

### §38. Experimental Work to Estimate Tritium Leak Rate through Recovery Loop in Falling Liquid LiPb Blanket of Laser Fusion Reactor

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In this collaboration work, LiPb-H<sub>2</sub> or -D<sub>2</sub> solubility and diffusivity, their isotope effects, a design study of LiPb loop and estimation of leak rate from the Li-Pb system are performed in 2011 [1-4]. Koyo-fast is a conceptual design for laser fusion reactor. Its total heat power is 1GWt, and Li-Pb circulates to protect its reactor chamber wall from high-intensity neutron irradiation. Li<sub>15.8</sub>Pb<sub>84.2</sub> has a liquid metal with the eutectic temperature at 235°C. The Li-Pb flow rate is 18.3t/s, and the inlet and outlet temperatures are 300°C and 500°C. In order to achieve self-sufficiency of tritium in the fusion reactor system, tritium generation rate in the reactor chamber is 1.5MCi/day. The tritium concentration in Li-Pb is estimated  $9.6 \times 10^{-9} \text{T/LiPb}$ , and the equilibrium pressure is  $1.8 \times 10^{-3} \text{Pa}$ . Li-Pb is supplied from the top of the reactor chamber, and goes out from the bottom. The whole system is illustrated in Fig. 1. Heat generated by the D-T and Li-n reactions is recovered by the Rankine cycle through the LiPb-H<sub>2</sub>O heat exchanger. The heat-transfer coefficient determined from the Dittus-Boelter equation is  $5 \times 10^3 \text{ W/m}^2\text{K}$ . Then, the surface area of the heat exchanger is estimated  $690 \text{ m}^2$ .

Tritium generated by the Li-n reaction is present as an atomic form in the Li-Pb flow. Since the tritium solubility is comparatively low, the Sieverts' law is held between tritium and LiPb. Tritium generated in the LiPb flow diffuses through a liquid boundary layer and reaches at the LiPb-metal interface. Then tritium is dissolved in metallic walls of the heat exchanger and diffuses through it to the secondary flow. Tritium atoms recombine to a molecular form and disperse in the secondary flow. The tritium permeation is a function of tritium diffusion through Li-Pb boundary layer and permeation through tube walls. The former is estimated from the mass-transfer coefficient of the LiPb boundary layer and the latter is correlated in terms of permeability. In especial, the former is a function of the velocity of Li-Pb flow and correlated in terms of Reynolds number and Sherwood number. The Sherwood number, Sh, is defined as  $Sh = k_{T, \text{LiPb}} d / D_{T, \text{LiPb}}$ , where d is a diameter of heat-exchanger tube. Figure 2 shows the tritium permeation rate as a function of the Sherwood number and the tritium concentration in Li-Pb. The present design values are considered proper judging from the overall tritium permeation rate and the design scale of heat exchanger.

Papers presented in 2011

- 1) T. Norimatsu, H. Saika, H. Homma, M. Nakai, S. Fukada; Leakage control of tritium through heat cycles of conceptual-design, laser-fusion reactor Koyo-F, Fusion Science and Technology, 60 (2011) 893-89.
- 2) S. Fukada, Y. Edao; Unresolved issues on tritium mass transfer in Li-Pb liquid blankets, Journal of Nuclear Materials, 417 (2011) 727-730.
- 3) Y. Edao, H. Okitsu, H. Noguchi, S. Fukada; Permeation of two-component hydrogen isotopes in lithium-lead eutectic alloy, Fusion Science and Technology, 60 (2011) 1163-1166.
- 4) Y. Edao, H. Noguchi, S. Fukada; Experiments of hydrogen isotope permeation, diffusion and dissolution in Li-Pb, Journal of Nuclear Materials, 417 (2011) 723-726.

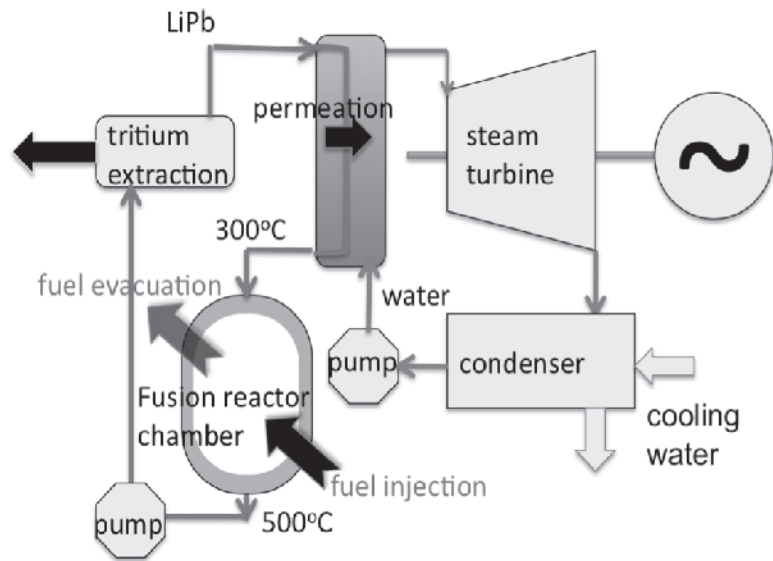


Fig. 1 LiPb loop for Laser fusion reactor and steam Rankine cycle

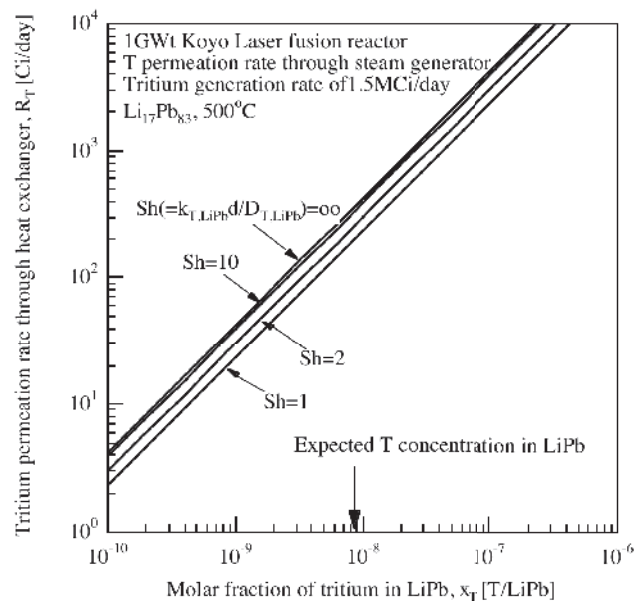


Fig. 2 Tritium permeation rate through heat exchanger tube