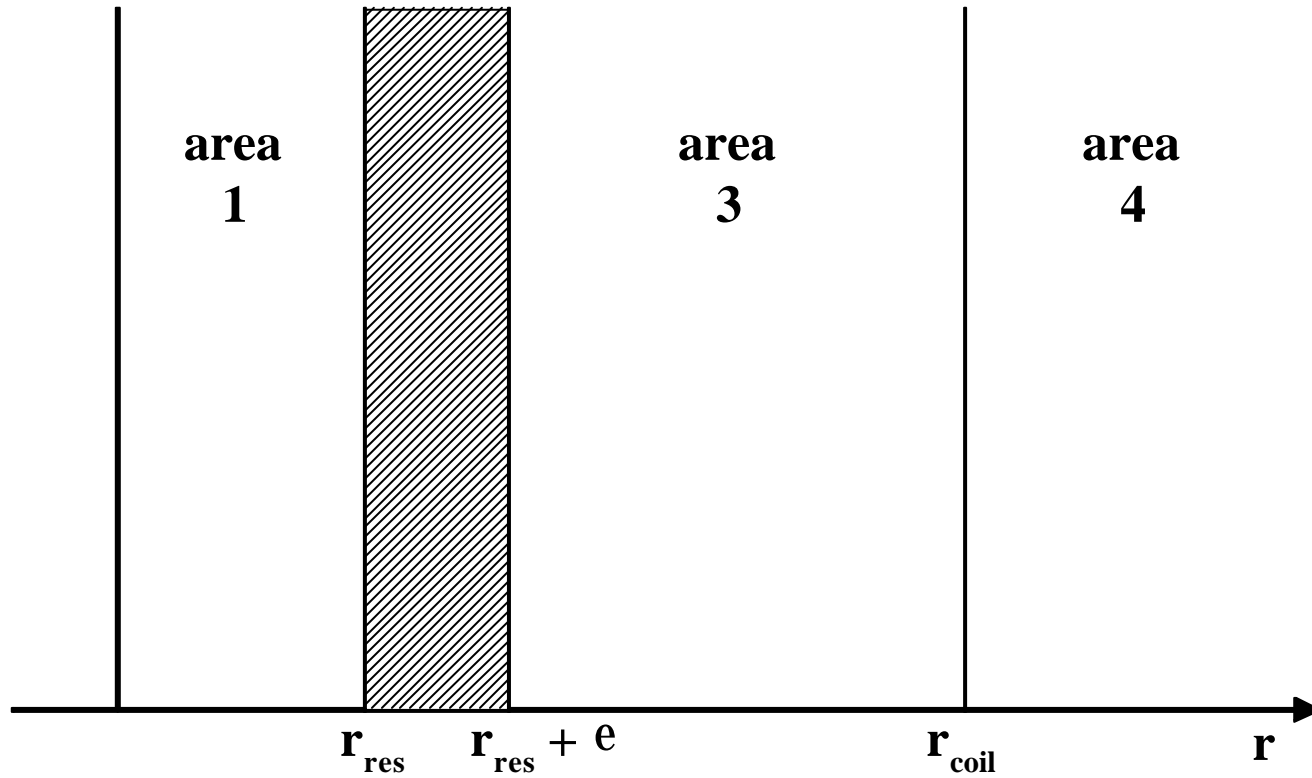


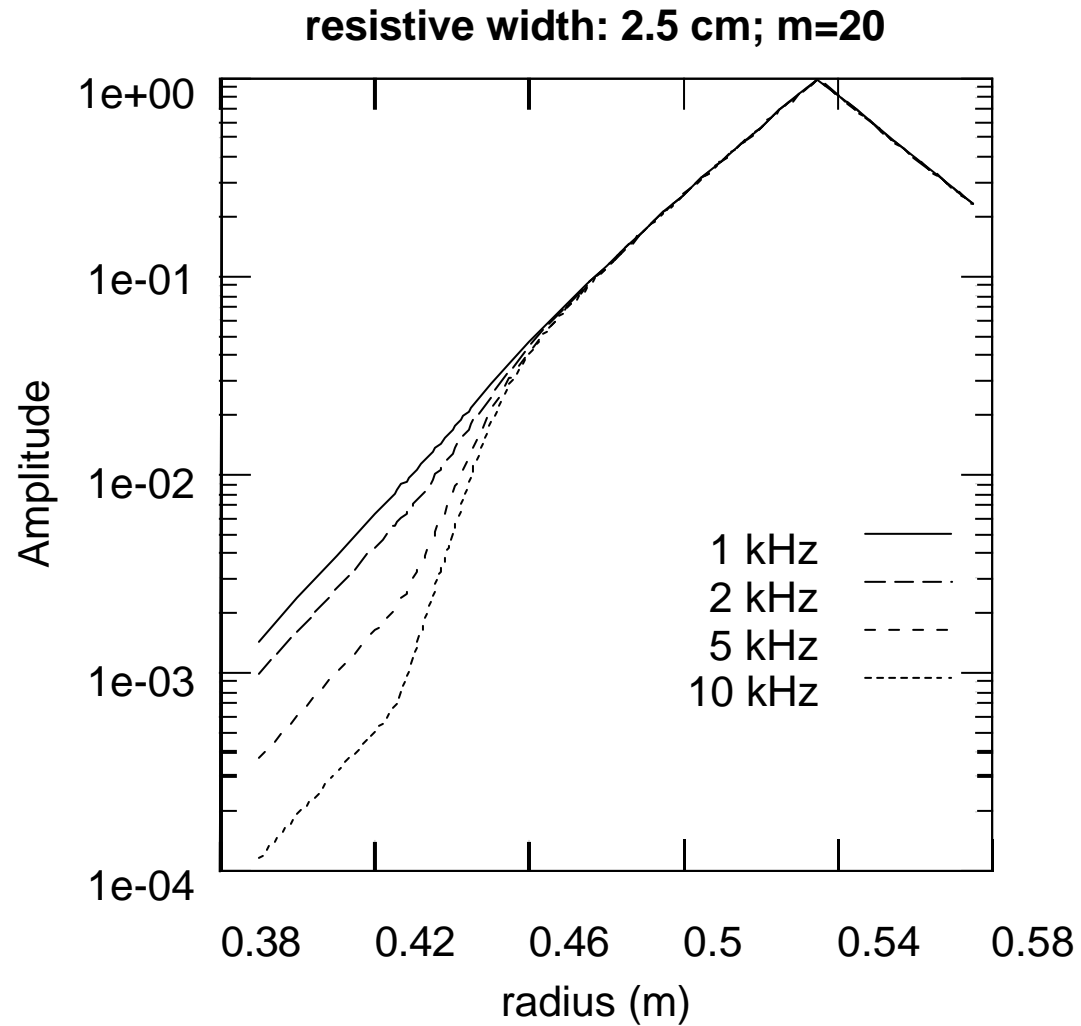


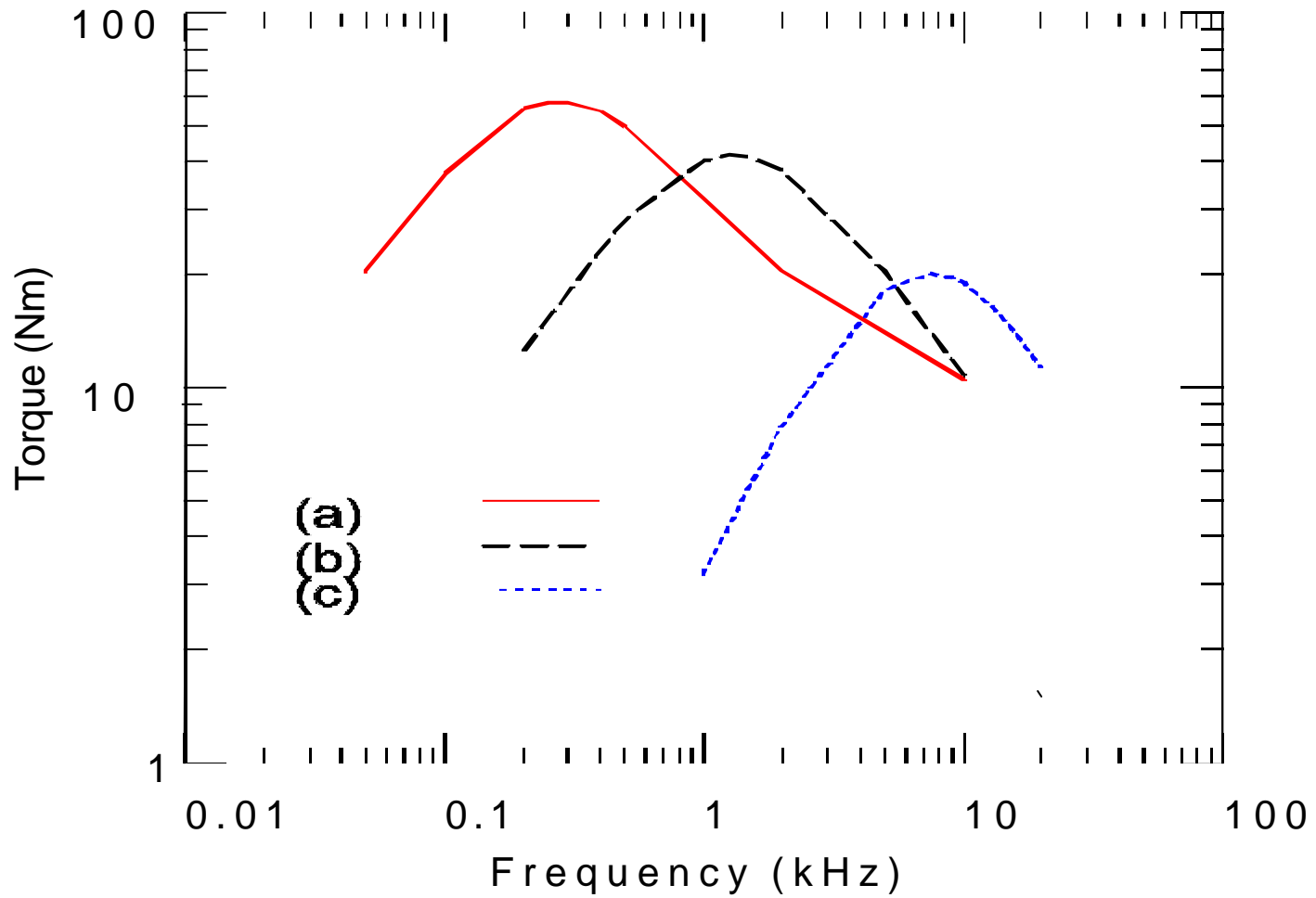
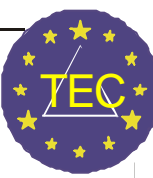


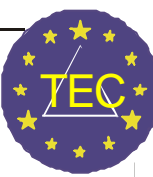












Summary

The DED-coils are continuous helical windings located at the HFS inside the vessel.

The Dynamic ergodic divertor will most likely provide a sufficient ergodization level at the plasma edge.

A laminar zone will form the main contact region with the wall; a 2D and 3D modeling was successful.

The field rotation imposes a torque at the plasma edge which is probably sufficient for generating a differential plasma rotation.

The differential rotation may lead to a suppression of turbulence and an improvement of the confinement; locked modes should be acceterated again.

