

Transport Modeling for W7-X on the Basis of W7-AS Experimental Results

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- High-performance discharges $(n(0) \ge 5 \times 10^{19} \text{ m}^{-3}, T \ge 1 \text{ keV})$ in W7-AS were well described by neoclassical theory.
- Although *B* chosen to reduce neoclassical losses in W7-X, their strong temperature dependence remains unchanged.
- ECRH power deposition and current drive (ECCD) in W7-AS discharges conformed to theoretical predictions.
- High-temperature discharges in W7-X should allow O2 heating (relevant for high-density operation).



- Brief review of relevant W7-AS results
- Numerical tools employed
- W7-X configurations and their properties
- Scenarios and results of transport modeling
- Summary and outlook

shot 34313: 680 kW NBI, 750 kW ECRH absorbed power



IDΠ

W7-AS: au_E Scaling With n for 1.2 MW ECRH Discharges



 $\chi^e_{an} \propto n^{-1}$ in edge region same dependence as found in the neoclassical $1/\nu$ regime

 $\Rightarrow \tau_E \propto n$

In contrast, ISS04 scaling has

 $\tau_E^{ISS04} \propto n^{0.54}$



ECCD launch-angle scans in $\epsilon = 0.35$ configuration of W7-AS

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The predictive 1-D transport code used (Yu. Turkin, *et al.*) solves the system of equations

$$\frac{3}{2}\frac{\partial}{\partial t}(n^{\alpha}T^{\alpha}) + \frac{1}{V'}\frac{\partial}{\partial r}(V'Q^{\alpha}) = P^{\alpha} + q^{\alpha}\Gamma^{\alpha}E_{r} \qquad \alpha = e, i$$

$$\frac{1}{V'}\frac{\partial}{\partial r}\left(V'rD_{E}\frac{\partial}{\partial r}\left(\frac{E_{r}}{r}\right)\right) - \epsilon_{0}\left(\frac{c}{v_{a}}\right)^{2}\left(1 + \frac{b_{1,0}^{2}}{\iota^{2}\epsilon_{t}^{2}}\right)\frac{\partial E_{r}}{\partial t} = \sum_{\alpha}q^{\alpha}\Gamma^{\alpha}$$

$$\sigma\frac{\partial\psi_{p}}{\partial t} = \frac{1}{2}\frac{1}{\tau}\frac{\partial}{\partial t}\left(V'\frac{\partial\psi_{p}}{\partial t}\right) - 2\pi R_{0}\left(L_{r} + L_{r} + L_{r}\right)$$

$$\sigma \frac{\partial r}{\partial t} - \frac{\partial r}{\mu_0} \frac{\partial r}{V'} \frac{\partial r}{\partial r} \left(V' \frac{\partial r}{\partial r} \right) = 2\pi R_0 \left(J_{bs} + J_{cd} + J_{ohm} \right)$$

$$\Gamma^{\alpha} = \Gamma^{\alpha}_{neo} - I\!\!D_{an} \frac{\partial n^{\alpha}}{\partial r} \qquad \qquad Q^{\alpha} = Q^{\alpha}_{neo} - \chi^{\alpha}_{an} n^{\alpha} \frac{\partial T^{\alpha}}{\partial r} - \frac{5}{2} I\!\!D_{an} T^{\alpha} \frac{\partial n^{\alpha}}{\partial r}$$

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The ray-tracing code TRAVIS (N. B. Marushchenko, et al.):

- calculates ray trajectory accounting for anomalous dispersion,
- calculates absorption in the fully relativistic approach,
- accounts for parallel electron momentum conservation (ECCD),
- can separate the trapped- and passing-electron contributions to macroscopic quantities it determines,
- allows for multiple-ray and multiple-pass scenarios,
- is user-friendly with extensive graphical interface,
- loads *B* from "magnetic configuration" library,
- operates stand-alone or coupled to the transport code.

IPP Relevant W7-X Characteristics – Dependence on b_{01} and eta№ 12 ₿ 3 0.7 0.6 10 0.5 0.4 0.3 **High-Mirror** 8 2 Standard ϵ_{eff} b01 6 4 0.2 0.1 2 -Low-Mirror 0.0 0 0 0.6 r/a 0.8 0.6 1.0 0.0 0.2 1.0 0.2 0.8 0.0 0.2 0.4 0.6 0.8 0.4 0.0 0.4 1.0 r/a r/a № 12-№ 1.2 0.7 -Standard vacuum 0.6 10 1.0 Standard $<\beta>=2\%$ 0.5 Standard $<\beta>=4\%$ 8 0.8 0.4 ϵ_{eff}^{eff} b01 ÷ 6 0.3 0.4 4 0.2 2 -0.2 -0.1 . Tu 0 0.0 0.0 0.6 r/a 0.0 0.2 0.4 0.8 1.0 0.0 0.2 0.4 0.6 0.8 1.0 0.0 0.2 0.4 0.6 0.8 1.0 r/a

r/a

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Off-Axis X2 for Vacuum W7-X High-Mirror Configuration

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Small ECCD sufficient to balance *I*_{bs} in High-Mirror Configuration

... and the Underlying Transport Coefficients





Summary of X2 Results





- $I_{bs} + I_{cd} \approx 0$ realistic for all W7-X configurations heated using 10 MW ECRH in X2 mode.
- Off-axis heating preferable \rightarrow avoid $\epsilon \approx 0$ near plasma center \rightarrow avoid electron root (high-mirror).
- Confinement improves with increasing β (low-mirror?)

Launch Geometry for the O2 Mode





all distances in meters

Transport Modeling for W7-X



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IPP **On-Axis O2 for** $<\beta>=4\%$ W7-X Standard Configuration $n_e [10^{20}/m^3]$ T_e, T_i [keV] $E_r [kV/m]$ 1.8 0 6 1.35 -4.5 4.5 0.9 3 1.5 -9 0.45 -13.5 0 E 0 0.3 r [m] 0.3 r [m] 0.3 r [m] 0.15 0.45 0.15 0.45 0.15 0.45 0 0 0 P_{ECRH} [MW/m³] j^e_{bs} jⁱ_{bs} j_{bs} [A/m²] ι_{cf}, ι_{bs} 6 1.045 1.95[.]10⁵ 4.5 0.99 1.3[.]10⁵ 0.935 1.5 6.5[.]10⁴ 0.88 **o** \mathbf{x} 0.45 0.3 r [m] 0.15 0.3 r [m] 0.45 0.3 r [m] 0.15 0 0.15 0.45 0 $I_{bs} = 82 \text{ kA}$ $P_{abs} = 9.75 \text{ MW}$ $<\beta>=4.13$ %



- ECCD compensation of the bootstrap current is possible for all X2 scenarios.
- ECCD becomes marginal for O2 conditions \rightarrow Bootstrap current contribution to * must be factored into discharge scenario.
- Refinements \rightarrow modeling of $\epsilon \approx 0$ regions; correction of neoclassical transport coefficients for conservation of momentum.
- Carry out free-boundary VMEC runs including internal current densities determined in simulations → extend field to vacuum region to model effects on divertor strike points.
- Develop plausible discharge scenarios.

Scalings of 1/
u Transport with Dimensional Examples

 $1/\nu$ transport scales as:

$$D_{1/
u} \propto rac{\epsilon_{eff}^{3/2} T^{7/2}}{n R_0^2 B_0^2}$$

Parameters for which $\chi^e_{neo} > 1 \text{ m}^2/\text{s}$ at r/a = 0.5

$n (10^{20} m^{-3})$	W7-AS	W7-X	"classical" W7-X
0.1	0.90 keV	3.50 keV	$1.35 { m ~keV}$
0.4	$1.25 \ \mathrm{keV}$	$5.20 \ \mathrm{keV}$	$2.00 \ \mathrm{keV}$
1.0	$1.60 { m keV}$	$6.70 \ \mathrm{keV}$	$2.50 { m ~keV}$

where possible effects due to E_r have been ignored.

shot 34609: 830 kW NBI, 330 kW ECRH absorbed power

